
**Wireless 2.0: Smart Radio Environments
Empowered by Reconfigurable Intelligent Surfaces
(How it Works, State of Research, and the Road Ahead)**

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The Main Takes of this Talk

- ❑ Smart Radio Environments
- ❑ Smart Surfaces: “Tiny” Antennas vs. Metasurfaces
- ❑ Surface Electromagnetics: Modeling Metasurfaces
- ❑ Uses, Applications, Prototypes of Smart Surfaces
- ❑ Advantages and Limitations of Smart Surfaces
- ❑ Recent Research Activities
 - ❑ Path-Loss Modeling of Metasurfaces **[new]**
 - ❑ Joint Encoding, Performance Evaluation, Training Overhead
- ❑ What’s Next ?

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- ❑ What’s Next ?
- ❑ **WTC-SIG “RISE” & other IEEE-COMSOC activities**

REVIEW

Open Access

Smart radio environments empowered by reconfigurable AI meta-surfaces: an idea whose time has come



Marco Di Renzo^{1*} , Merouane Debbah², Dinh-Thuy Phan-Huy³, Alessio Zappone⁴, Mohamed-Slim Alouini⁵, Chau Yuen⁶, Vincenzo Sciancalepore⁷, George C. Alexandropoulos⁸, Jakob Hoydis⁹, Haris Gacanin¹⁰, Julien de Rosny, Ahcene Bounceur¹², Geoffroy Lerosey¹³ and Mathias Fink¹¹

Abstract

Future wireless networks are expected to constitute a distributed intelligent wireless communications, sensing, and computing platform, which will have the challenging requirement of interconnecting the physical and digital worlds in a seamless and sustainable manner. Currently, two main factors prevent wireless network operators from building such networks: (1) the lack of control of the wireless environment, whose impact on the radio waves cannot be customized, and (2) the current operation of wireless radios, which consume a lot of power because new signals are generated whenever data has to be transmitted. In this paper, we challenge the usual “more data needs more power and emission of radio waves” status quo, and motivate that future wireless networks necessitate a smart radio environment: a transformative wireless concept, where the environmental objects are coated with artificial thin films of electromagnetic and reconfigurable material (that are referred to as reconfigurable intelligent meta-surfaces), which are capable of sensing the environment and of applying customized transformations to the radio waves. Smart radio environments have the potential to provide future wireless networks with uninterrupted wireless connectivity,

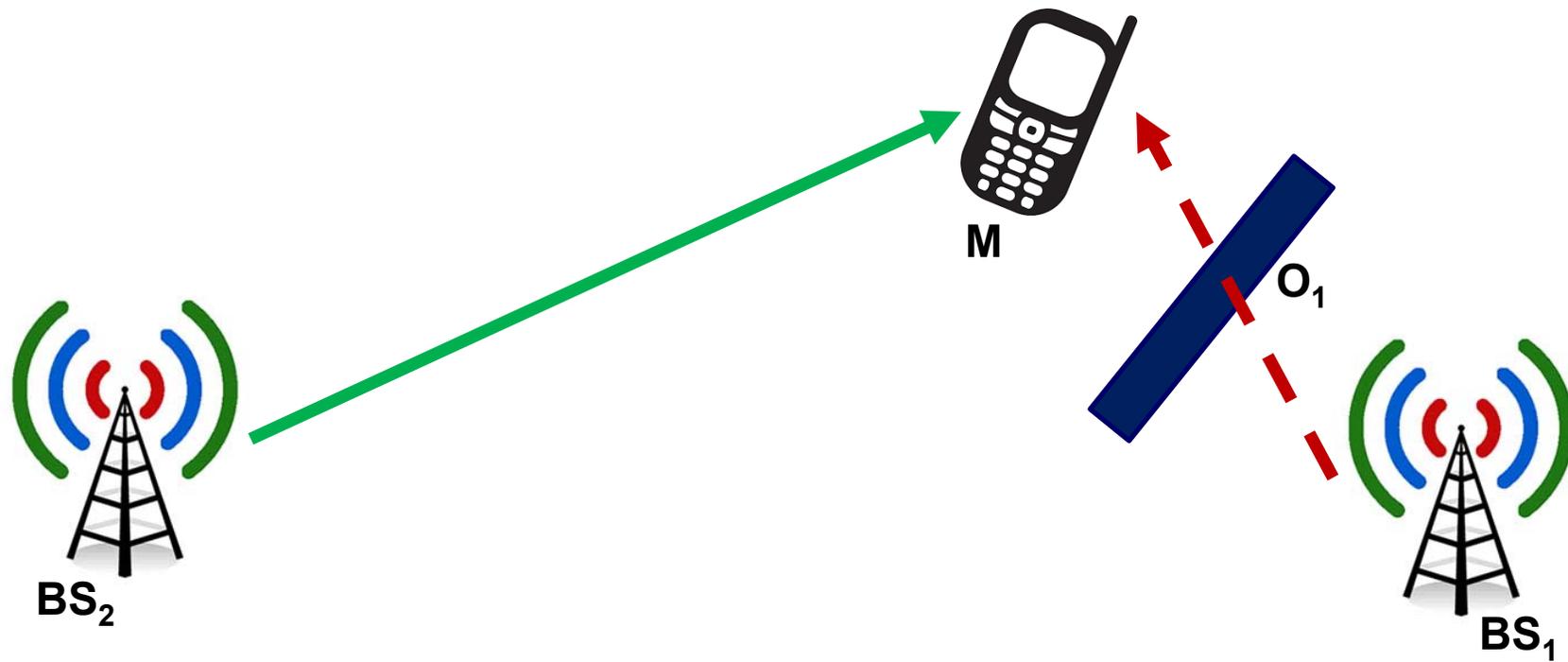
Current Wireless Networks



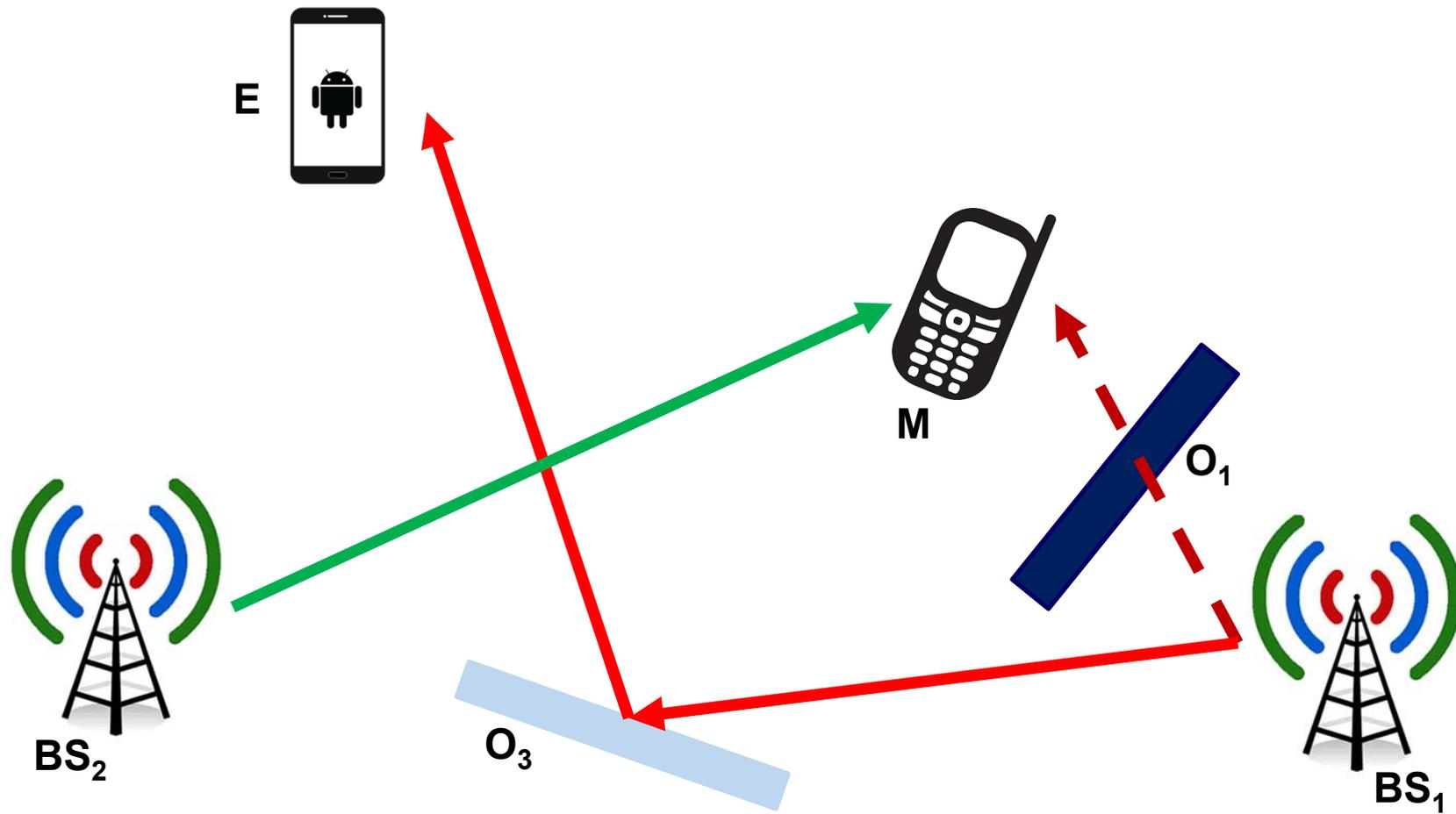
Current Wireless Networks



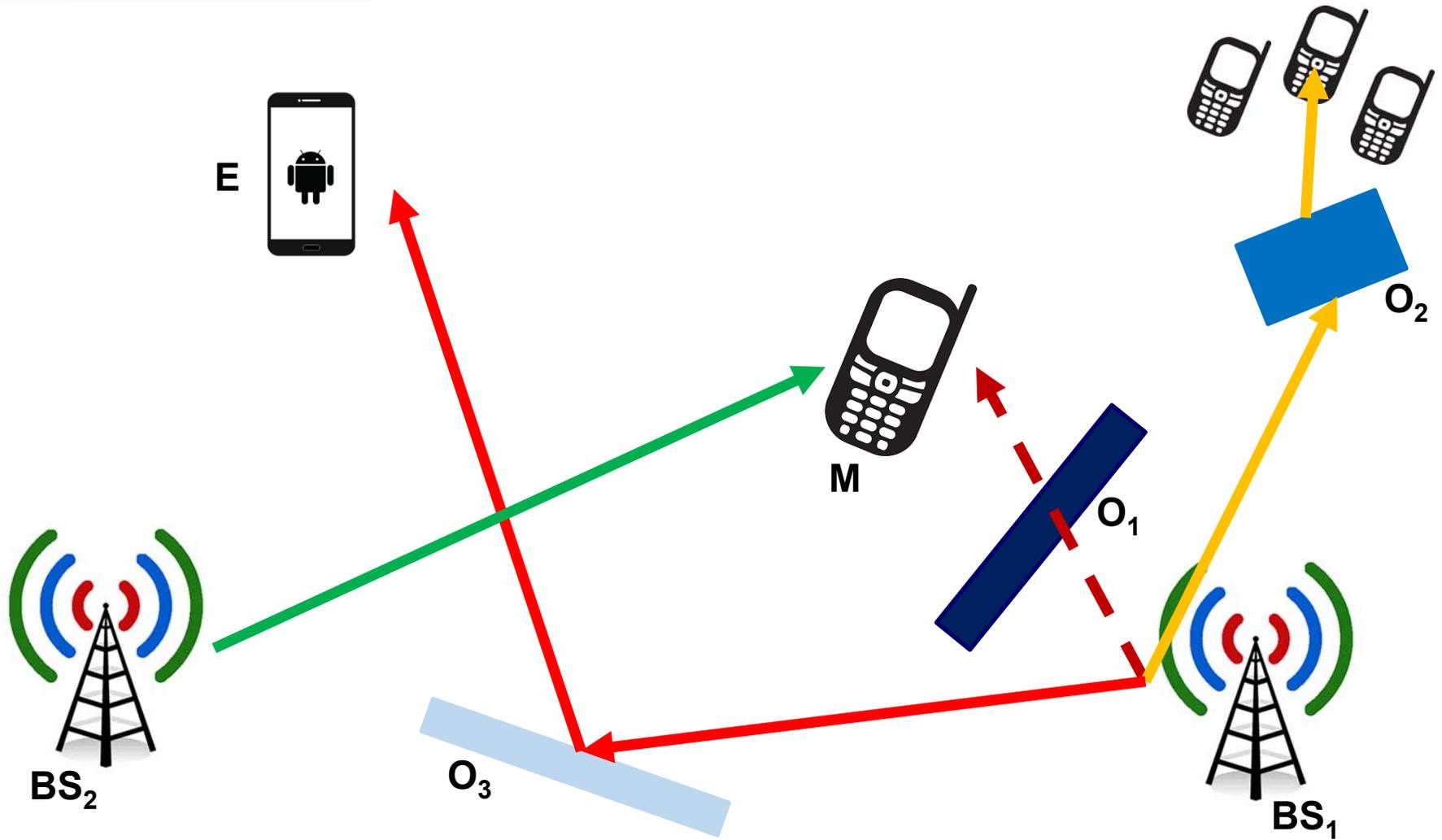
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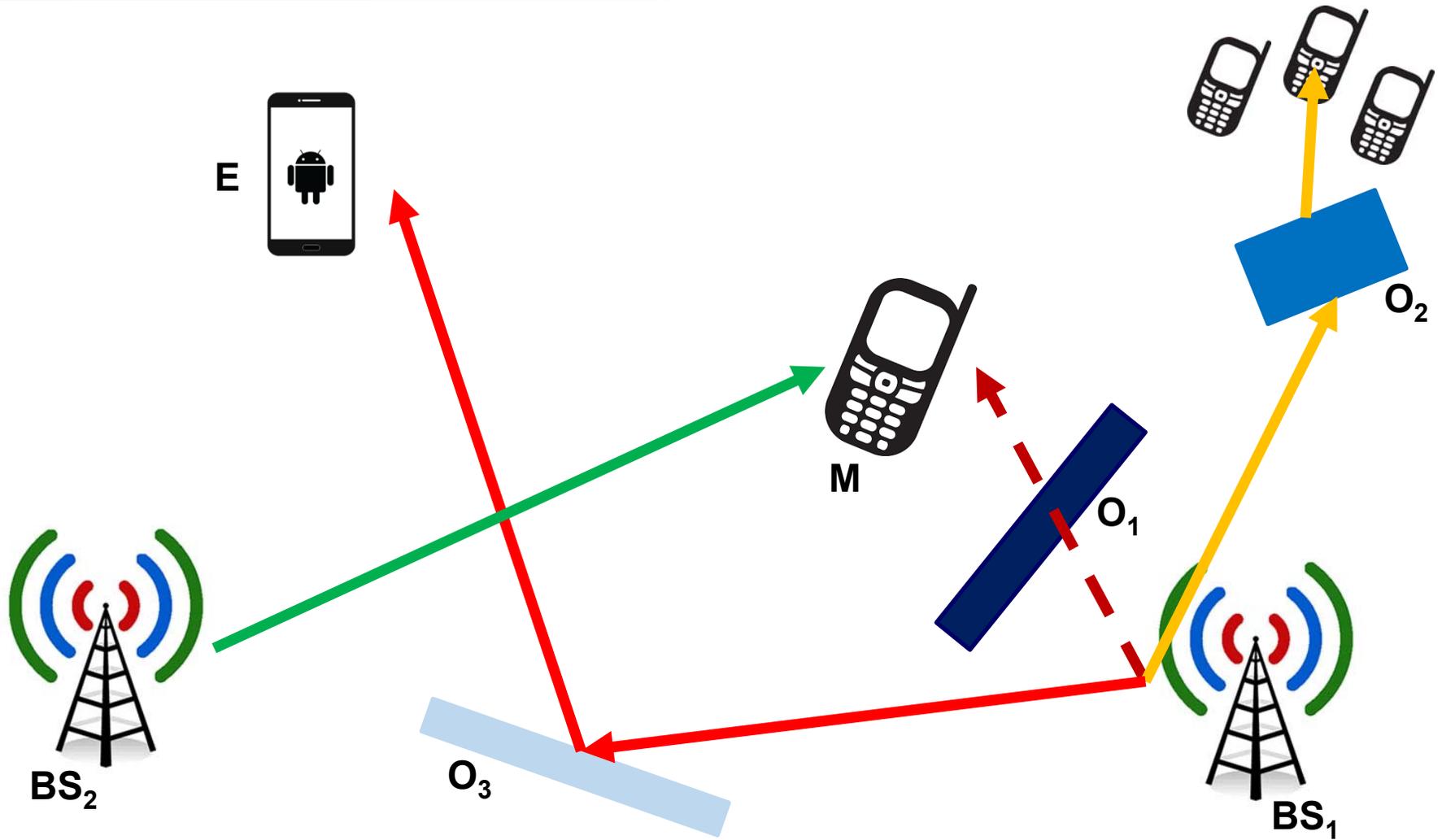
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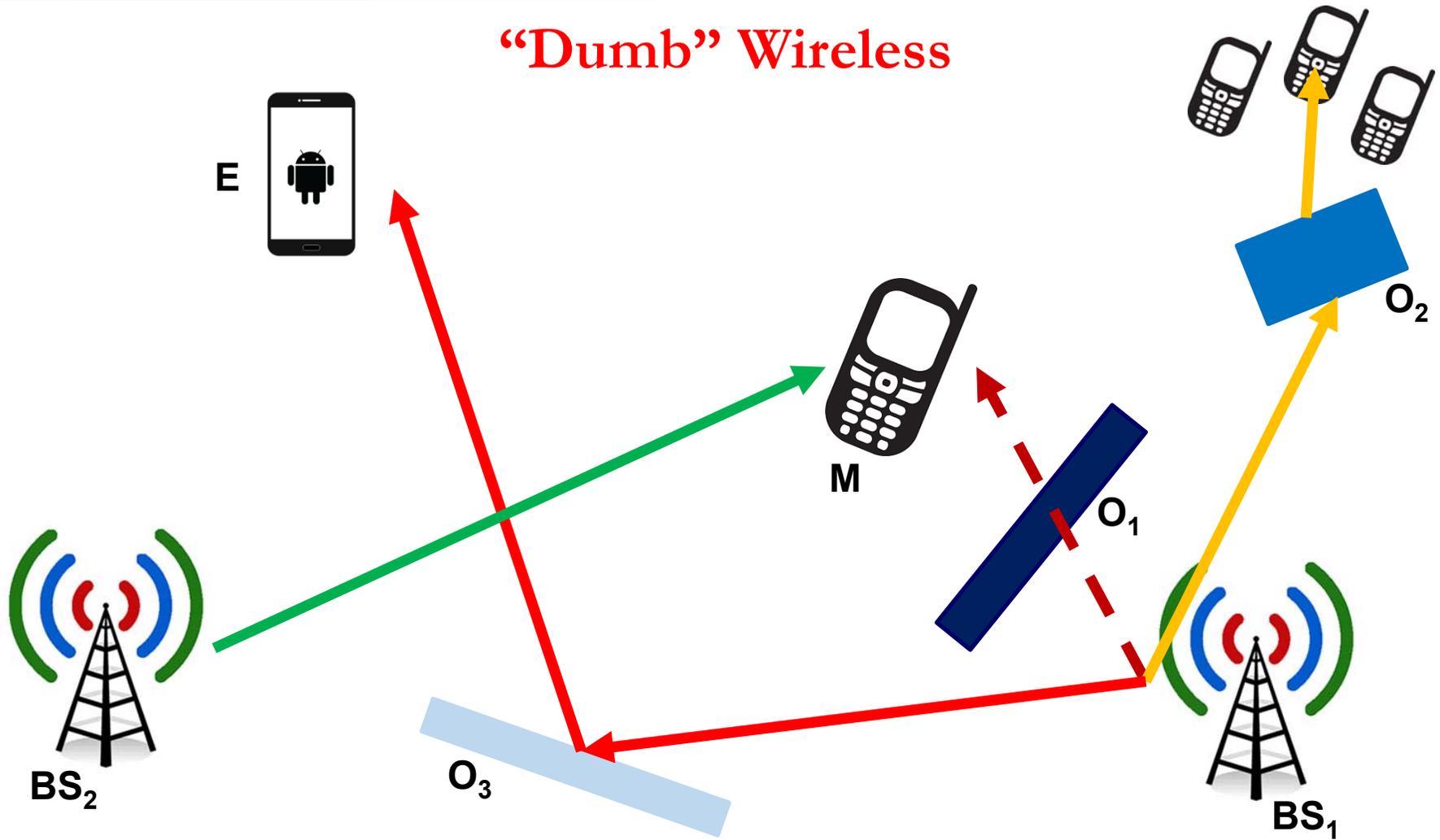


Current Wireless Networks: No Control of Radio Waves



Current Wireless Networks: No Control of Radio Waves

“Dumb” Wireless



Current Wireless Networks: No Control of Radio Waves

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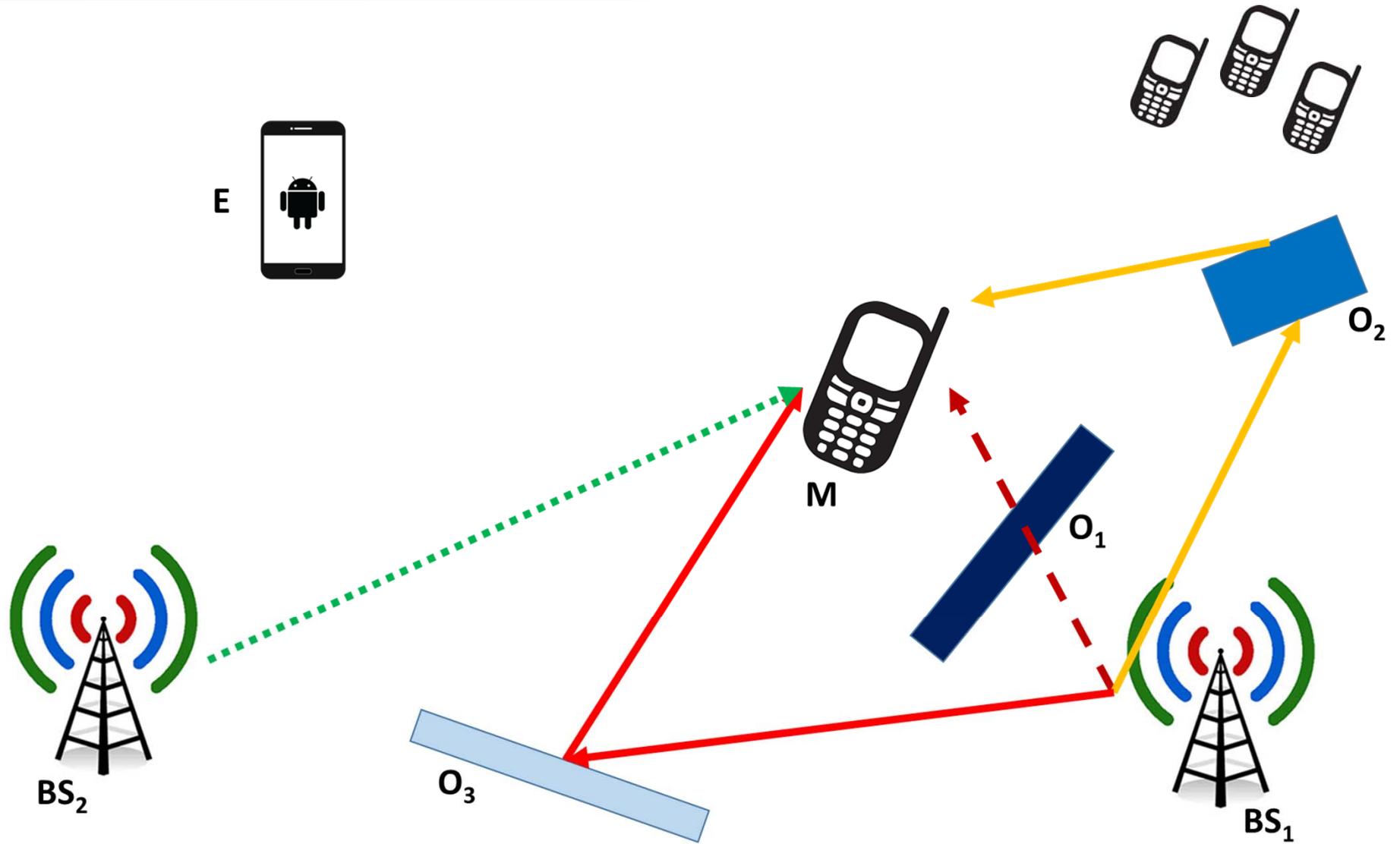
Current Wireless Networks: No Control of Radio Waves

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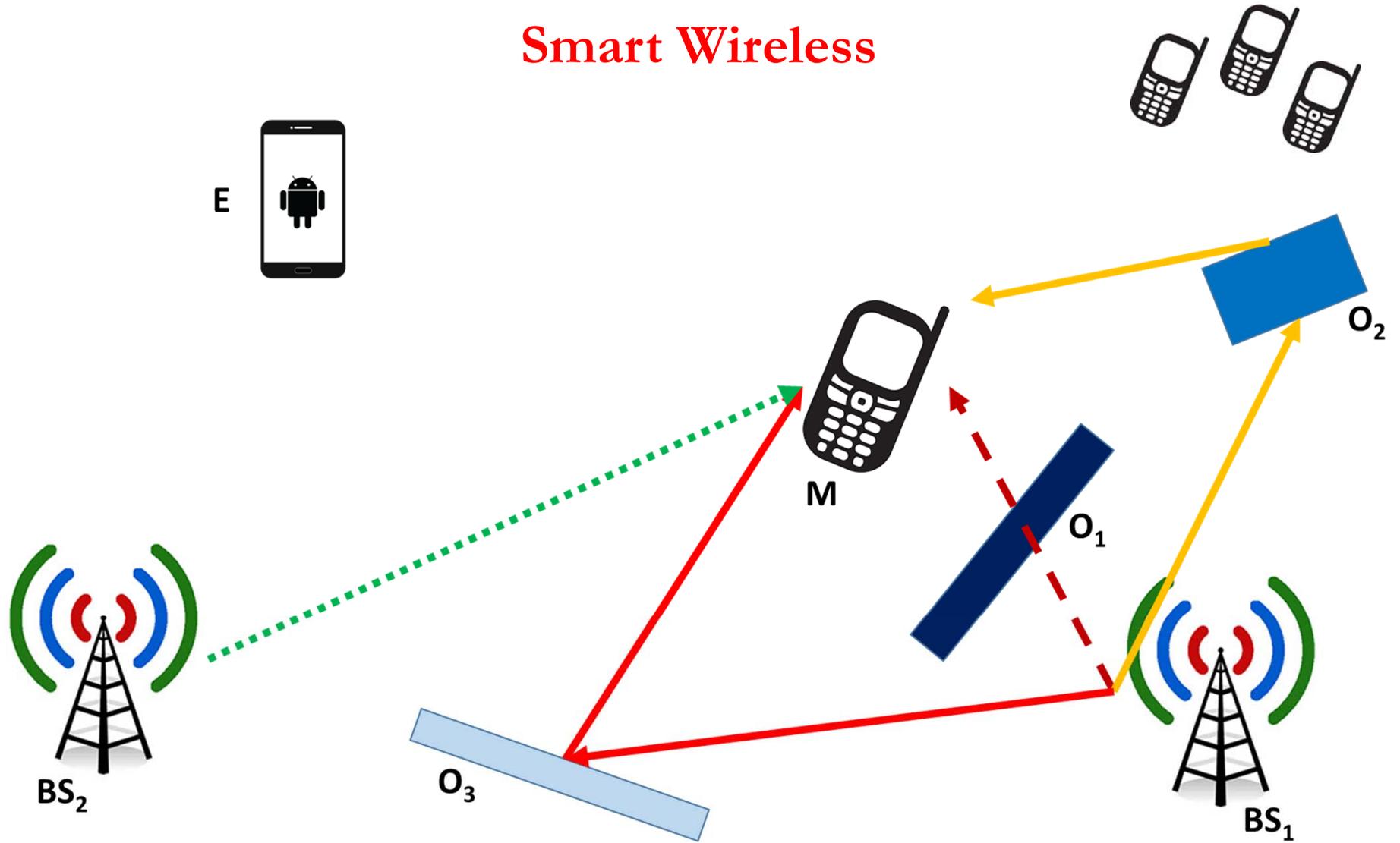
... WHAT IF ...

Smart Radio Environments



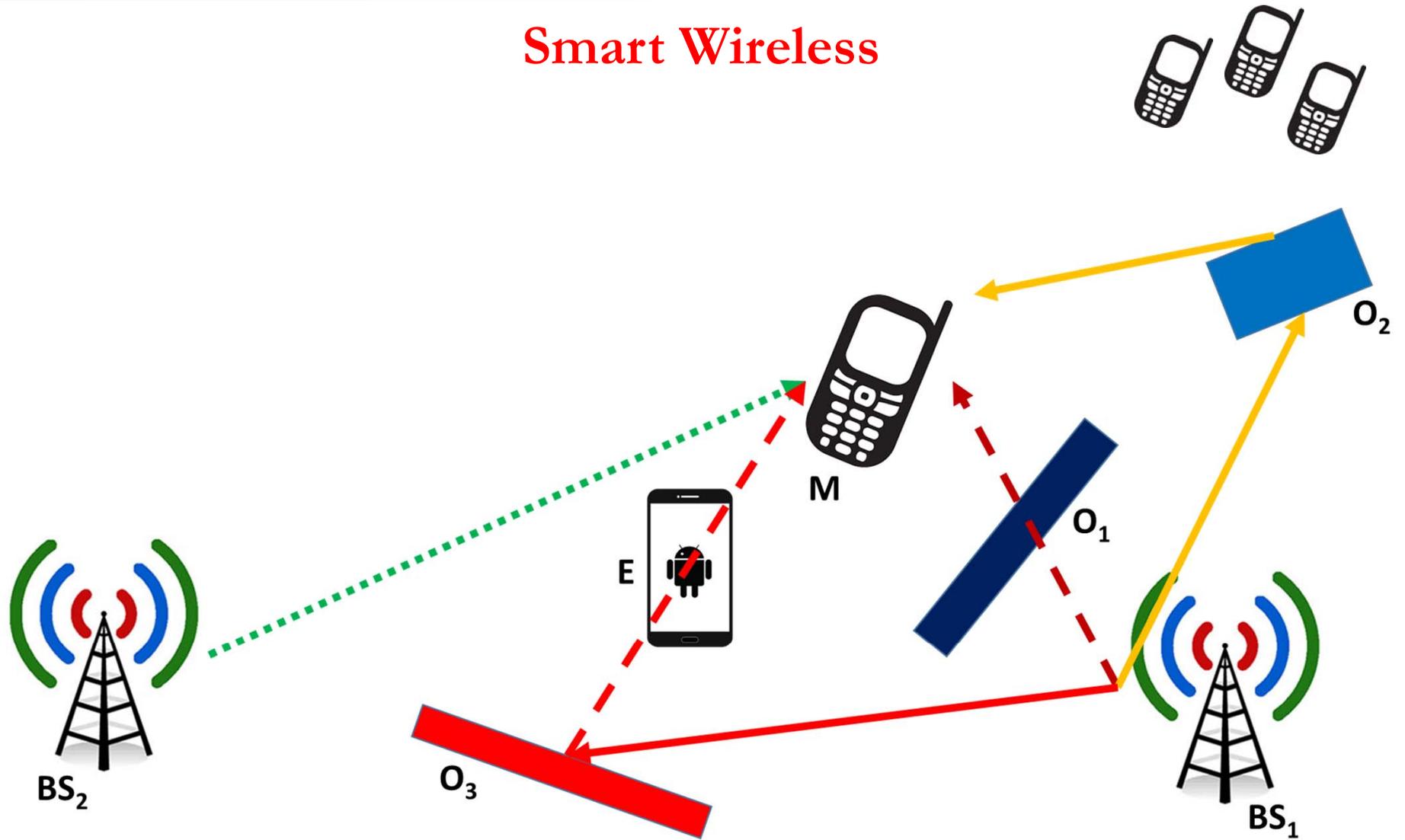
Smart Radio Environments

Smart Wireless



Smart Radio Environments

Smart Wireless



Smart Radio Environments

Smart Wireless

... from adaptation to ...

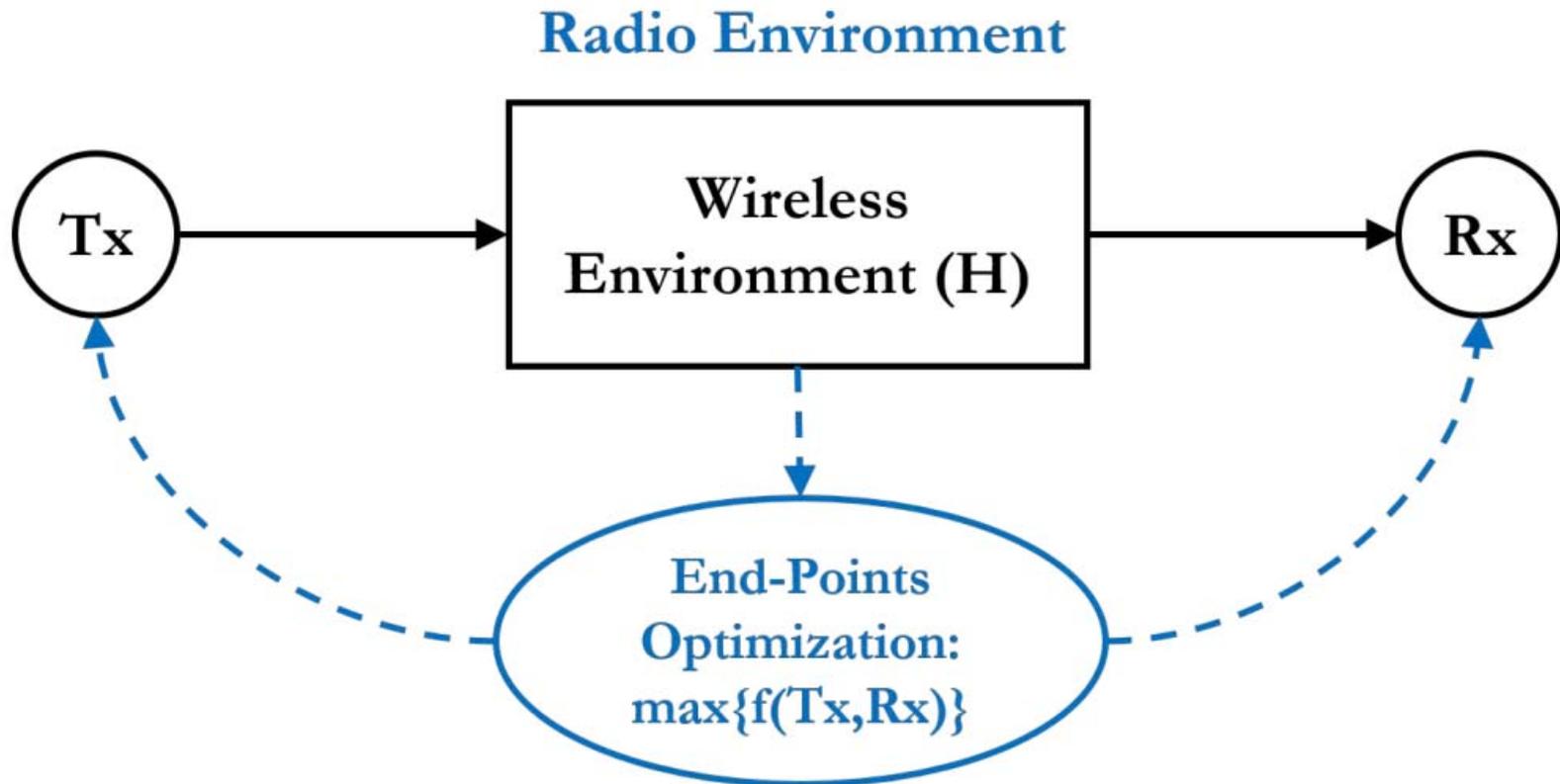
Control & Programmability

Radio Environments

Adaptation: End-Points Optimization

Radio Environments

Adaptation: End-Points Optimization

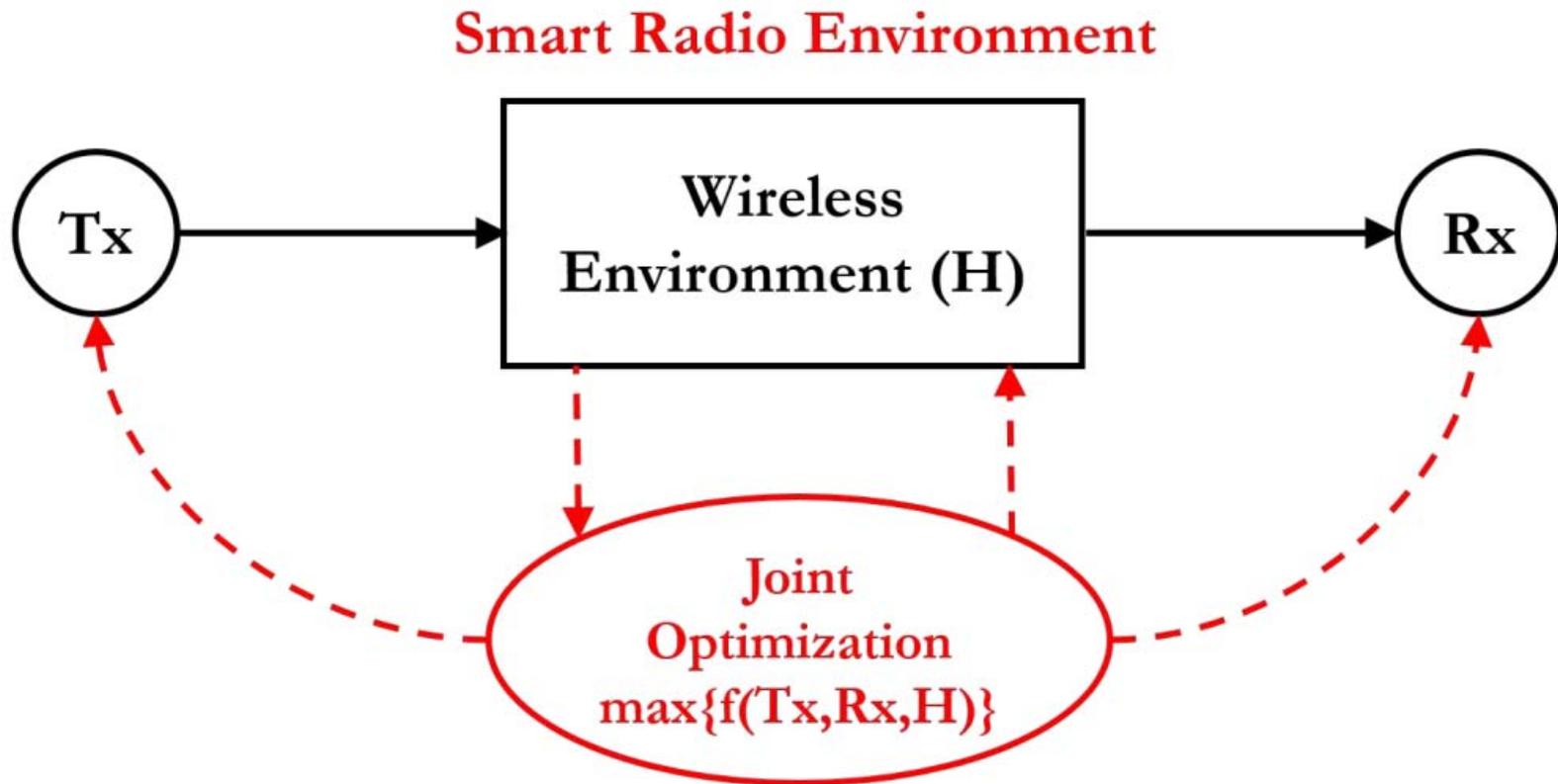


Smart Radio Environments

Control & Programmability: Joint Optimization

Smart Radio Environments

Control & Programmability: Joint Optimization



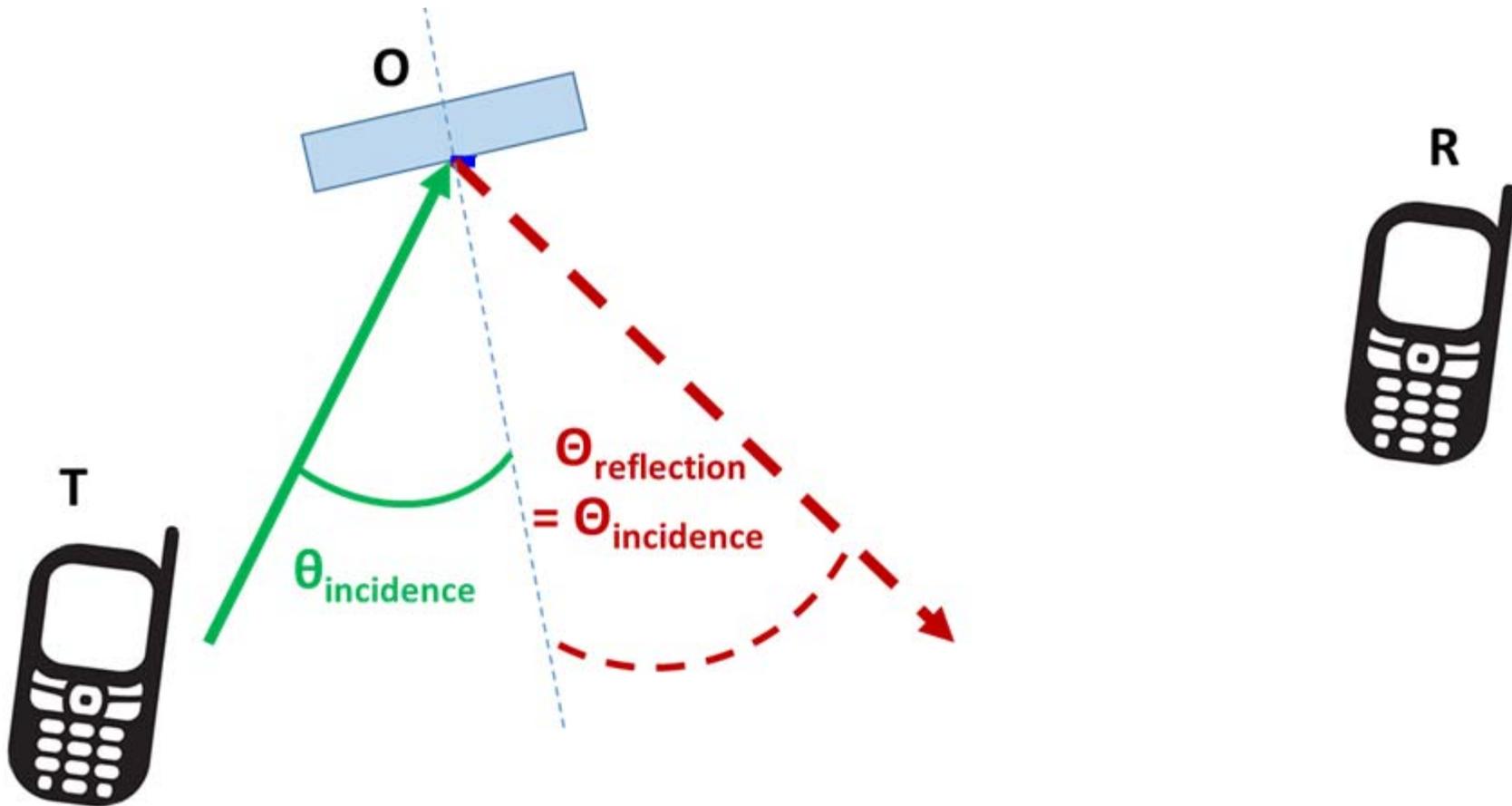
How Can We Design Smart Radio Environments ?

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Reconfigurable Intelligent Surfaces (RISs)

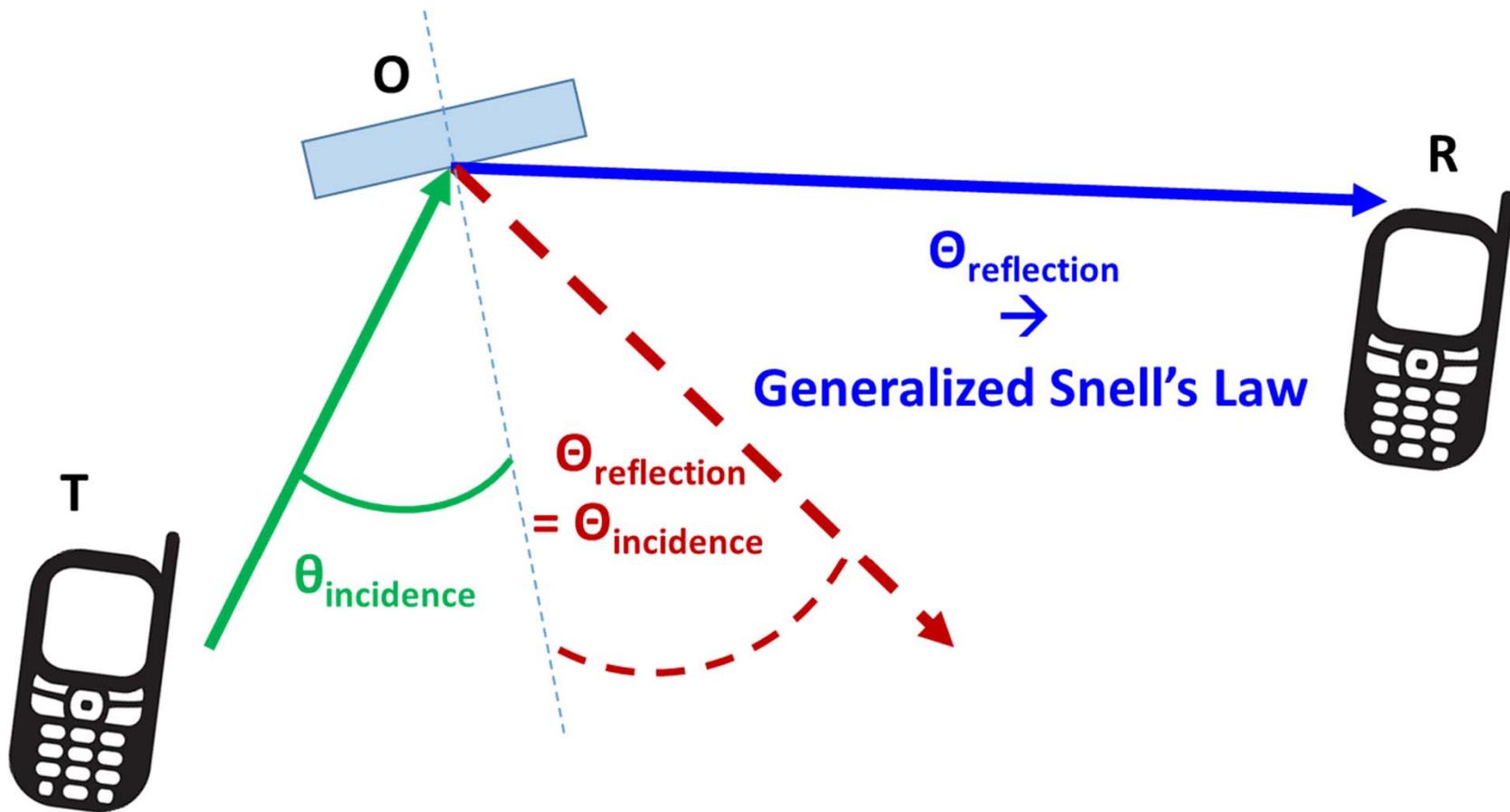
How Can We Design Smart Radio Environments ?

Without an RIS: From Reflections ...



How Can We Design Smart Radio Environments ?

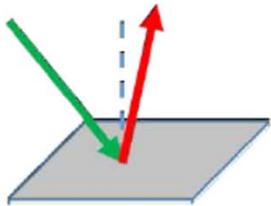
With an RIS: To Smart Reflections ...



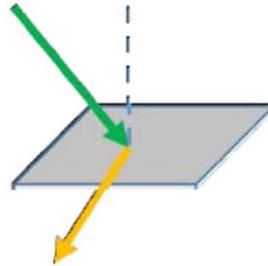
How Can We Design Smart Radio Environments ?

... RISs are more than just “smart reflections” ...

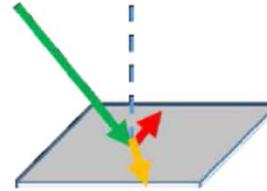
reflection



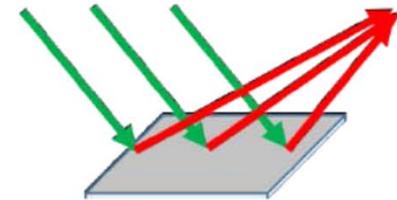
refraction



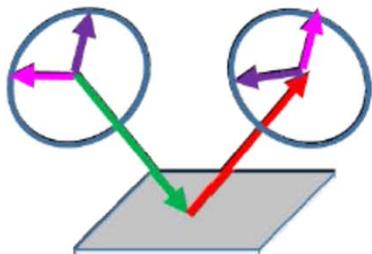
absorption



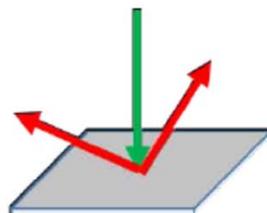
focusing



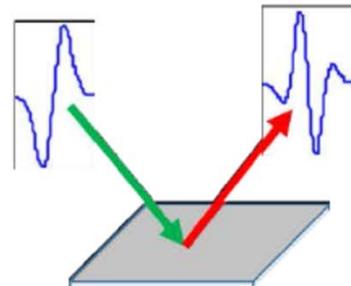
polarization



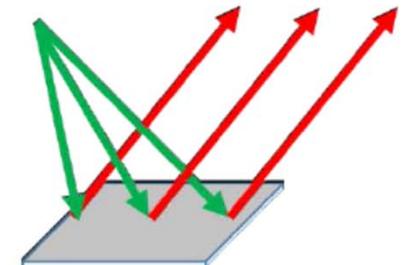
splitting



analog processing



collimation

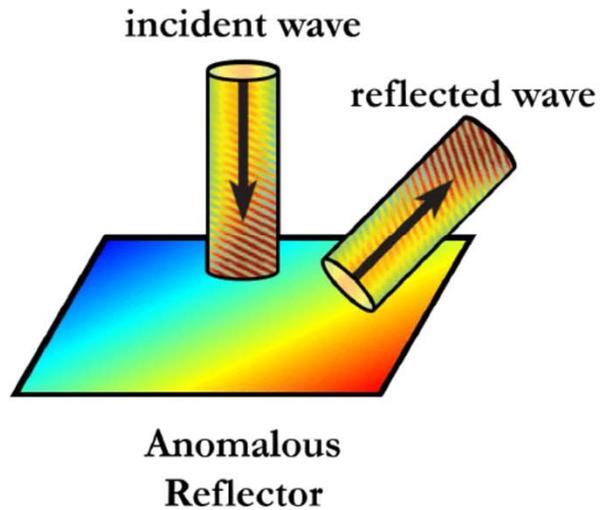


How Can We Design Smart Radio Environments ?

RISs for Wireless Communications

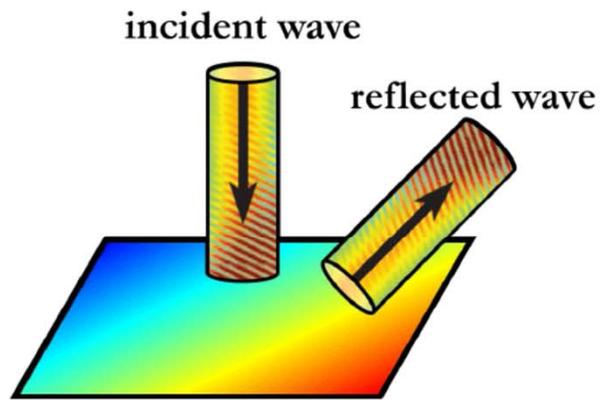
How Can We Design Smart Radio Environments ?

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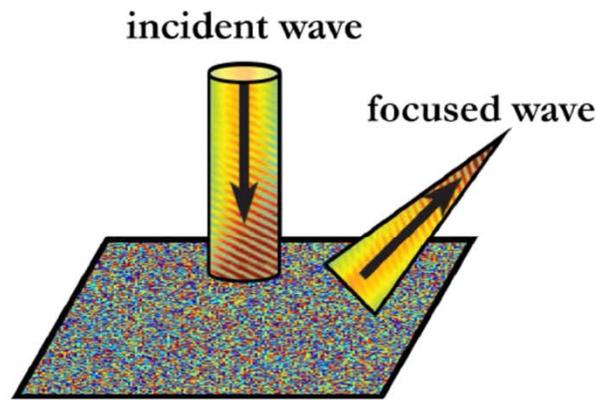


How Can We Design Smart Radio Environments ?

RISs for Wireless Communications



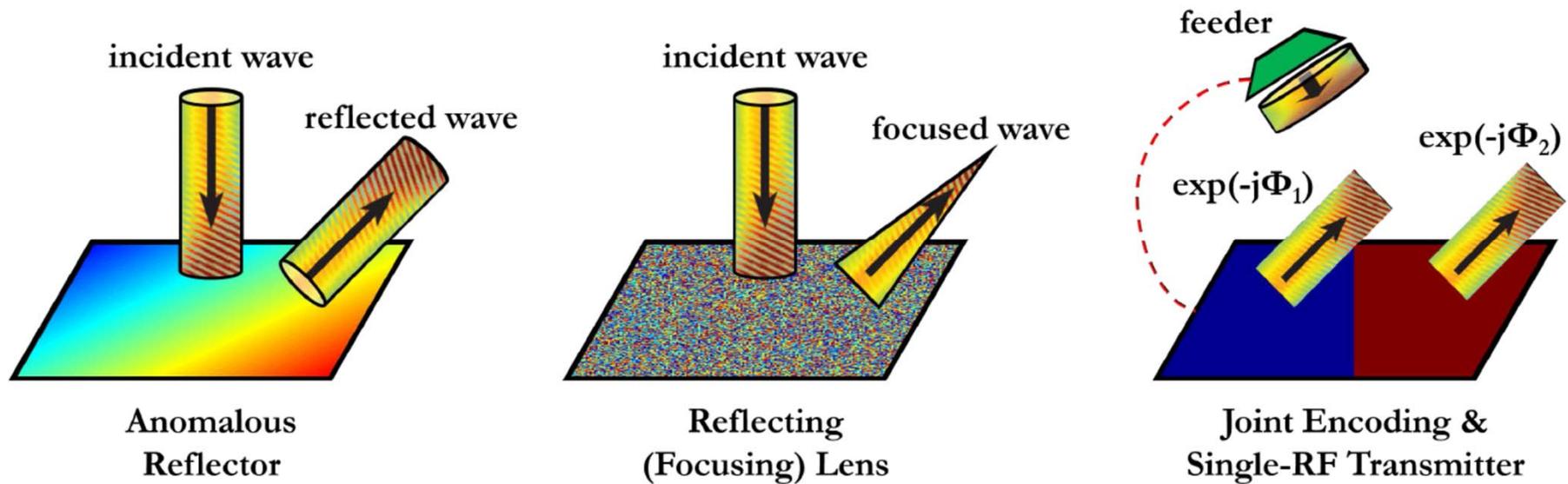
**Anomalous
Reflector**



**Reflecting
(Focusing) Lens**

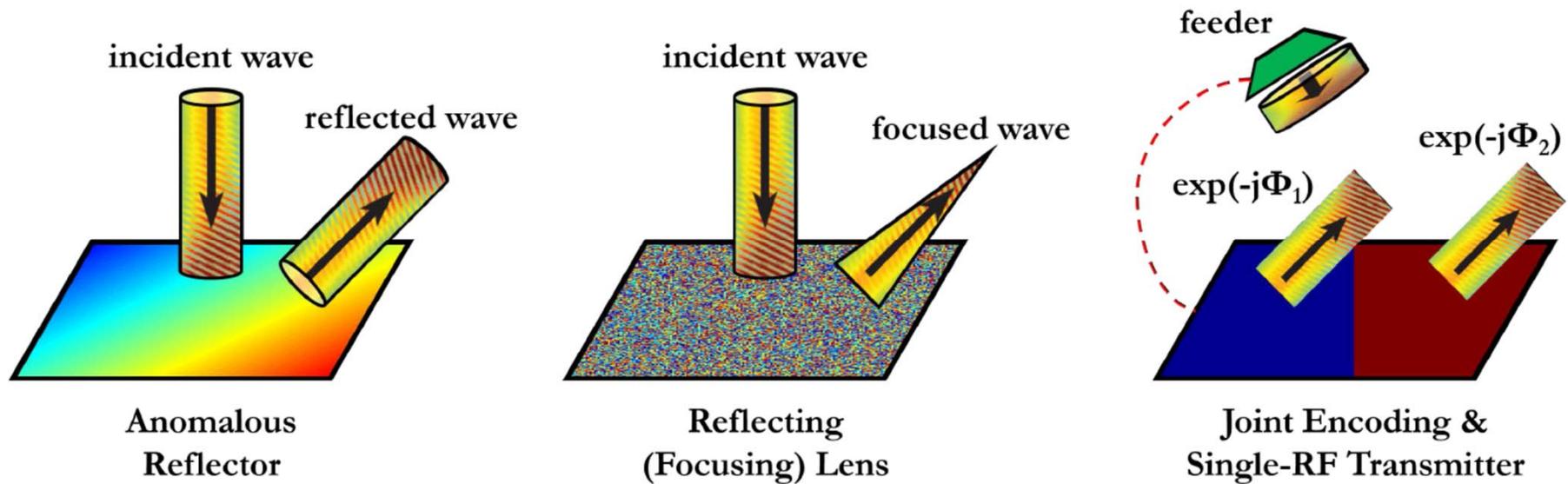
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RISs for Wireless Communications



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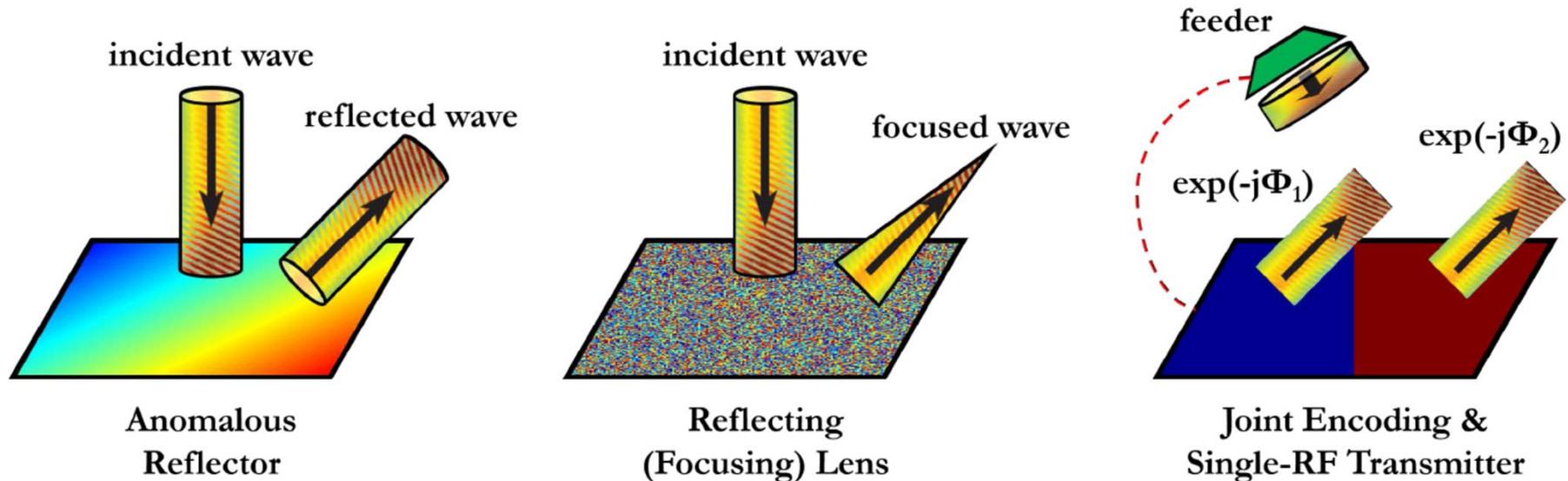
RISs for Wireless Communications



$$E^{(\text{scattered})}(S) \propto E^{(\text{incident})}(S) \left[A(S) \cdot \exp(j\Phi(S)) \right]$$

How Can We Design Smart Radio Environments ?

RISs for Wireless Communications



$$E^{(\text{scattered})}(S) \propto E^{(\text{incident})}(S) \left[A(S) \cdot \exp(j\Phi(S)) \right]$$

\Downarrow

$$E^{(\text{scattered})}(V) \propto \text{Surface Equivalent Theorem} \left\{ E^{(\text{scattered})}(S) \right\}$$

How Can We Design Smart Radio Environments ?

How To Construct an RIS ?

How Can We Design Smart Radio Environments ?

How To Construct an RIS ?

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 - Implementations based on **large arrays of inexpensive antennas** that are usually **spaced half of the wavelength apart**

How Can We Design Smart Radio Environments ?

How To Construct an RIS ?

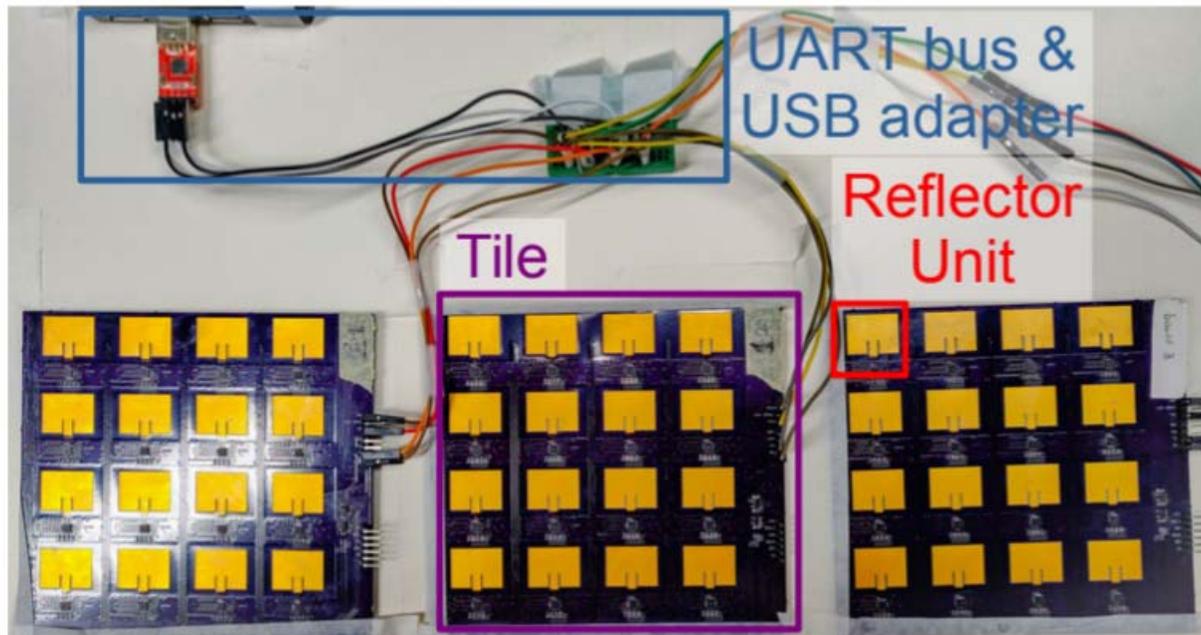
- RISs can be built in different ways, which include:
 - Implementations based on **large arrays of inexpensive antennas** that are usually **spaced half of the wavelength** apart
 - **Metamaterial-based** planar or conformal large surfaces whose **scattering elements** have sizes and inter-distances much **smaller than the wavelength**

How Can We Design Smart Radio Environments ?

RISs: Tiny Antennas Spaced $\sim\lambda/2$

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RISs: Tiny Antennas Spaced $\sim\lambda/2$ (e.g., ScatterMIMO)

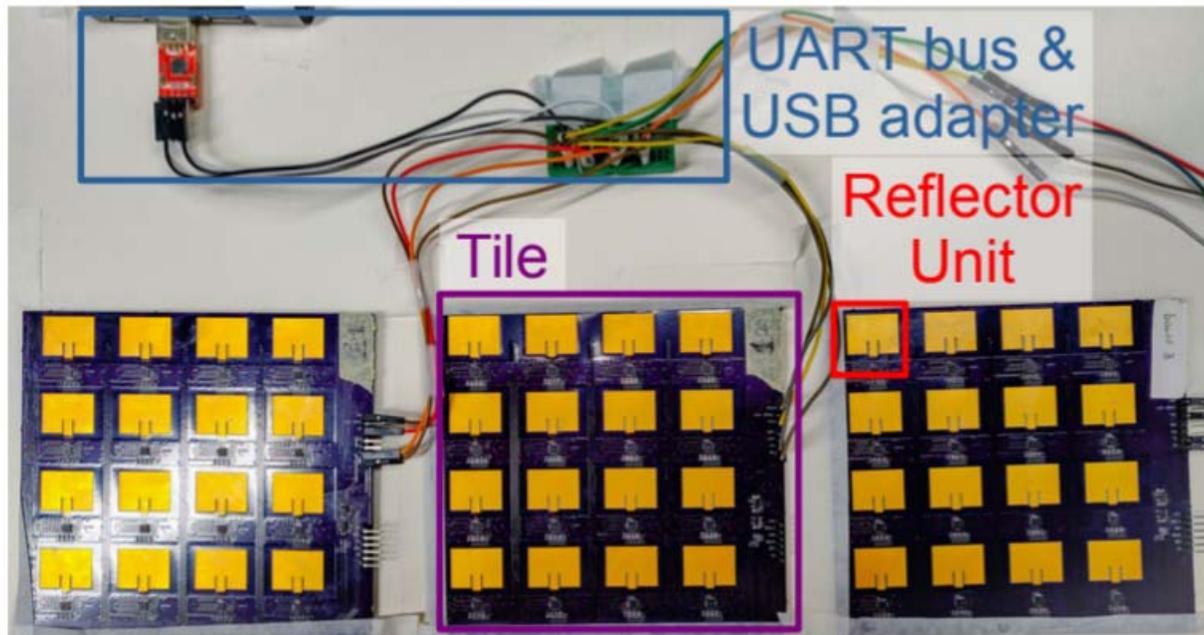


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San Diego
MobiCom 2020

Properties	ScatterMIMO
# antenna elements	48
Algorithm Latency	3 packets
Coverage	upto 45m

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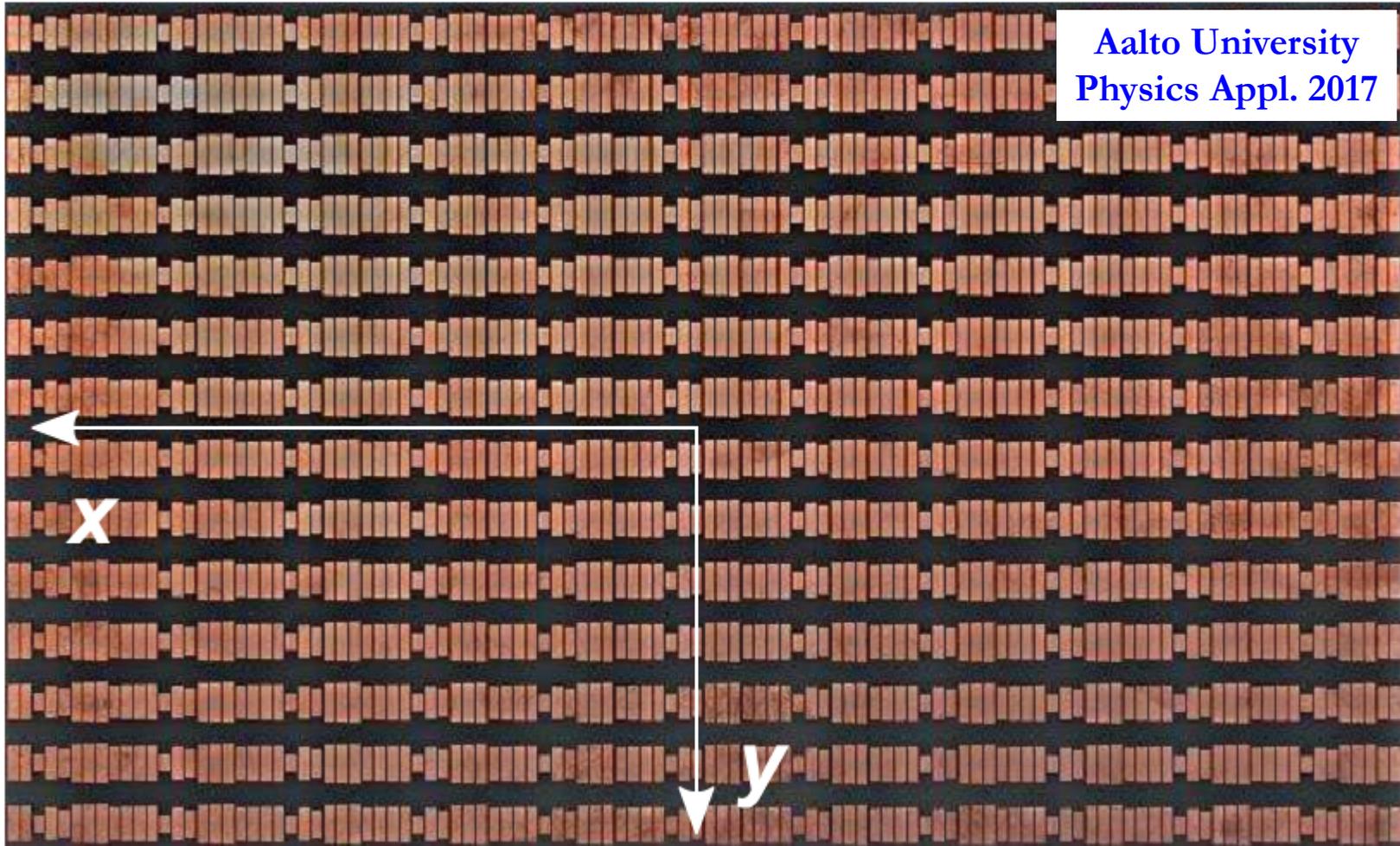
Properties	ScatterMIMO	LAIA [30]	RFocus [9]
# antenna elements	48	36	3720
Algorithm Latency	3 packets	72 packets	4000 packets
Coverage	upto 45m	8 m	30 m

How Can We Design Smart Radio Environments ?

RISs: Metasurfaces Spaced $< \lambda/2$

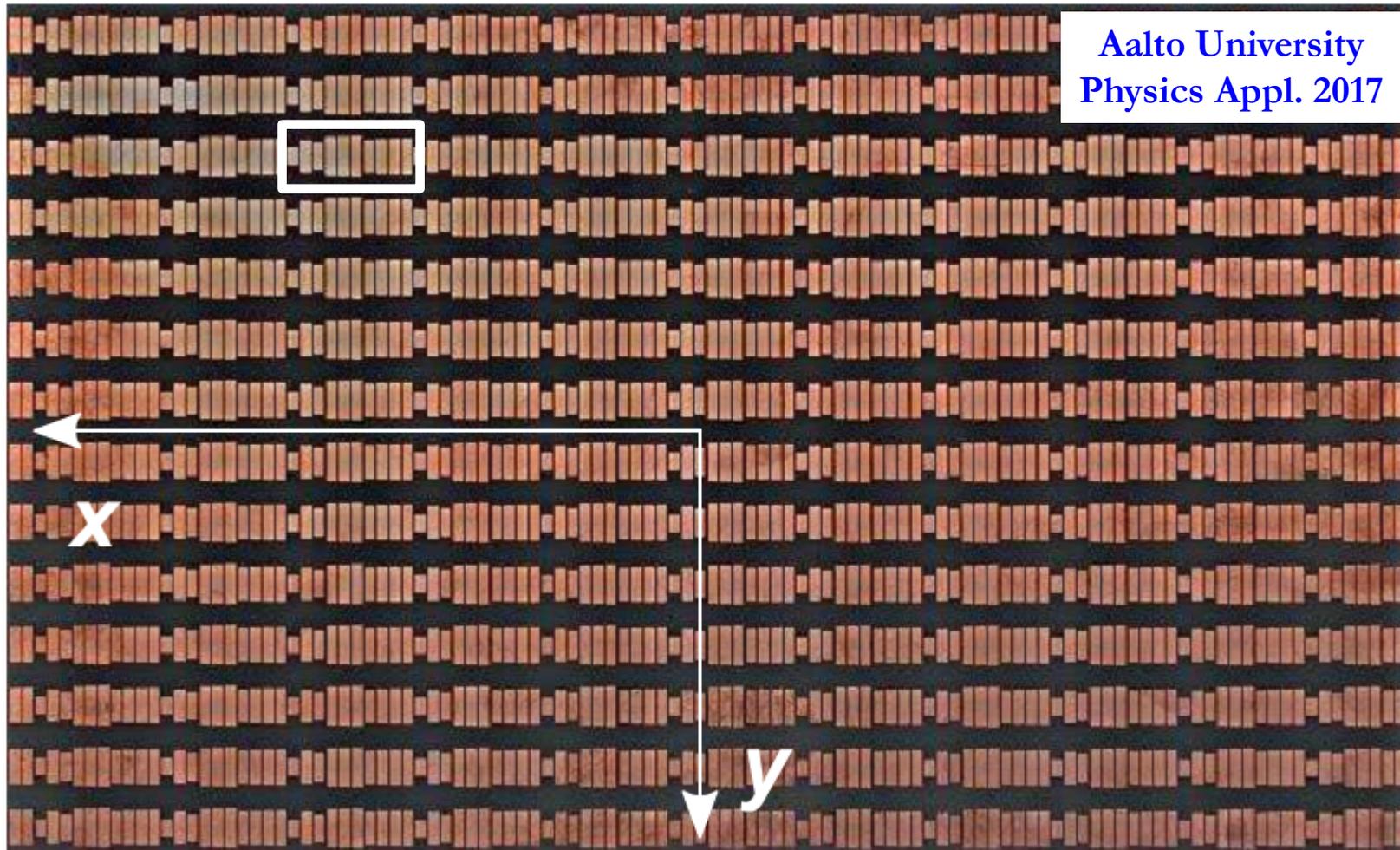
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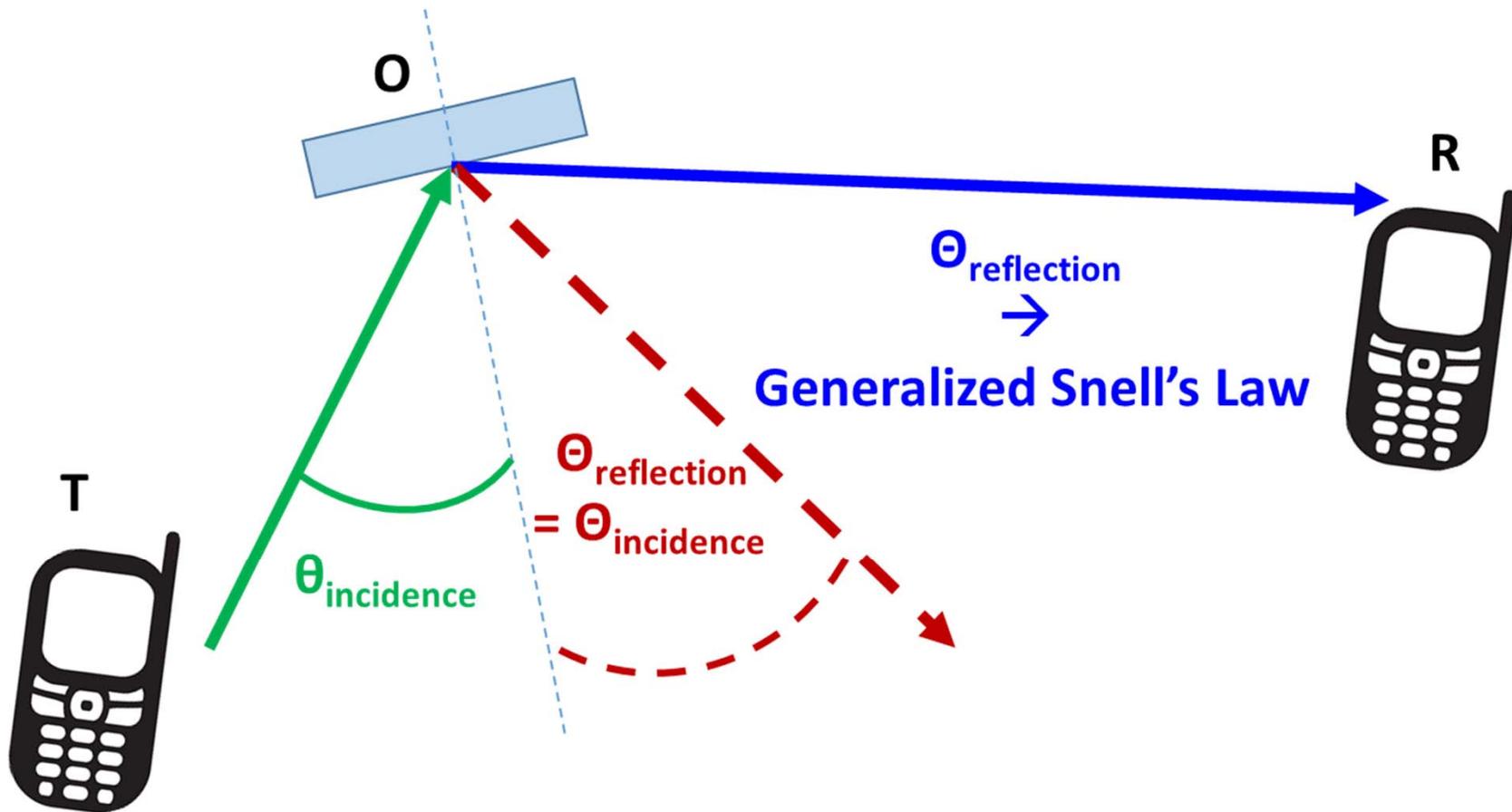


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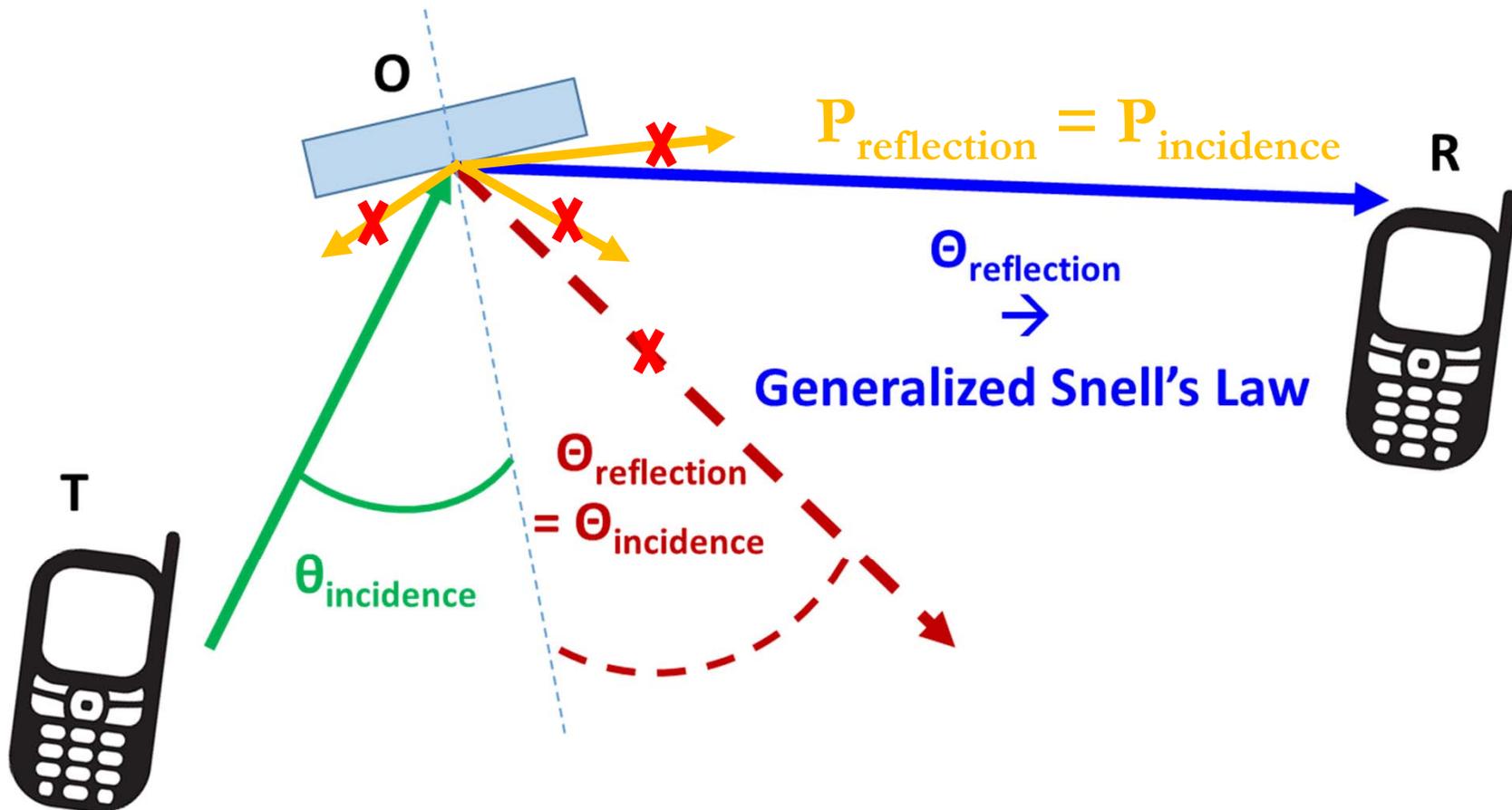
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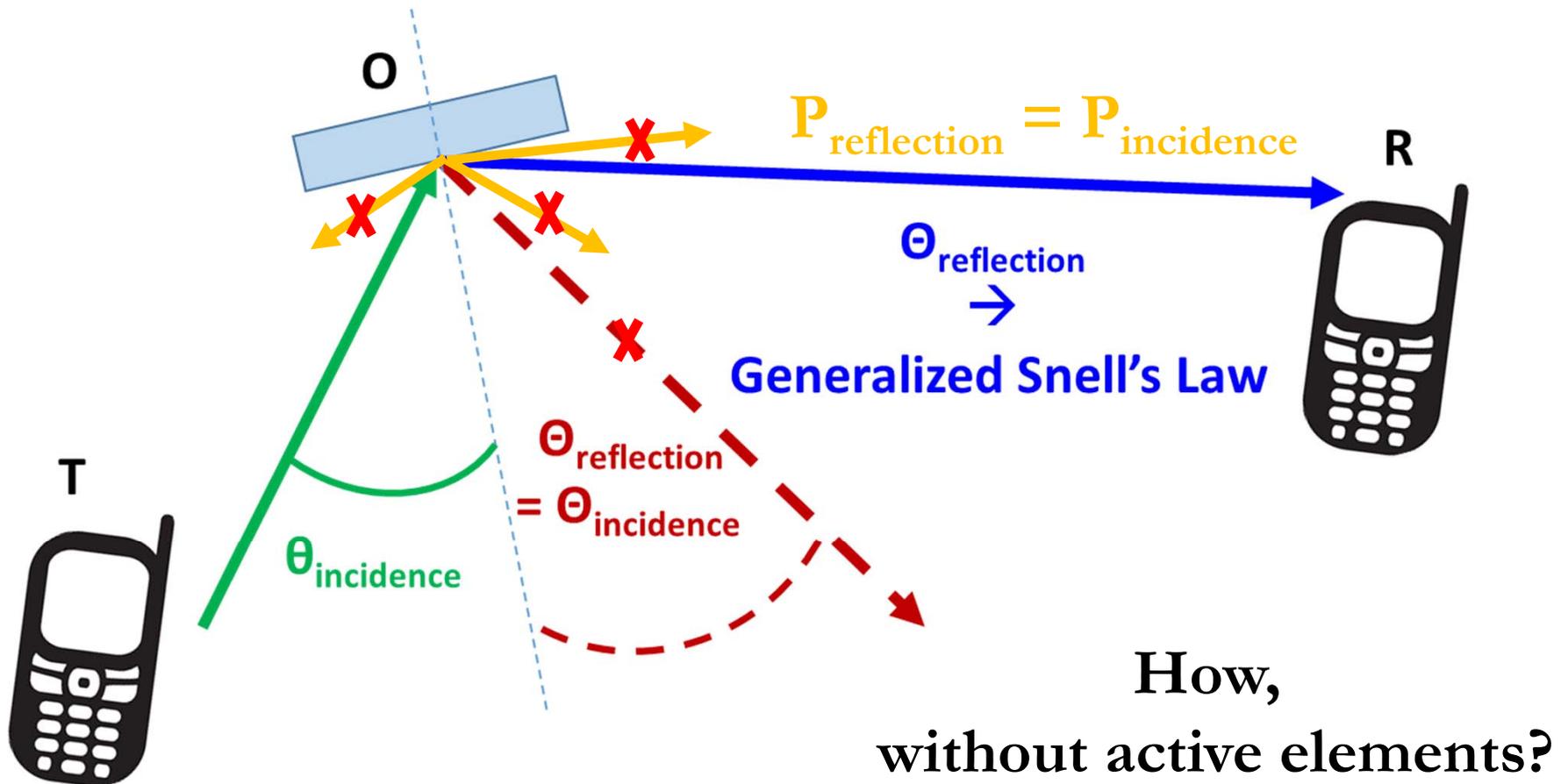
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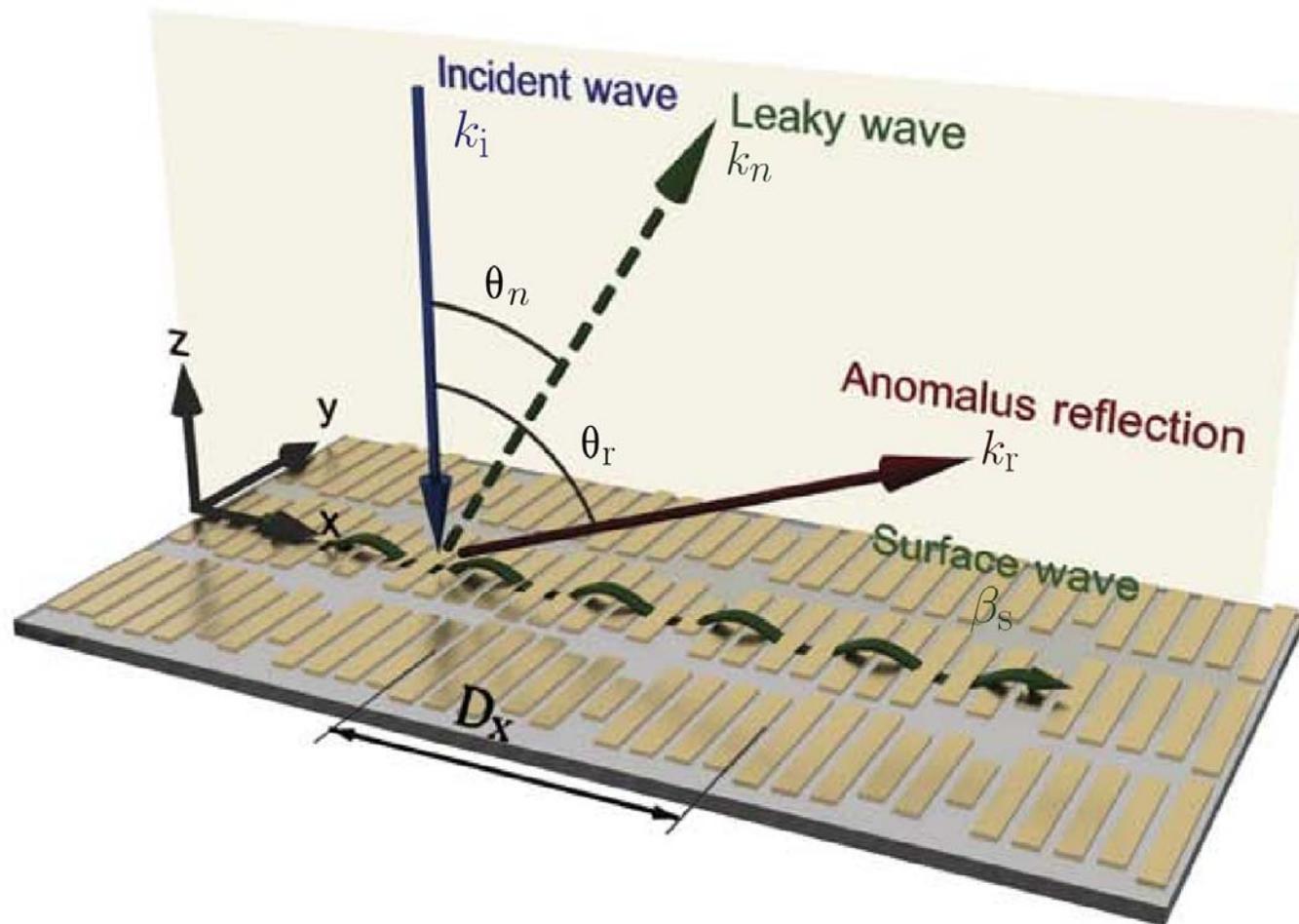
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(e.g., Perfect Anomalous Reflection \rightarrow non-local design)

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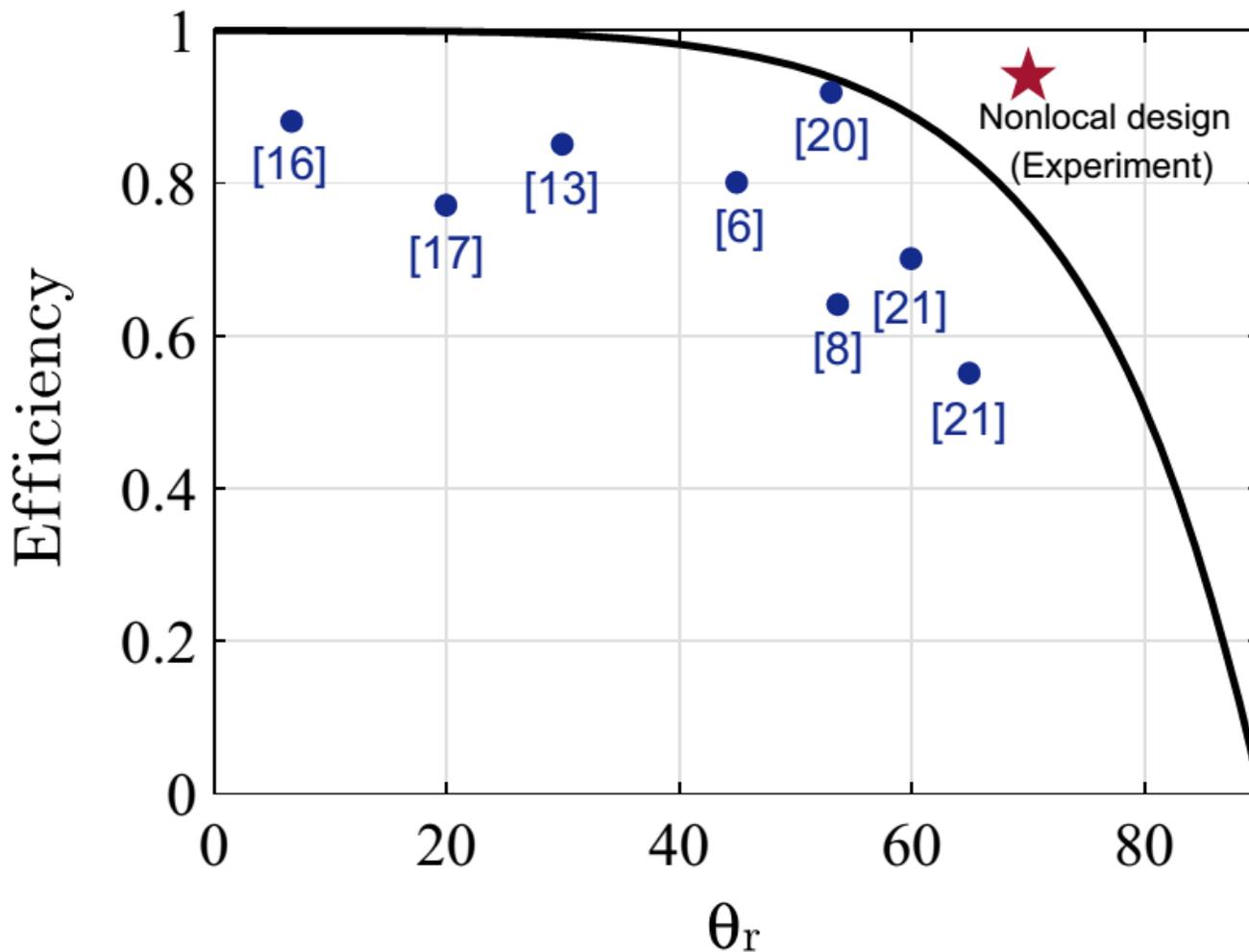
RISs: Metasurfaces Spaced $< \lambda/2$

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How Can We Design Smart Radio Environments ?

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How Can We Design Smart Radio Environments ?

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(local design vs. non-local design)

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How Can We Design Smart Radio Environments ?

RISs: Metasurfaces Spaced $< \lambda/2$
(local design vs. non-local design)

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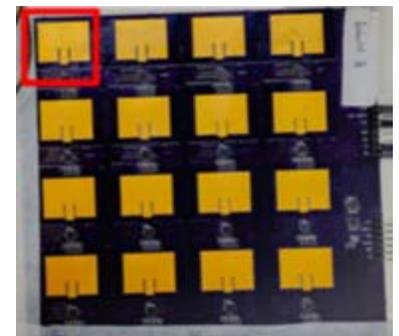
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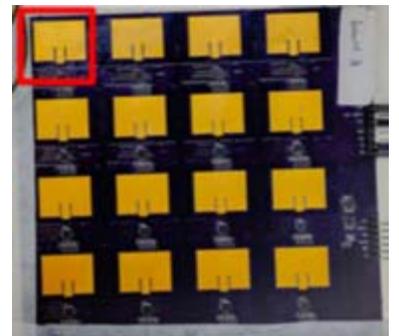
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locally passive implementation

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How Can We Design Smart Radio Environments ?

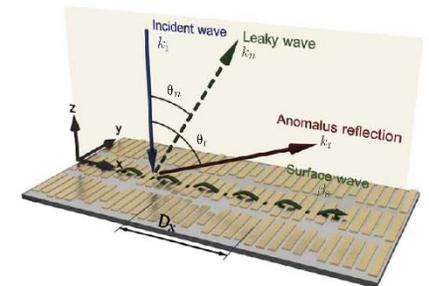
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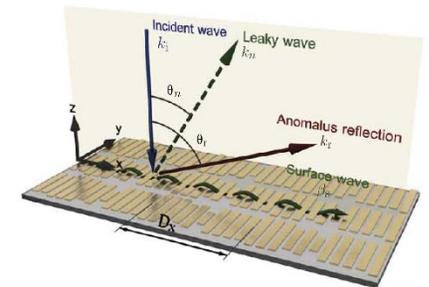
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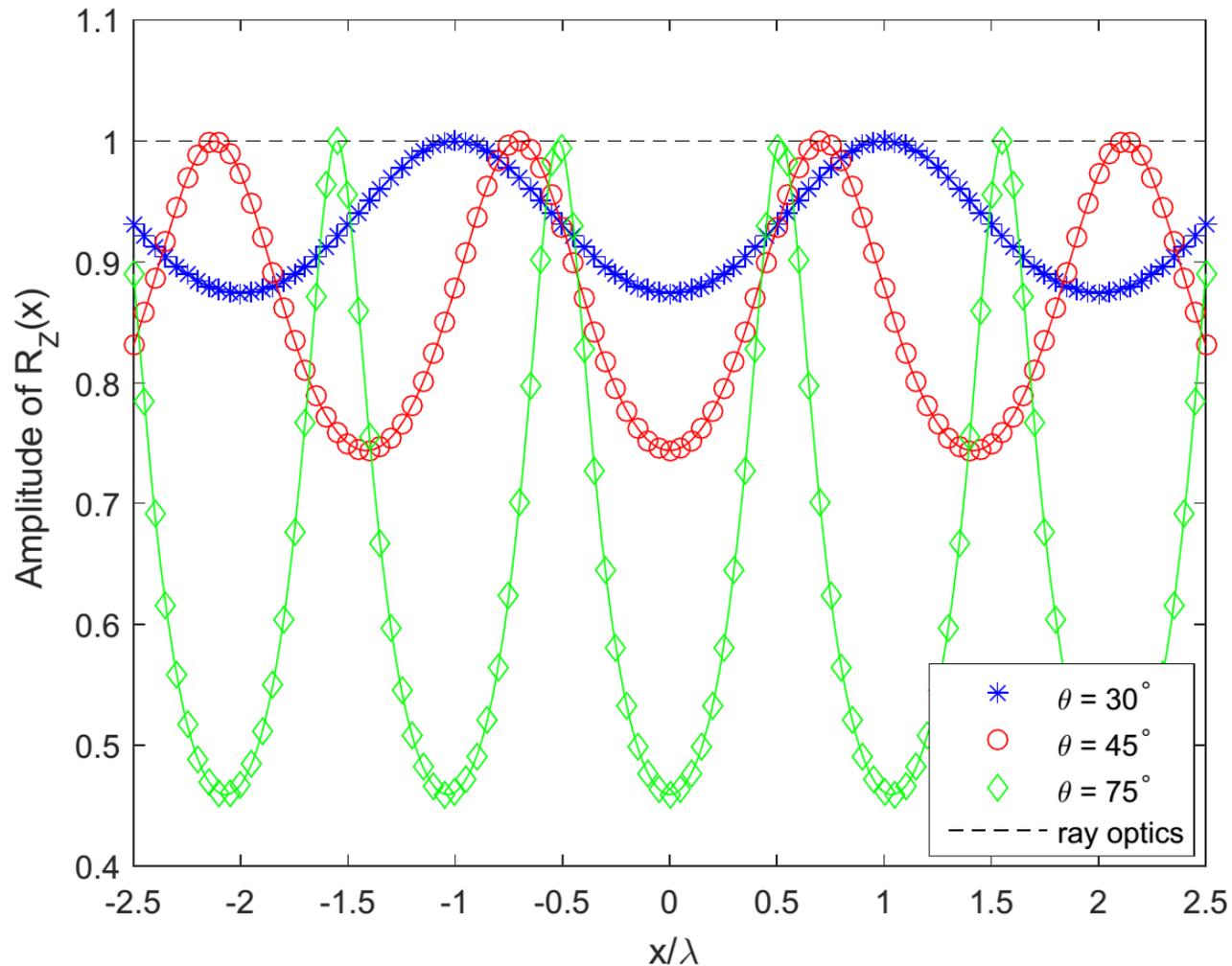
globally passive implementation

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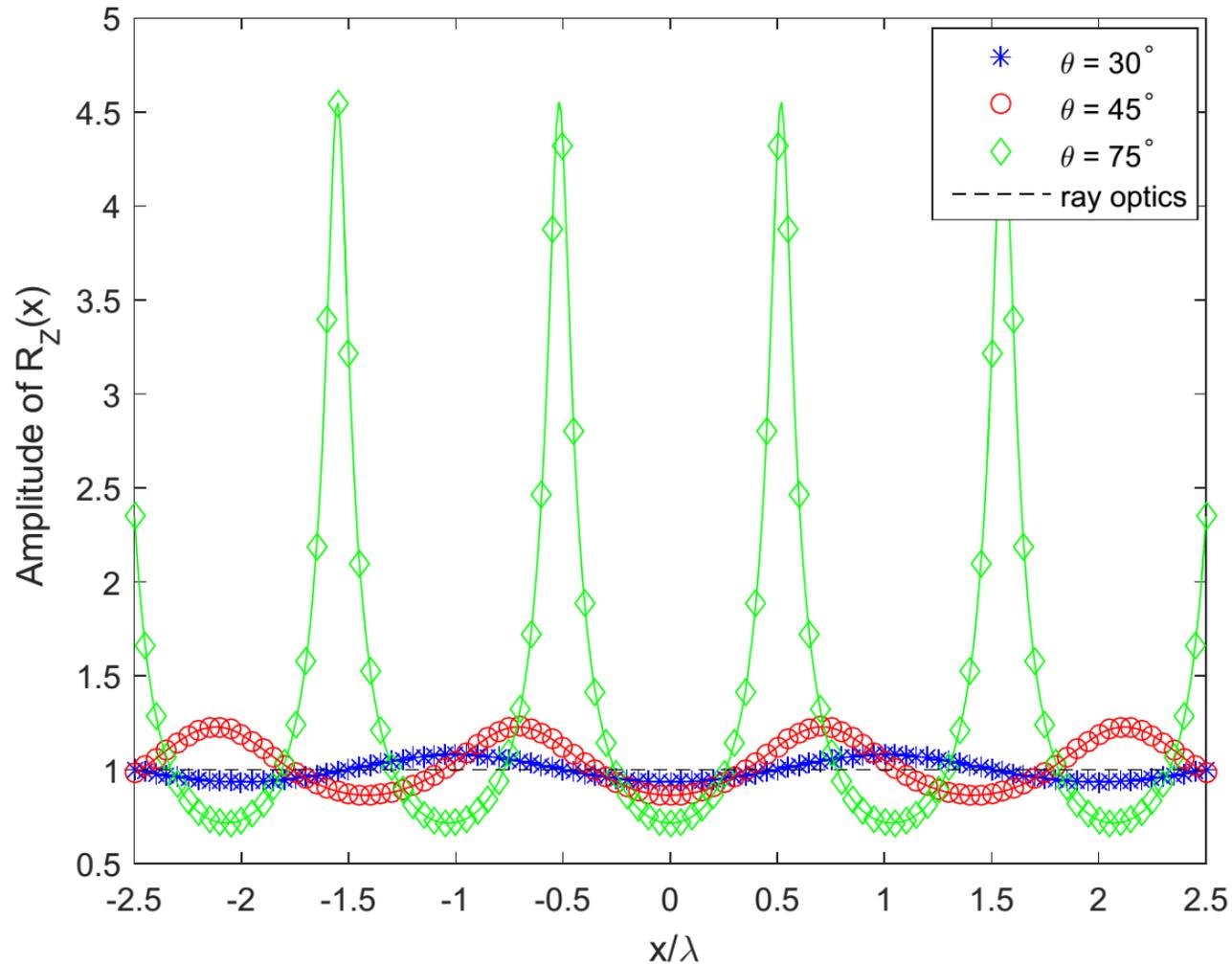


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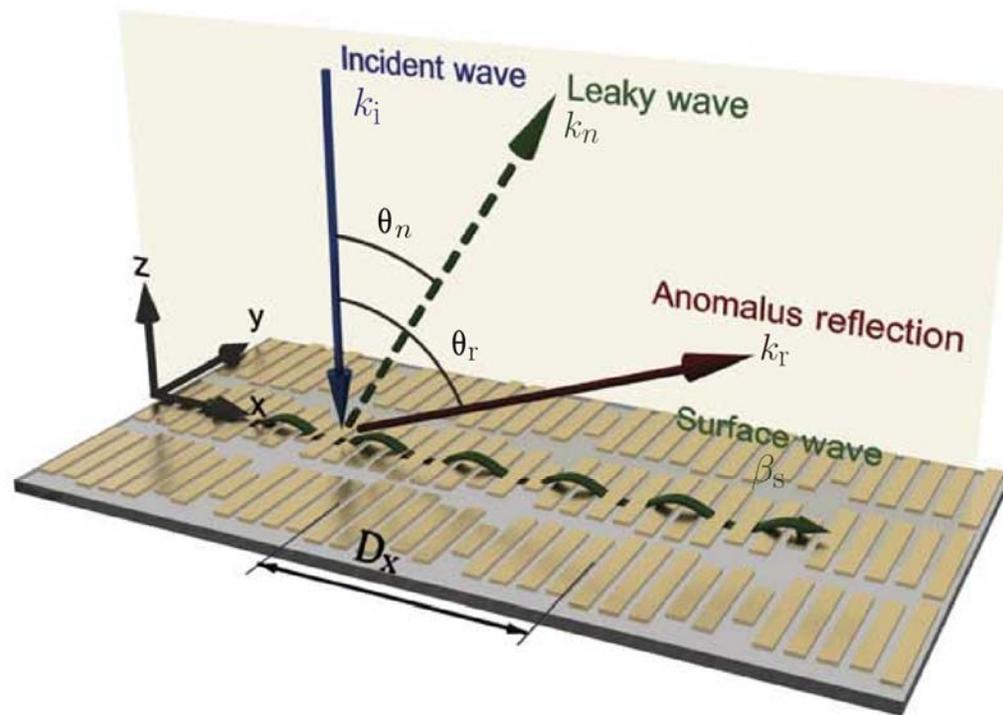
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(local design vs. non-local design)



How Can We Design Smart Radio Environments ?

RISs: Metasurfaces Spaced $< \lambda/2$

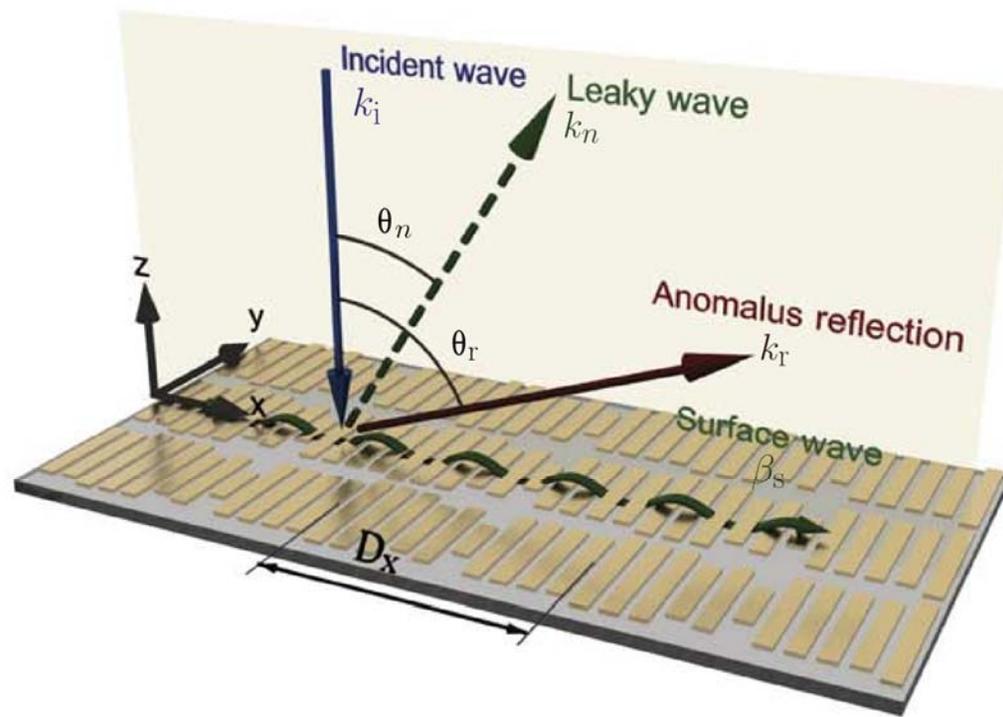
(e.g., Perfect Anomalous Reflection \rightarrow non-local design)



How Can We Design Smart Radio Environments ?

RISs: Metasurfaces Spaced $< \lambda/2$

(e.g., Perfect Anomalous Reflection \rightarrow non-local design)

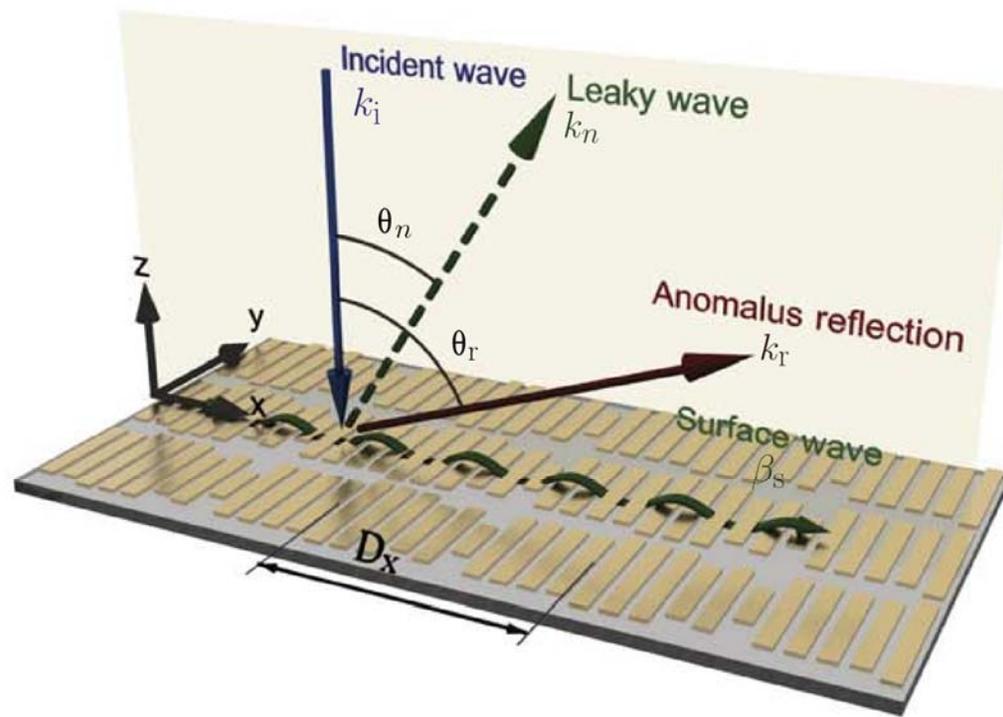


$$P^{(\text{reflected})} - P^{(\text{incident})} \geq 0 \quad \text{but} \quad \int_{\text{Surface}} \left(P^{(\text{reflected})} - P^{(\text{incident})} \right) \leq 0$$

How Can We Design Smart Radio Environments ?

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$$P^{(\text{reflected})} - P^{(\text{incident})} \geq 0 \quad \text{but} \quad \int_{\text{Surface}} \left(P^{(\text{reflected})} - P^{(\text{incident})} \right) \leq 0$$

without using active elements \rightarrow surface waves

How Can We Design Smart Radio Environments ?

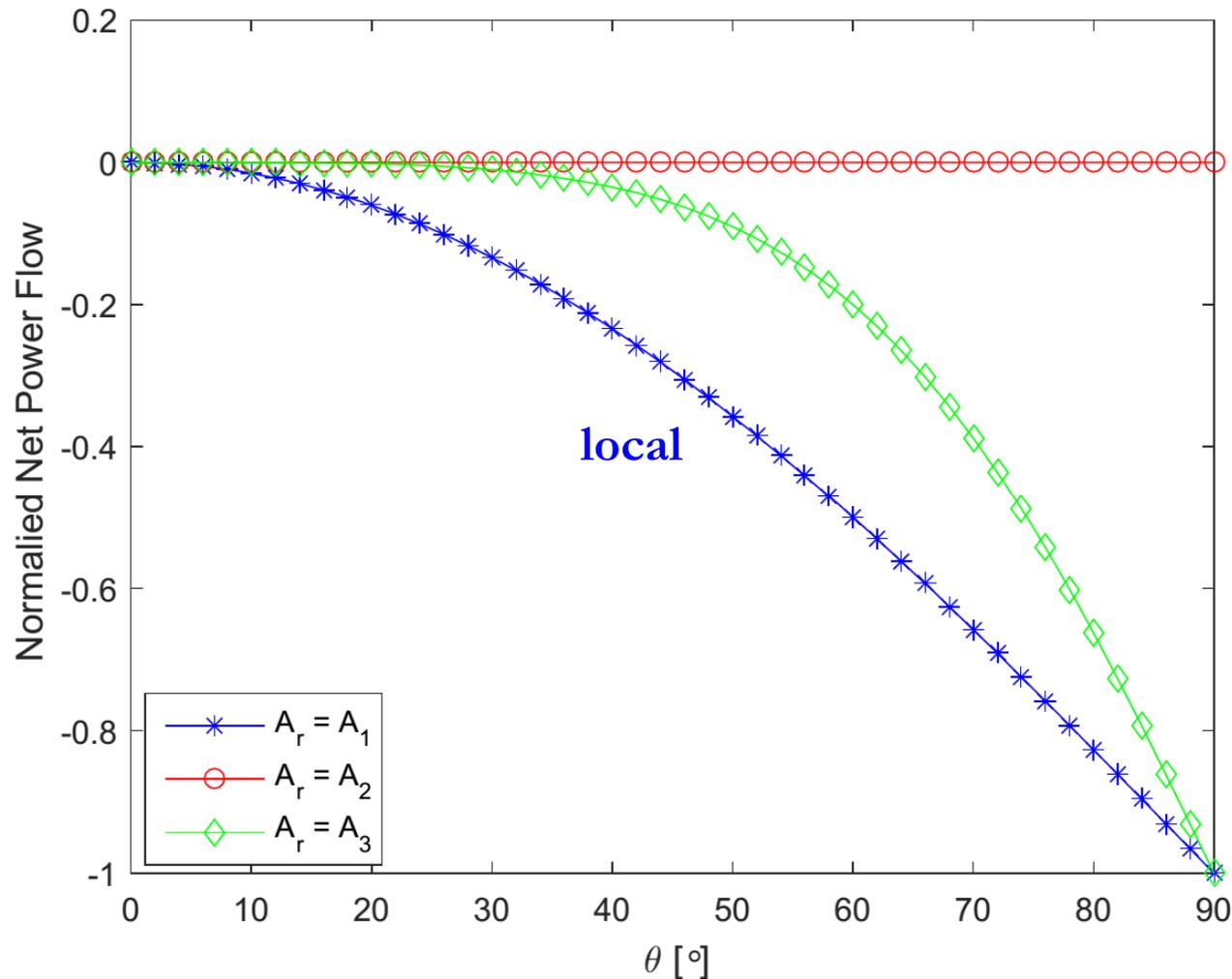
RISs: Metasurfaces Spaced $< \lambda/2$

(local design vs. non-local design: Net Power Flow)

How Can We Design Smart Radio Environments ?

RISs: Metasurfaces Spaced $< \lambda/2$

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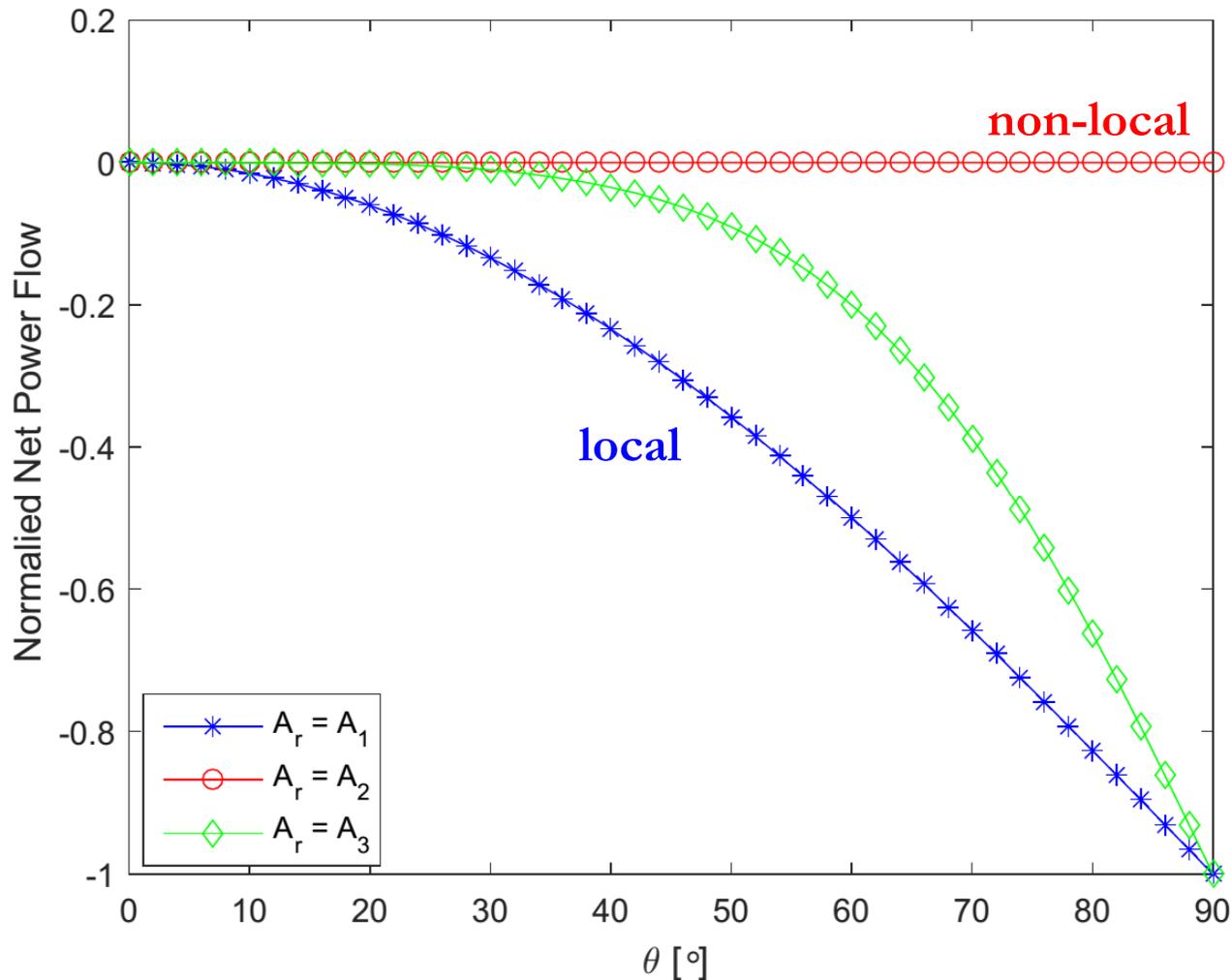


$$A(\theta^{(\text{incident})}, \theta^{(\text{reflected})}) = 1$$

How Can We Design Smart Radio Environments ?

RISs: Metasurfaces Spaced $< \lambda/2$

(local design vs. non-local design: Net Power Flow)



$$A(\theta^{(\text{incident})}, \theta^{(\text{reflected})}) = 1$$

$$A(\theta^{(\text{incident})}, \theta^{(\text{reflected})}) = \sqrt{\frac{\cos(\theta^{(\text{incident})})}{\cos(\theta^{(\text{reflected})})}}$$

How Can We Design Smart Radio Environments ?

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(local design vs. non-local design)

How Can We Design Smart Radio Environments ?

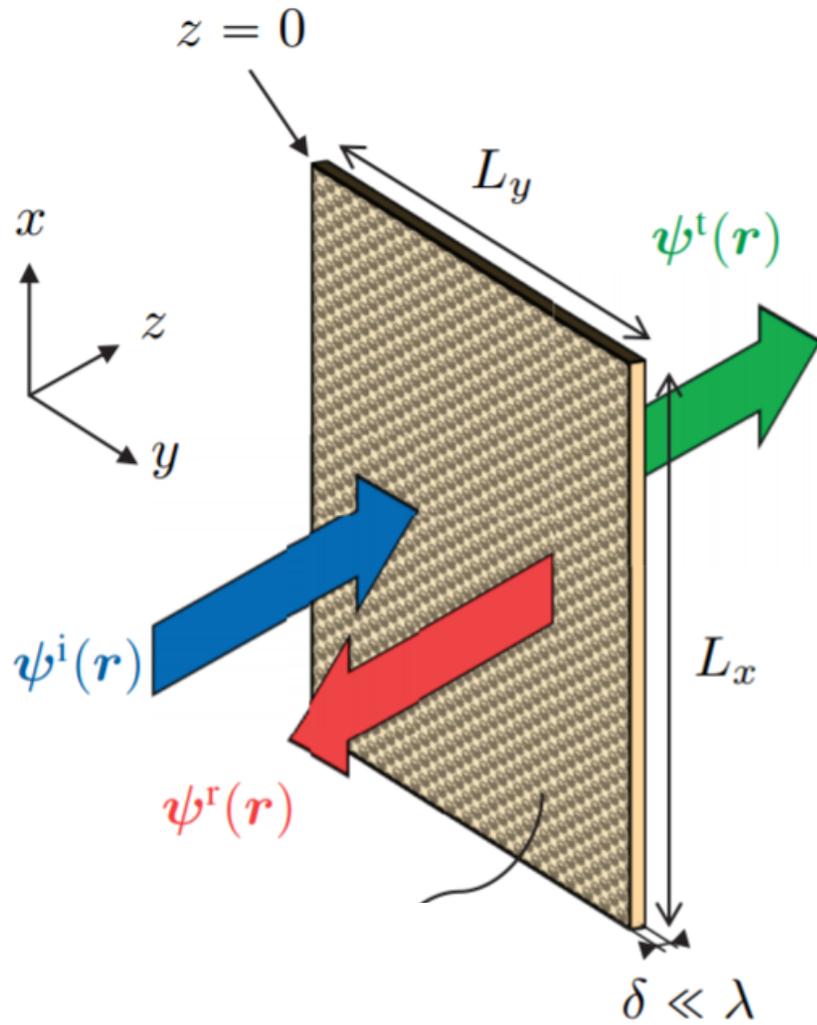
RISs: Metasurfaces Spaced $< \lambda/2$
(local design vs. non-local design)

A non-local design allows one to realize

Globally Passive Structures
(with) High Power Efficiency
(for) Large Angles of Reflection

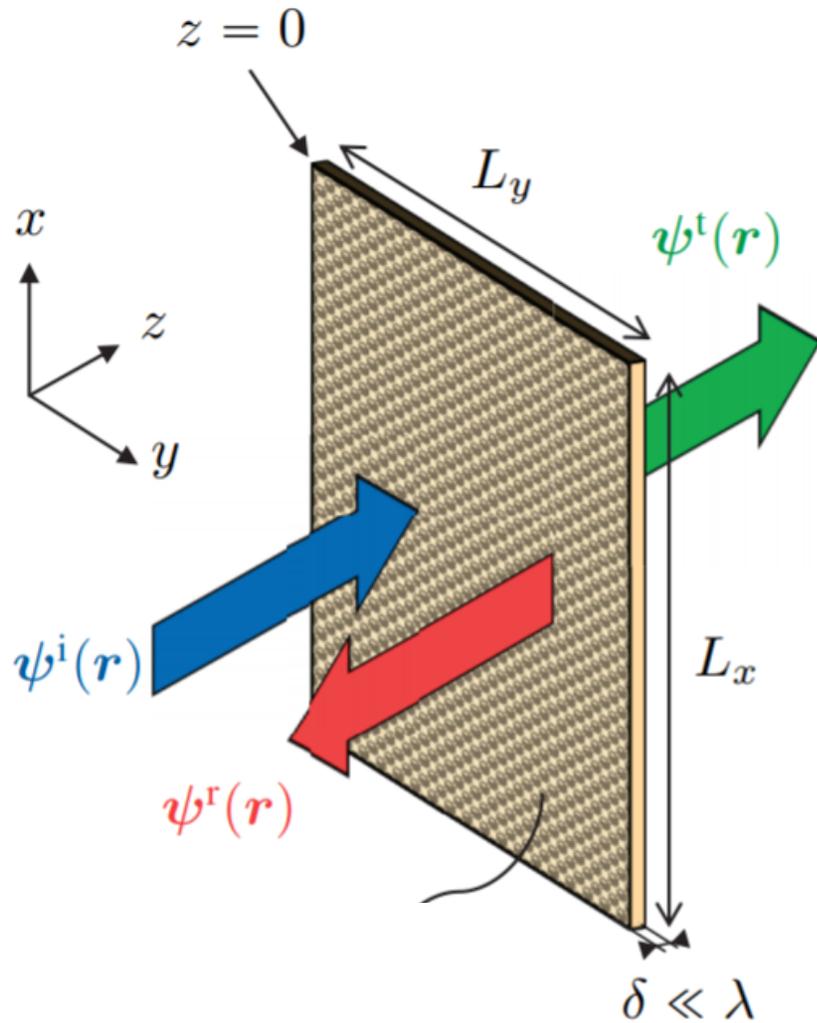
Reconfigurable Intelligent Metasurfaces

Reconfigurable Intelligent Metasurfaces

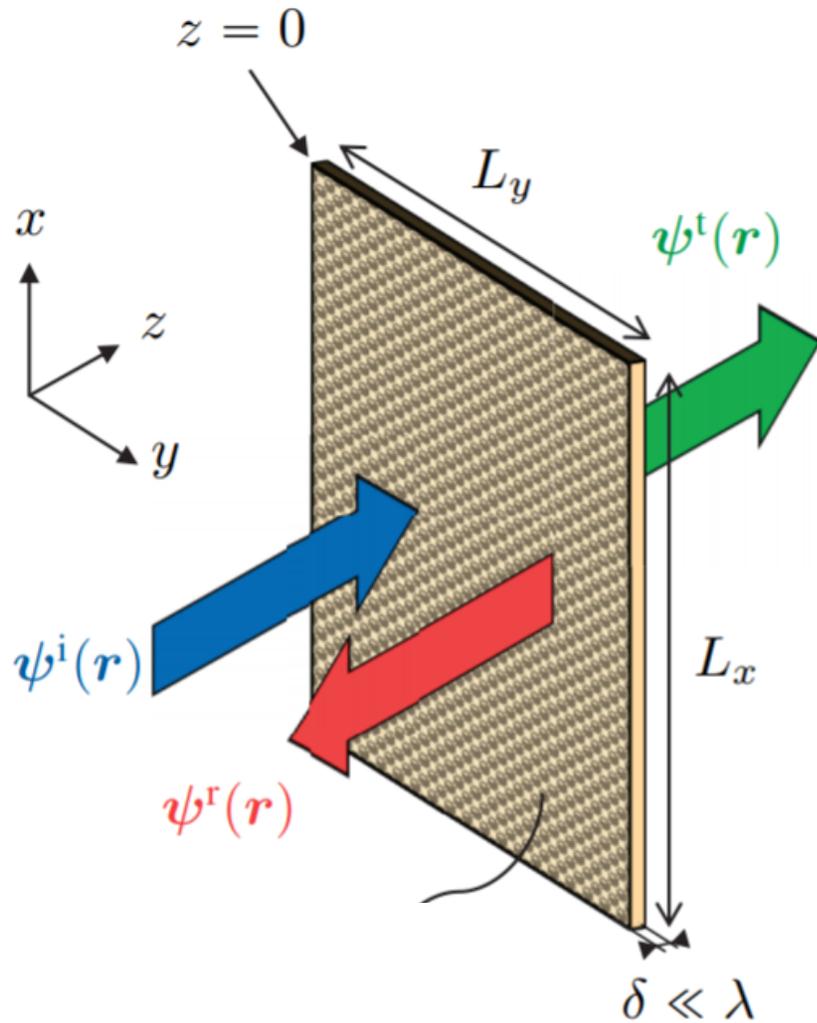


Reconfigurable Intelligent Metasurfaces

□ Main characteristics



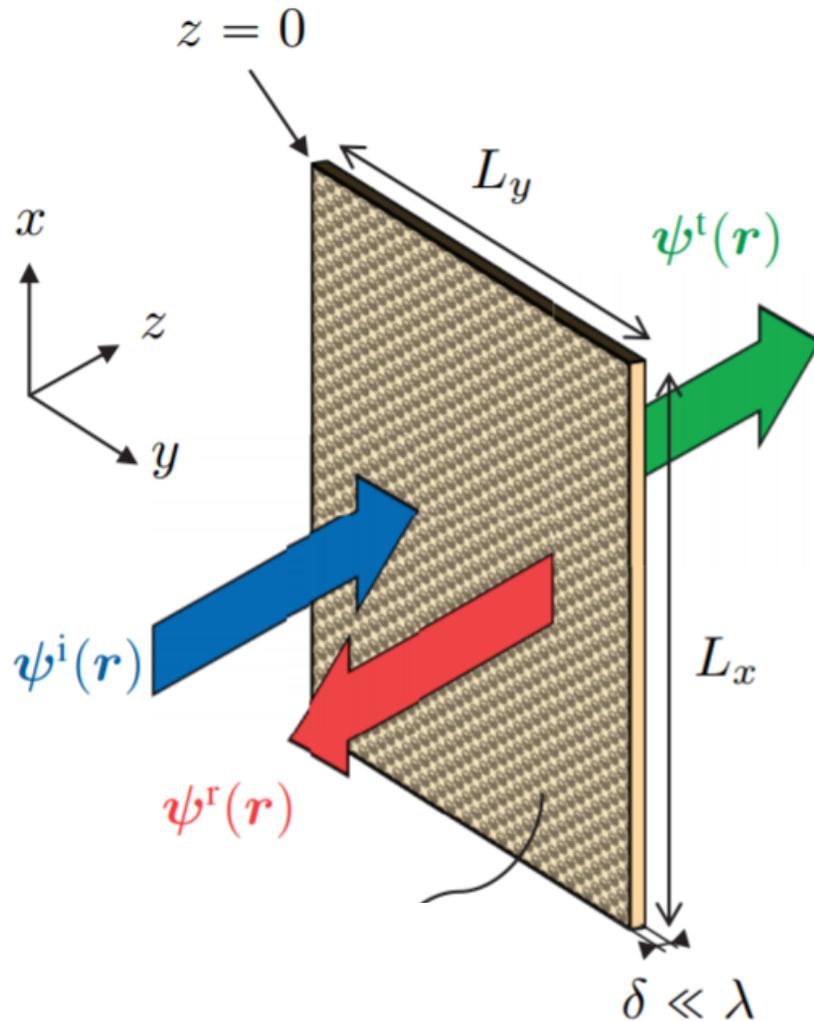
Reconfigurable Intelligent Metasurfaces



□ Main characteristics

- **Electrically thin:**
The thickness is considerably smaller than the wavelength

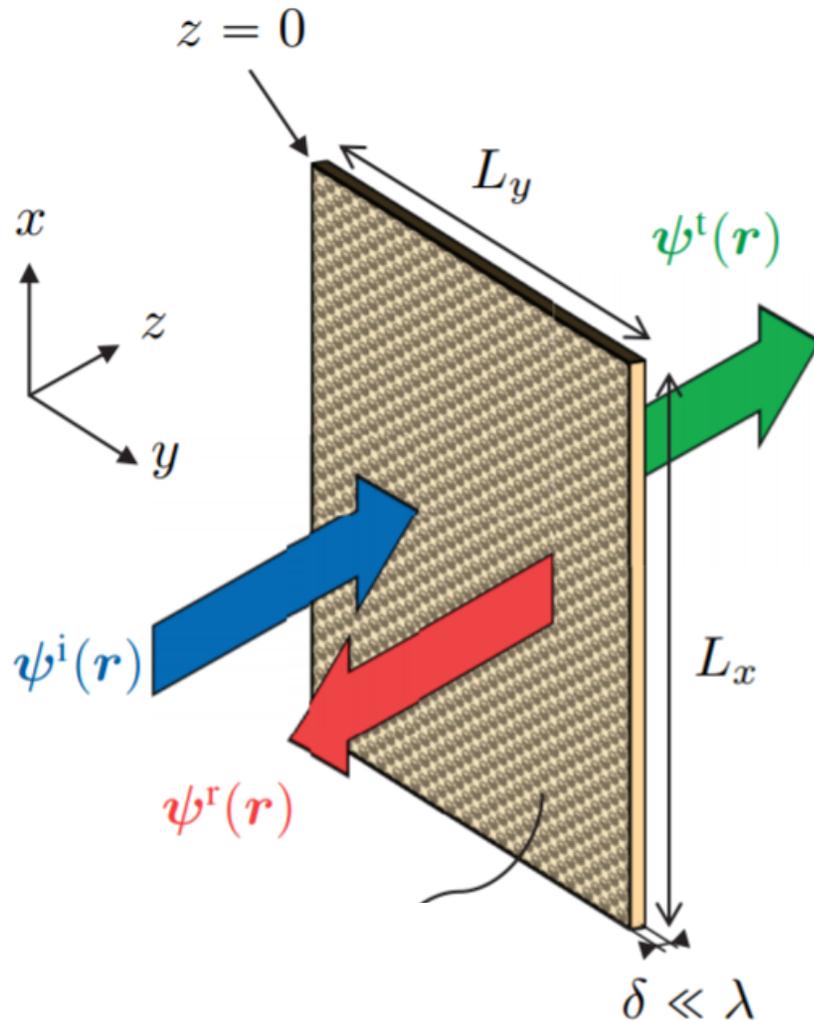
Reconfigurable Intelligent Metasurfaces



□ Main characteristics

- **Electrically thin:**
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- **Electrically large:**
The transverse size is relatively large as compared with the wavelength

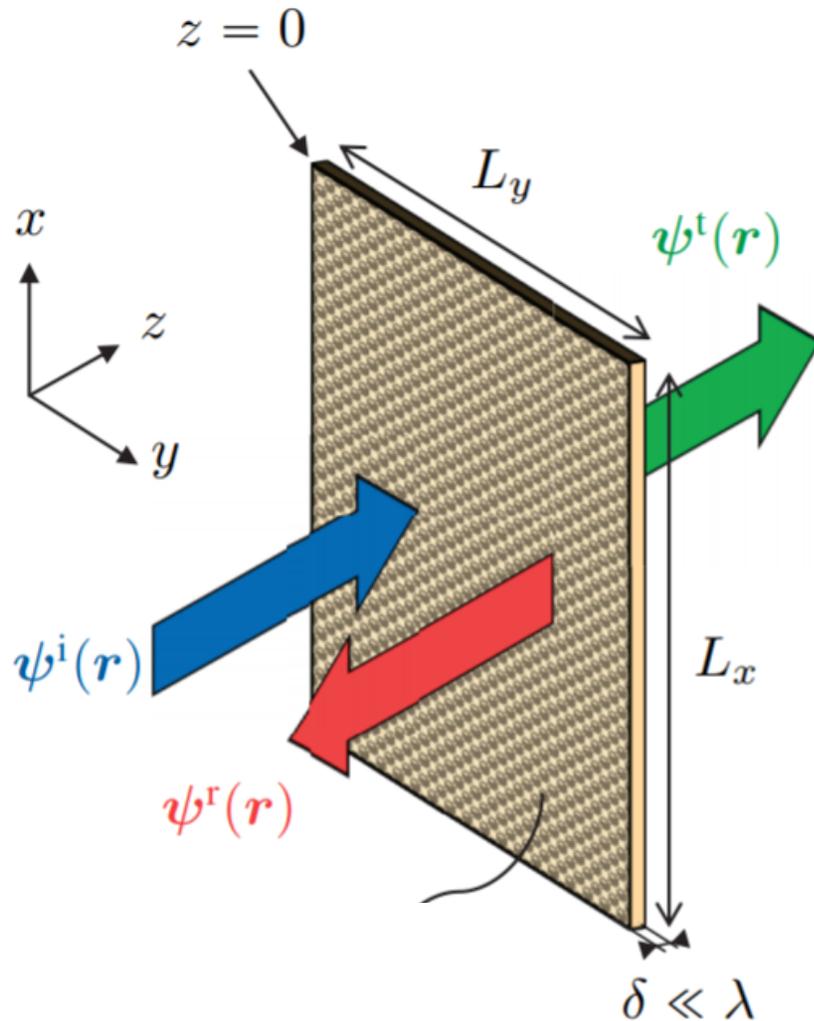
Reconfigurable Intelligent Metasurfaces



□ Main characteristics

- **Electrically thin:**
The thickness is considerably smaller than the wavelength
- **Electrically large:**
The transverse size is relatively large as compared with the wavelength
- **Homogenizable:**
The distance between adjacent unit cells is much smaller than the wavelength

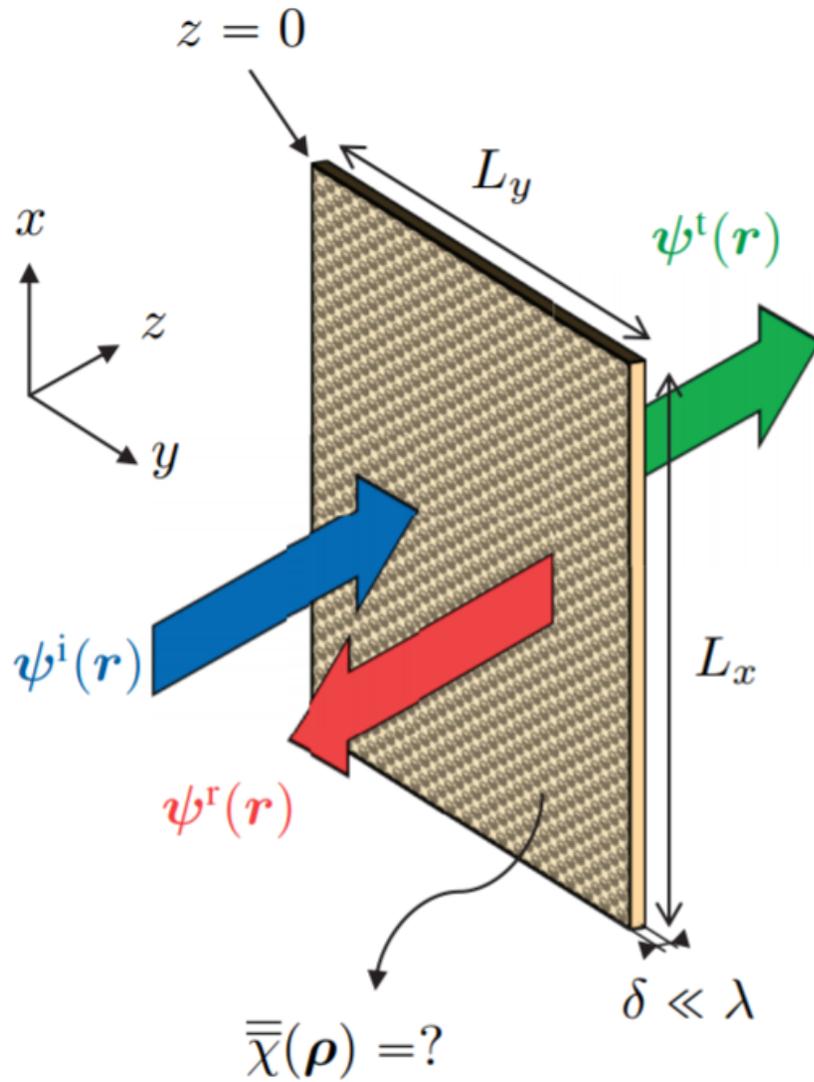
Reconfigurable Intelligent Metasurfaces



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The distance between adjacent unit cells is much smaller than the wavelength
- **Sub-wavelength structure:**
The size of each unit cell is much smaller than the wavelength

Reconfigurable Intelligent Metasurfaces

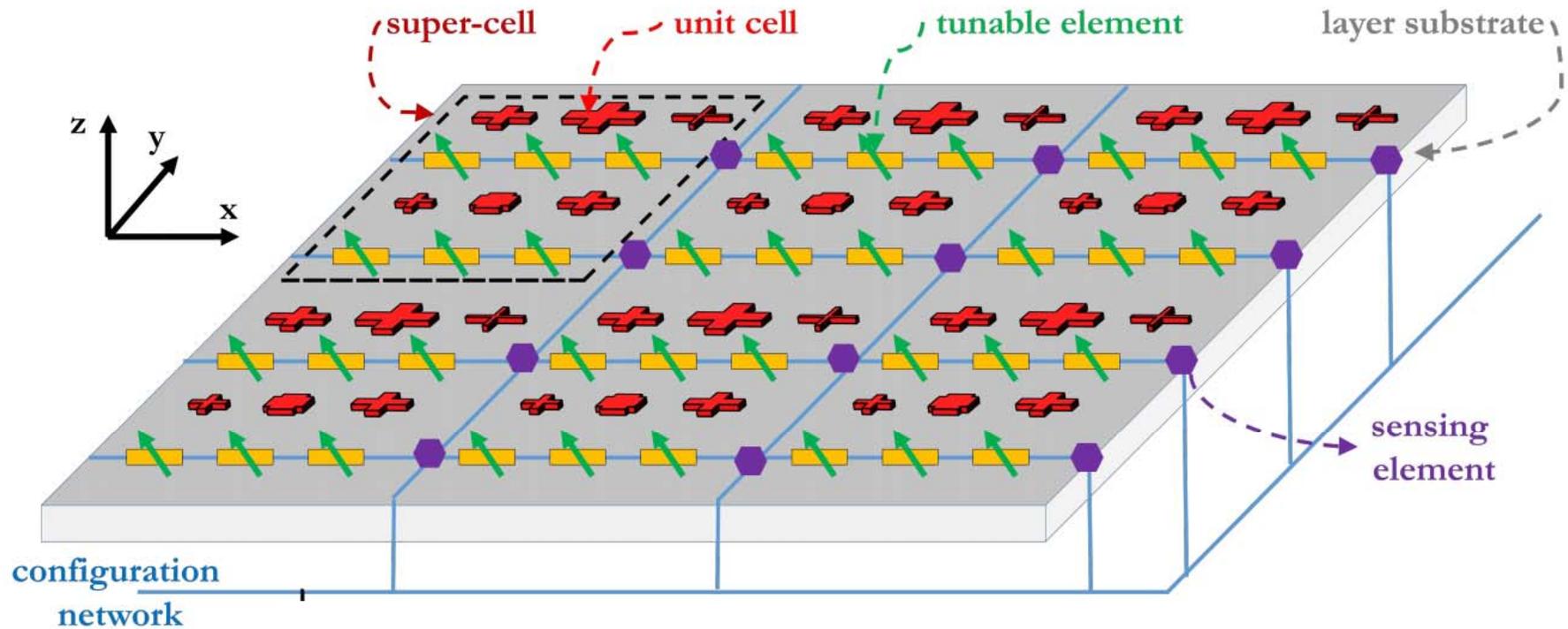


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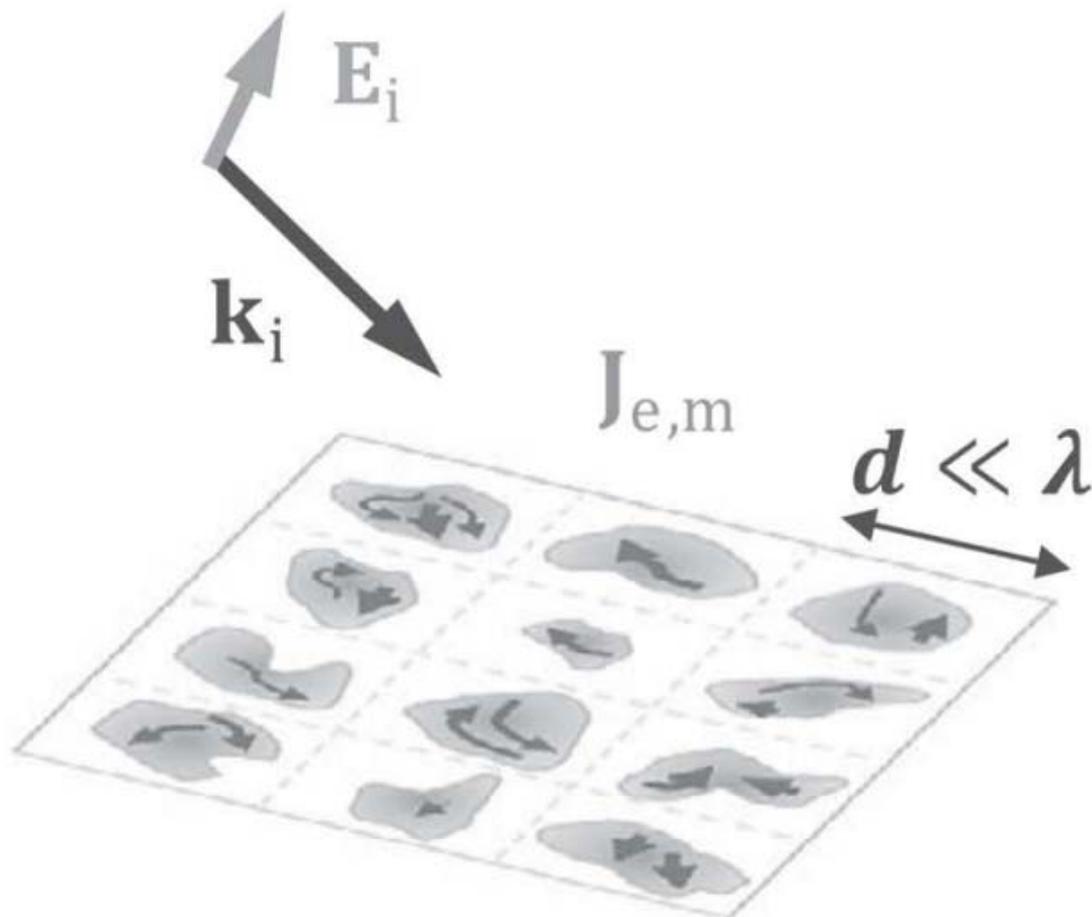
Reconfigurable Intelligent (Meta)Surfaces

Conceptual Structure



Reconfigurable Intelligent Metasurfaces

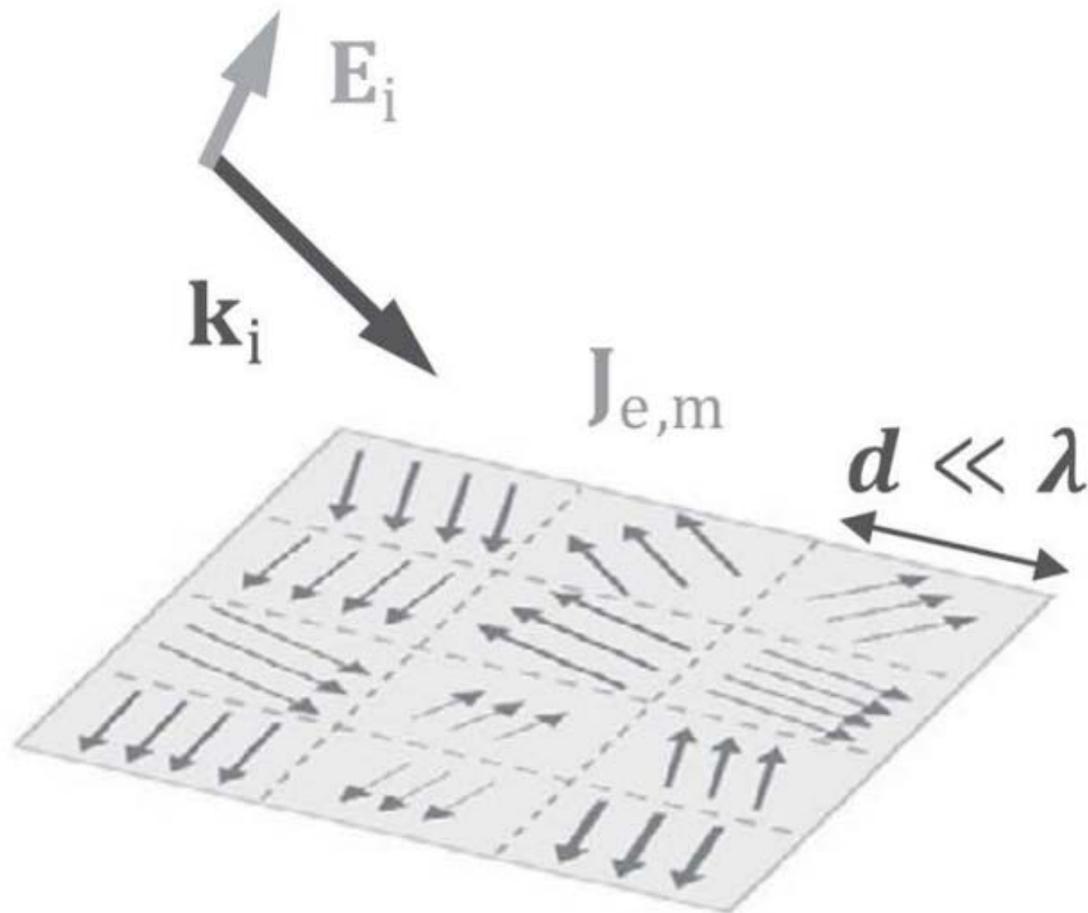
Homogenizable
... from sub-wavelength scatterers ...



Reconfigurable Intelligent Metasurfaces

Homogenizable

... to a continuous sheet of currents ...

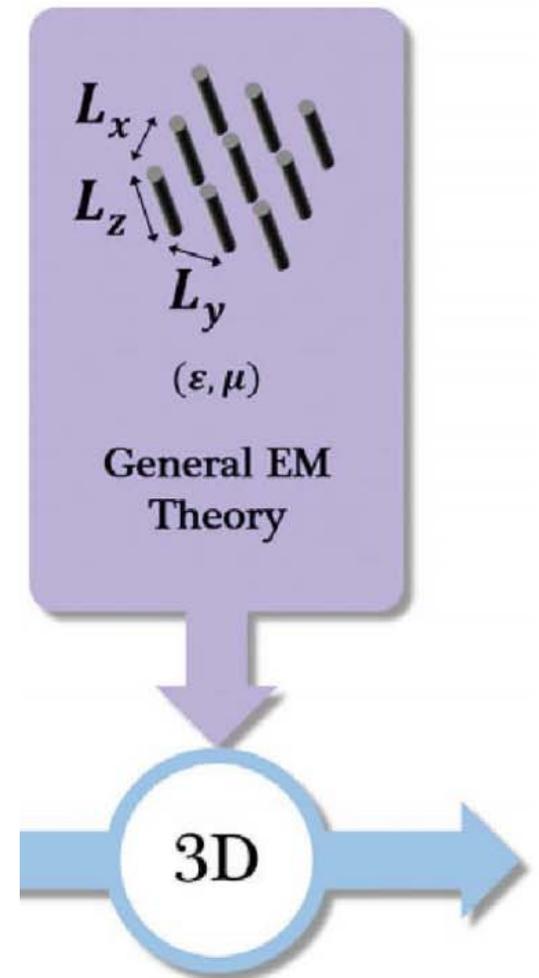
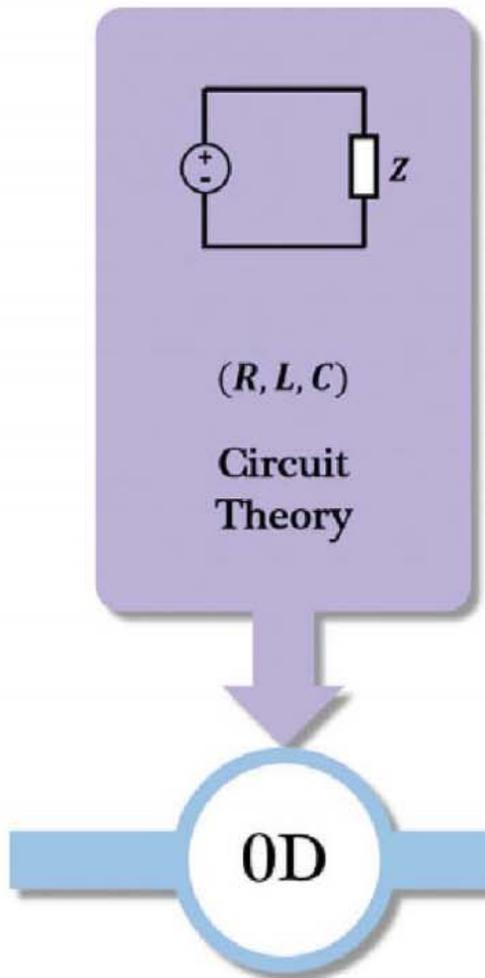


Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances

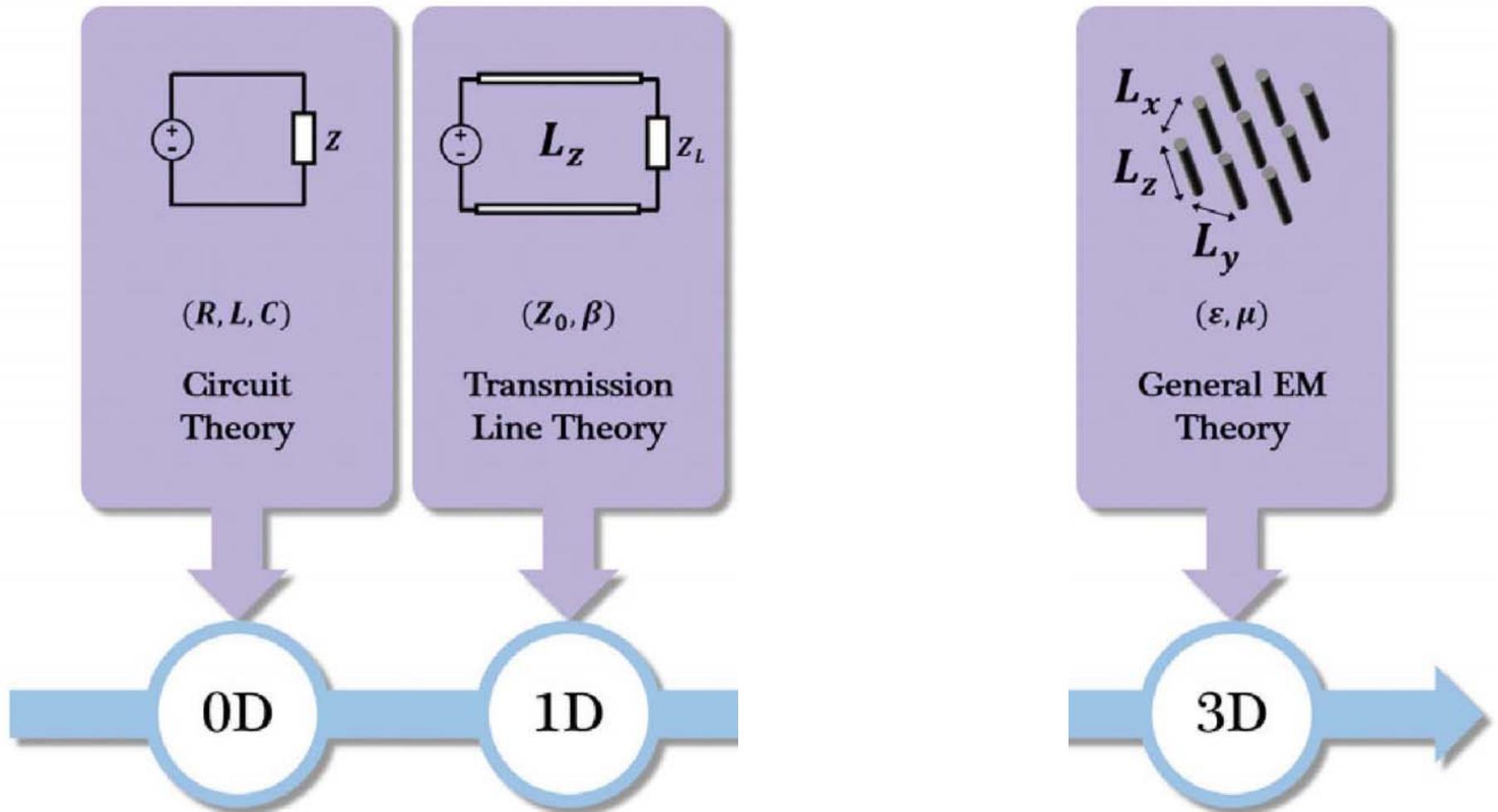
Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances



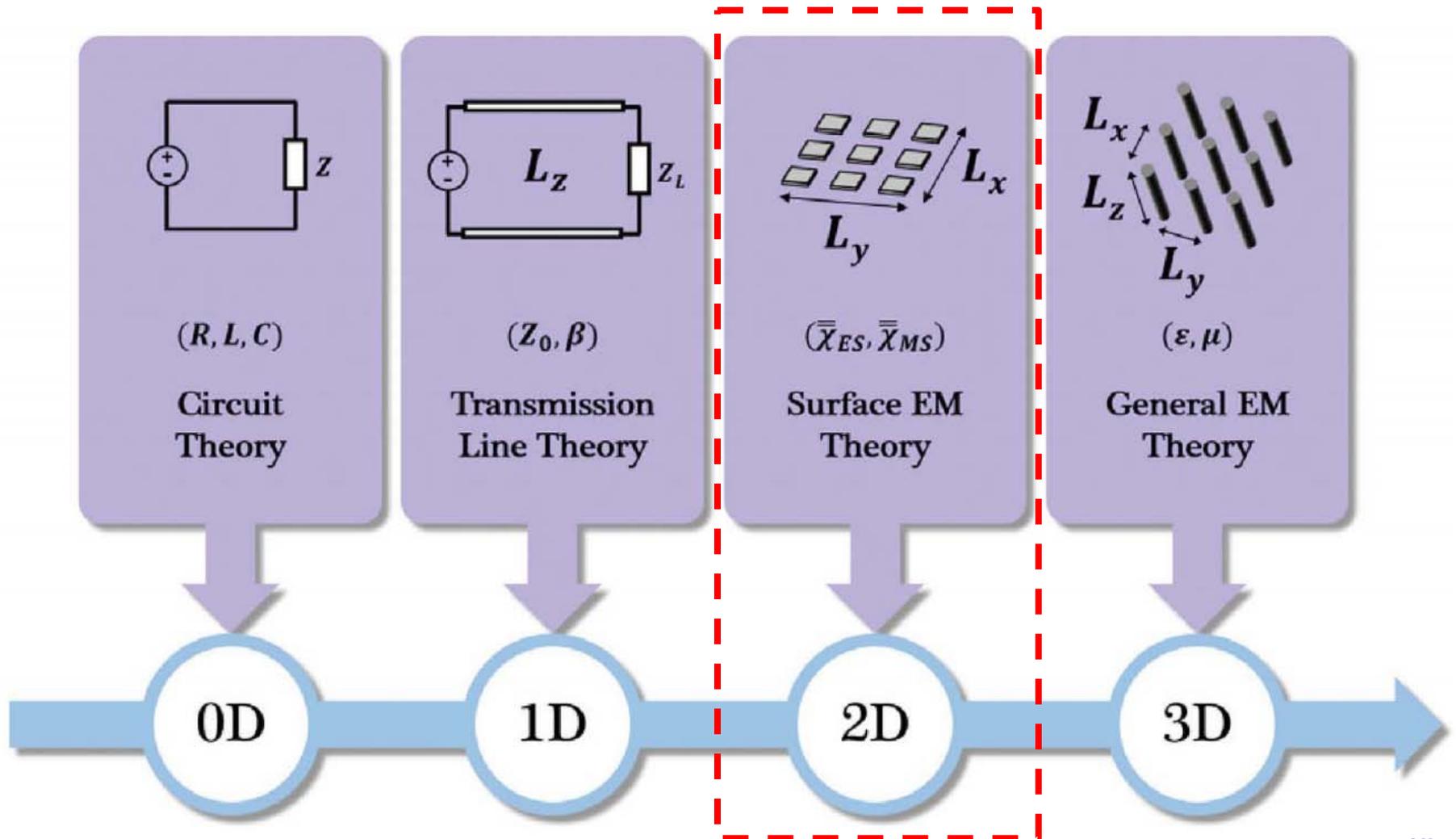
Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances



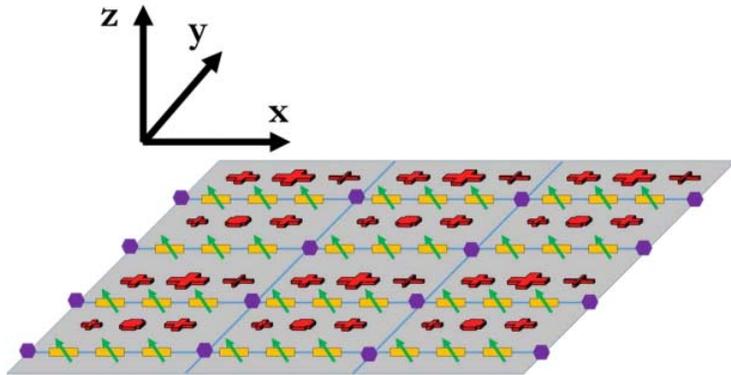
Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances



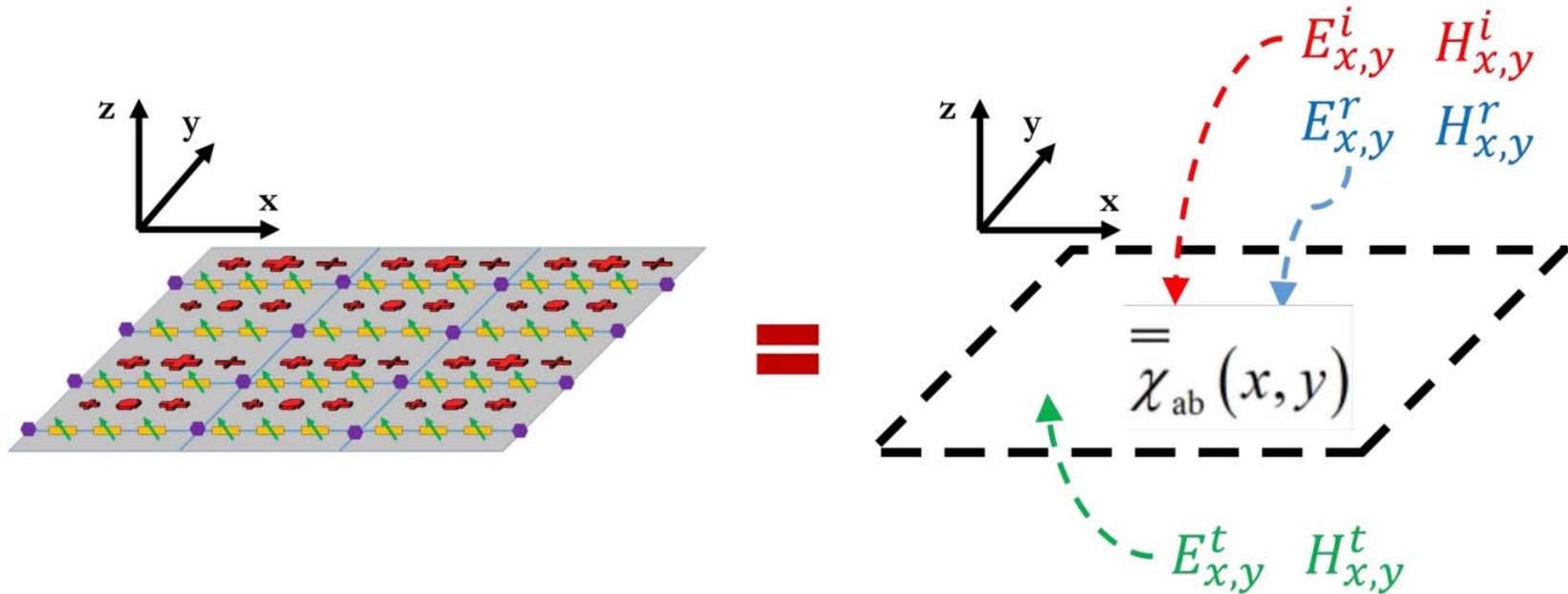
Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances



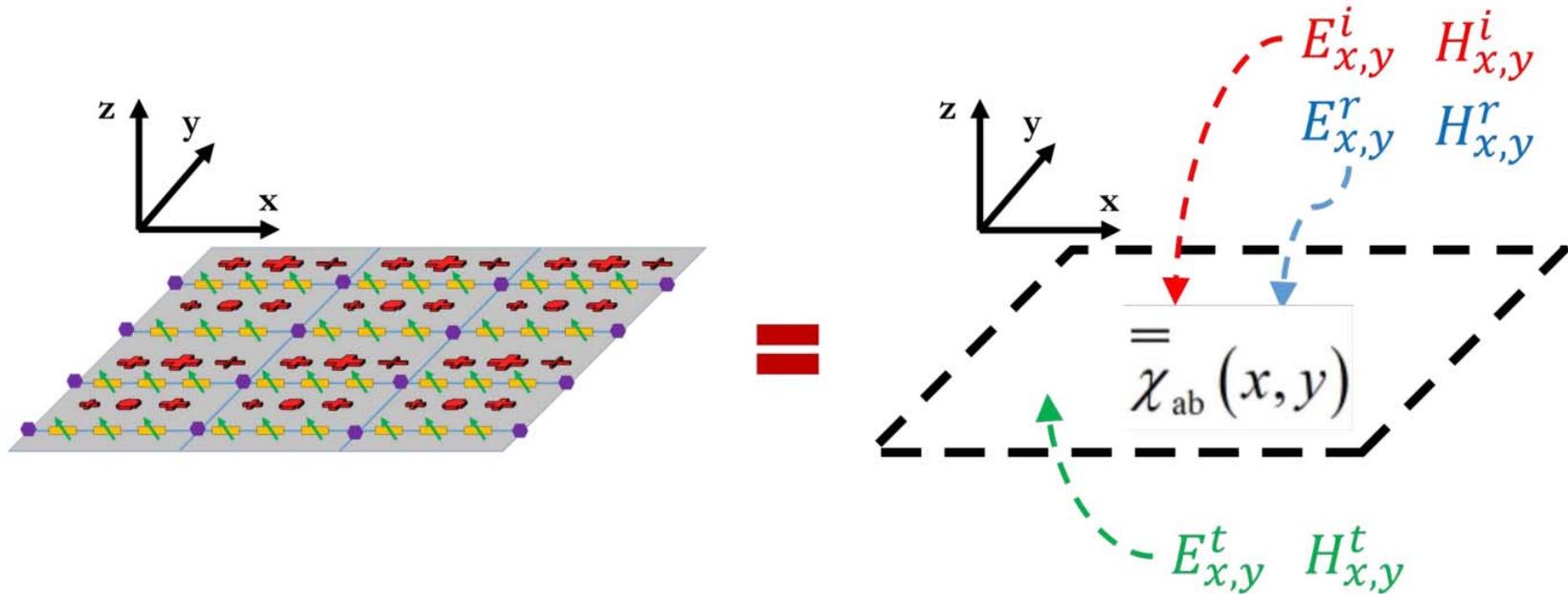
Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances



Reconfigurable Intelligent Metasurfaces: Modeling

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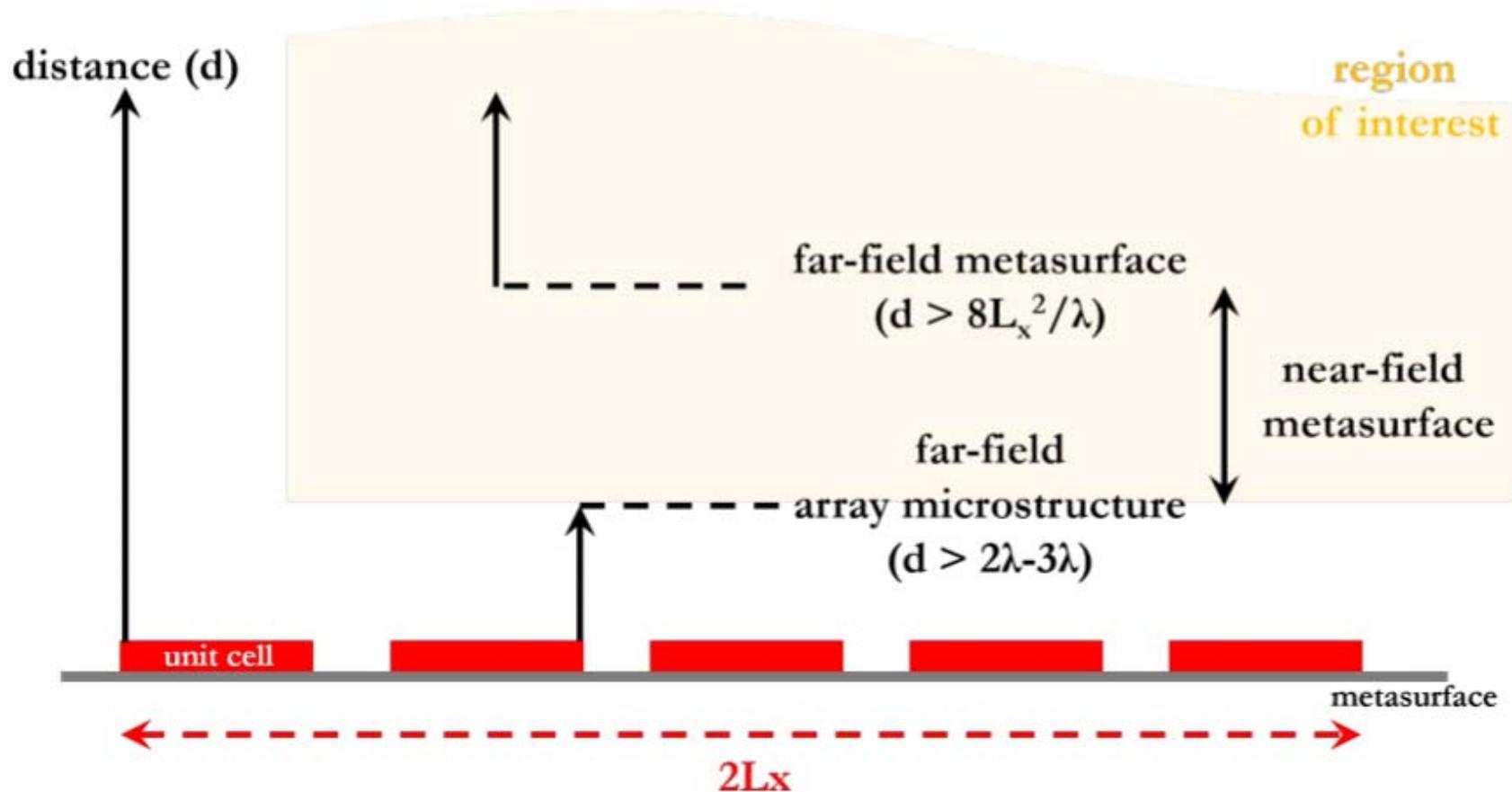


Perfect Anomalous Reflection

$$\chi_{ee}^{yy}(x, y) = -\frac{2}{j\omega\epsilon} \frac{H_x^i(x, y) + H_x^r(x, y)}{E_y^i(x, y) + E_y^r(x, y)}$$

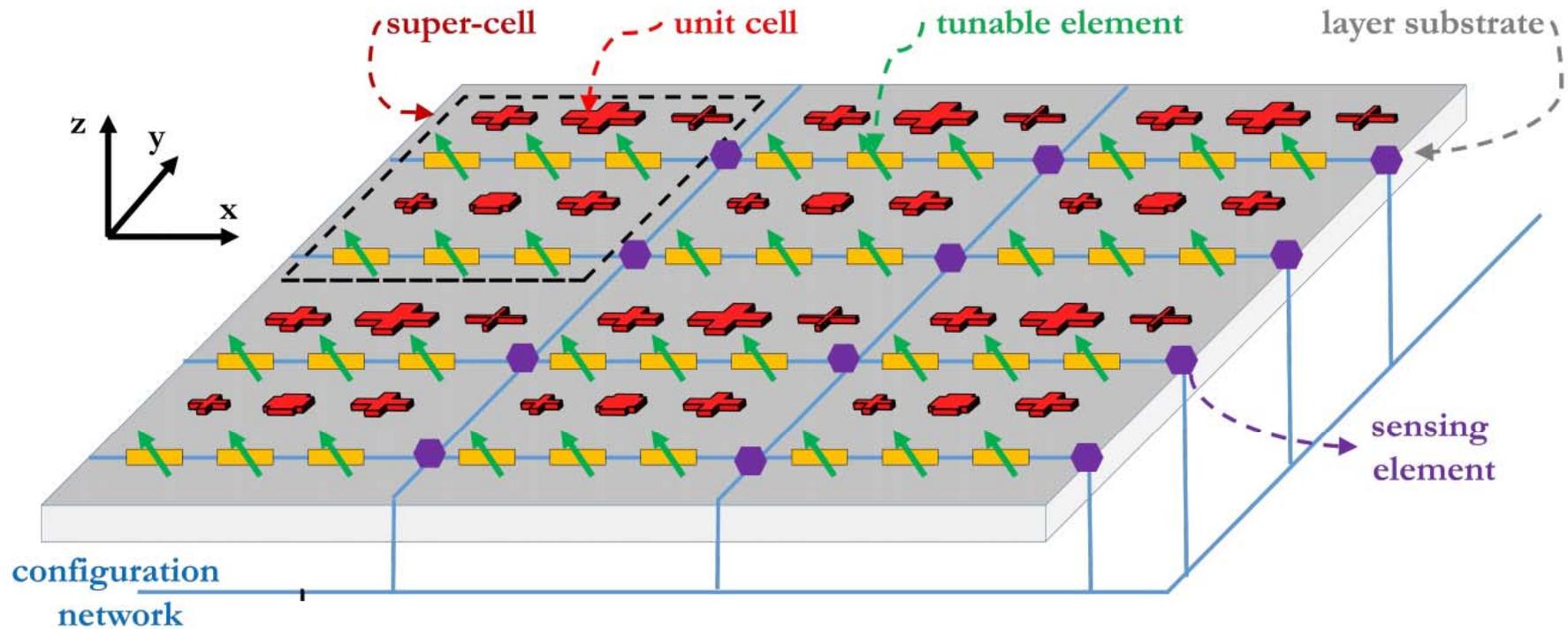
Reconfigurable Intelligent Metasurfaces: Modeling

Surface Susceptibilities / Impedances: Applicability



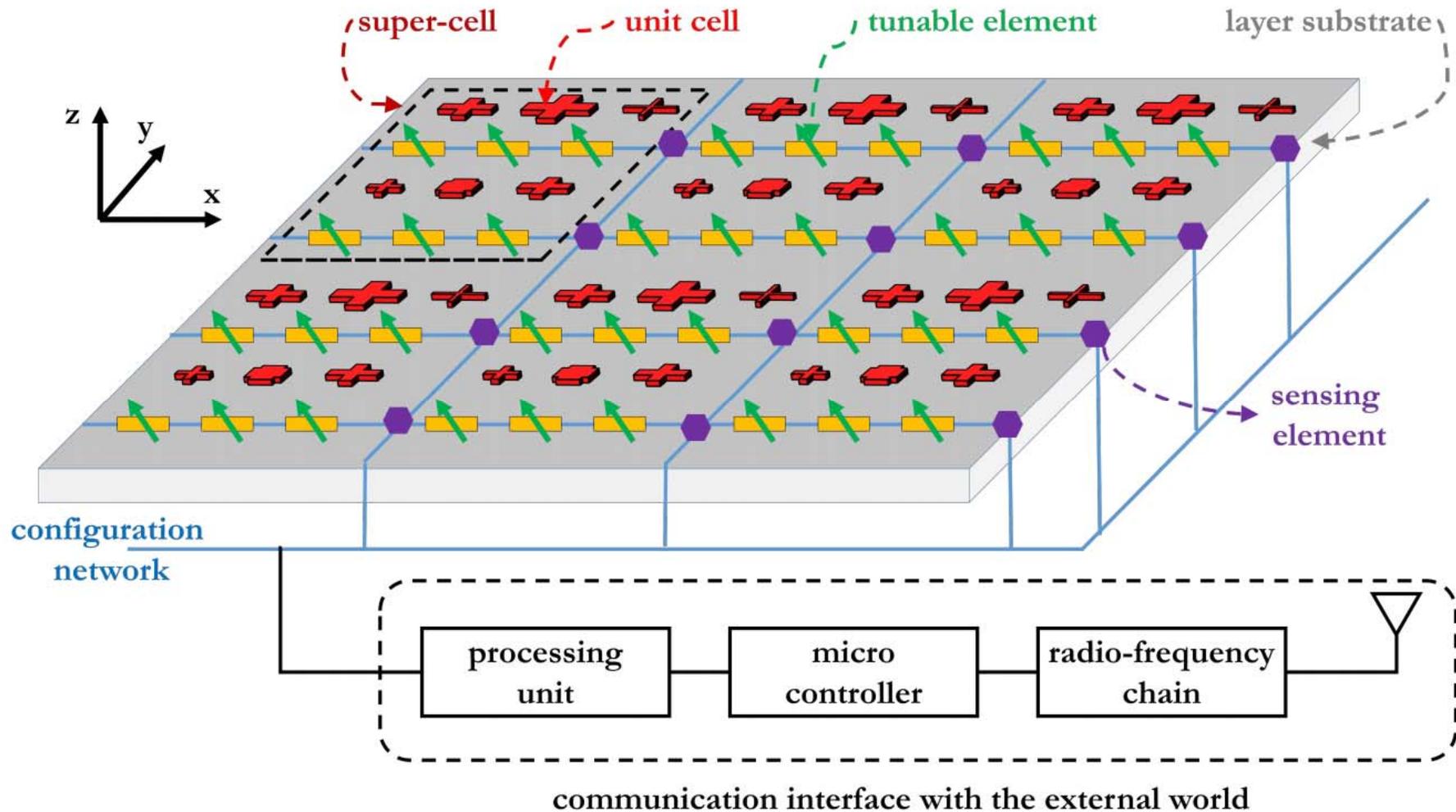
Reconfigurable Intelligent (Meta)Surfaces

Conceptual Structure



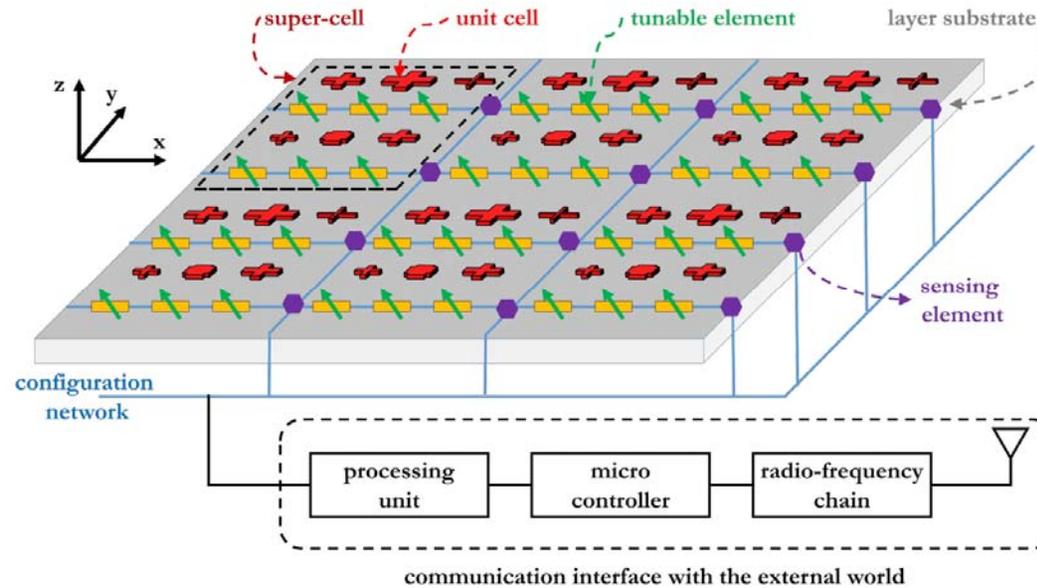
Reconfigurable Intelligent (Meta)Surfaces

Conceptual Structure and Operation



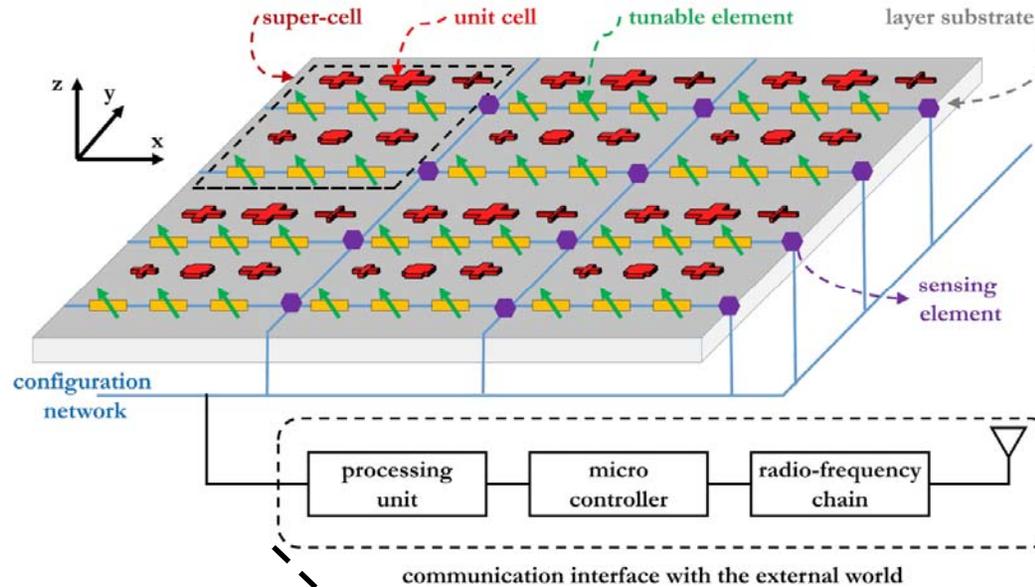
Reconfigurable Intelligent (Meta)Surfaces

Conceptual Structure and Operation



Reconfigurable Intelligent (Meta)Surfaces

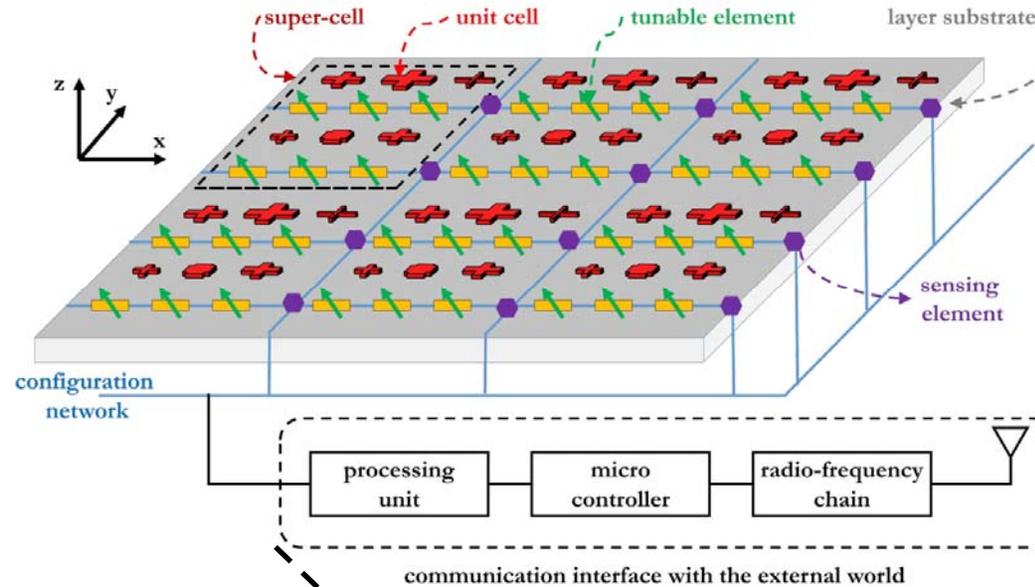
Conceptual Structure and Operation



Control & Configuration Phase

Reconfigurable Intelligent (Meta)Surfaces

Conceptual Structure and Operation

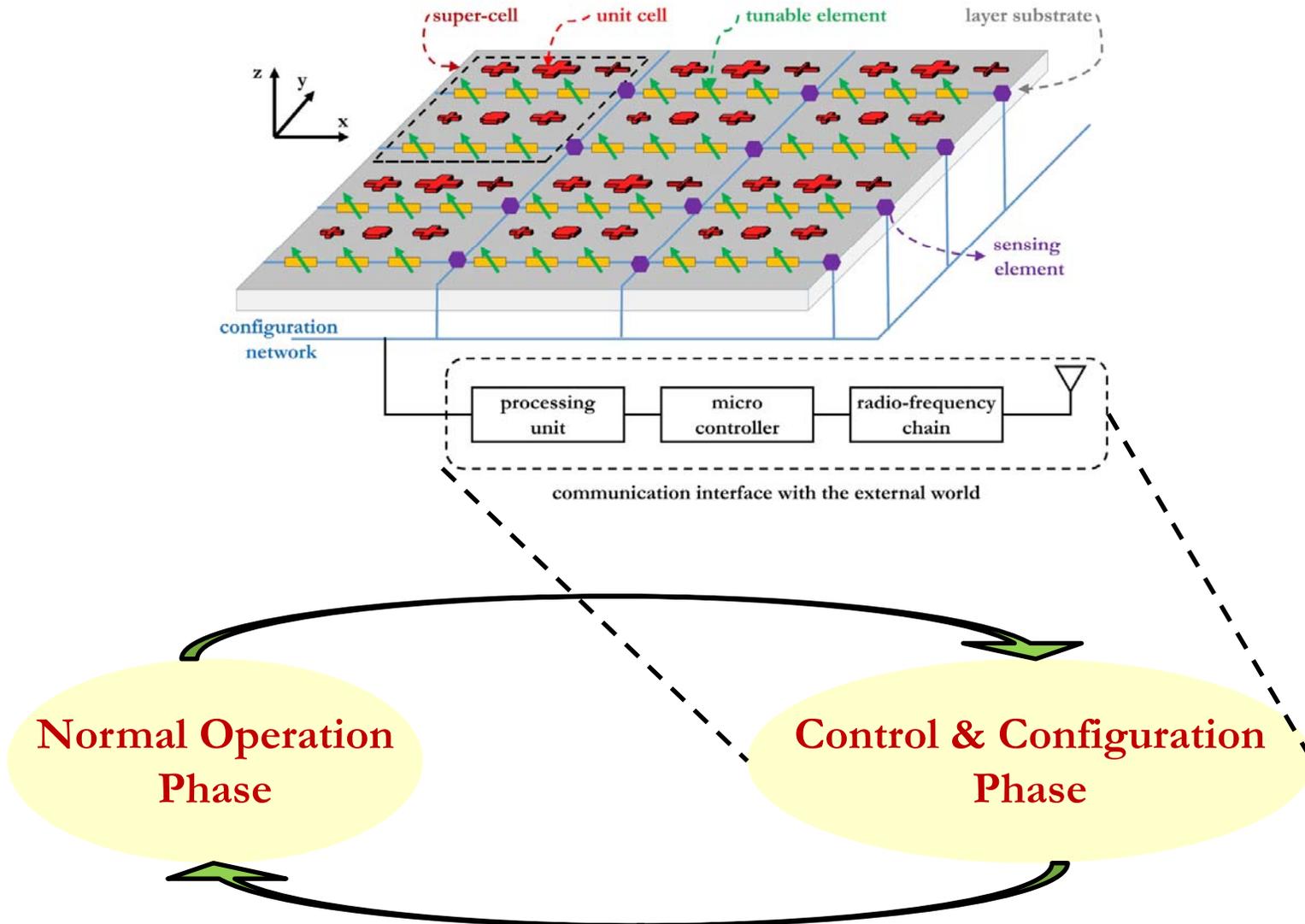


**Normal Operation
Phase**

**Control & Configuration
Phase**

Reconfigurable Intelligent (Meta)Surfaces

Conceptual Structure and Operation



Reconfigurable Intelligent (Meta)Surfaces

Passive vs. Nearly-Passive

Reconfigurable Intelligent (Meta)Surfaces

Passive vs. Nearly-Passive

- Non-reconfigurable surfaces may be passive

Reconfigurable Intelligent (Meta)Surfaces

Passive vs. Nearly-Passive

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- ❑ Reconfigurable (or dynamic) surfaces cannot be passive but may be nearly-passive

Reconfigurable Intelligent (Meta)Surfaces

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Reconfigurable Intelligent (Meta)Surfaces

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 - ❑ **Minimal digital signal processing** capabilities are needed only to configure the surface (during the control and programming phase)

Reconfigurable Intelligent (Meta)Surfaces

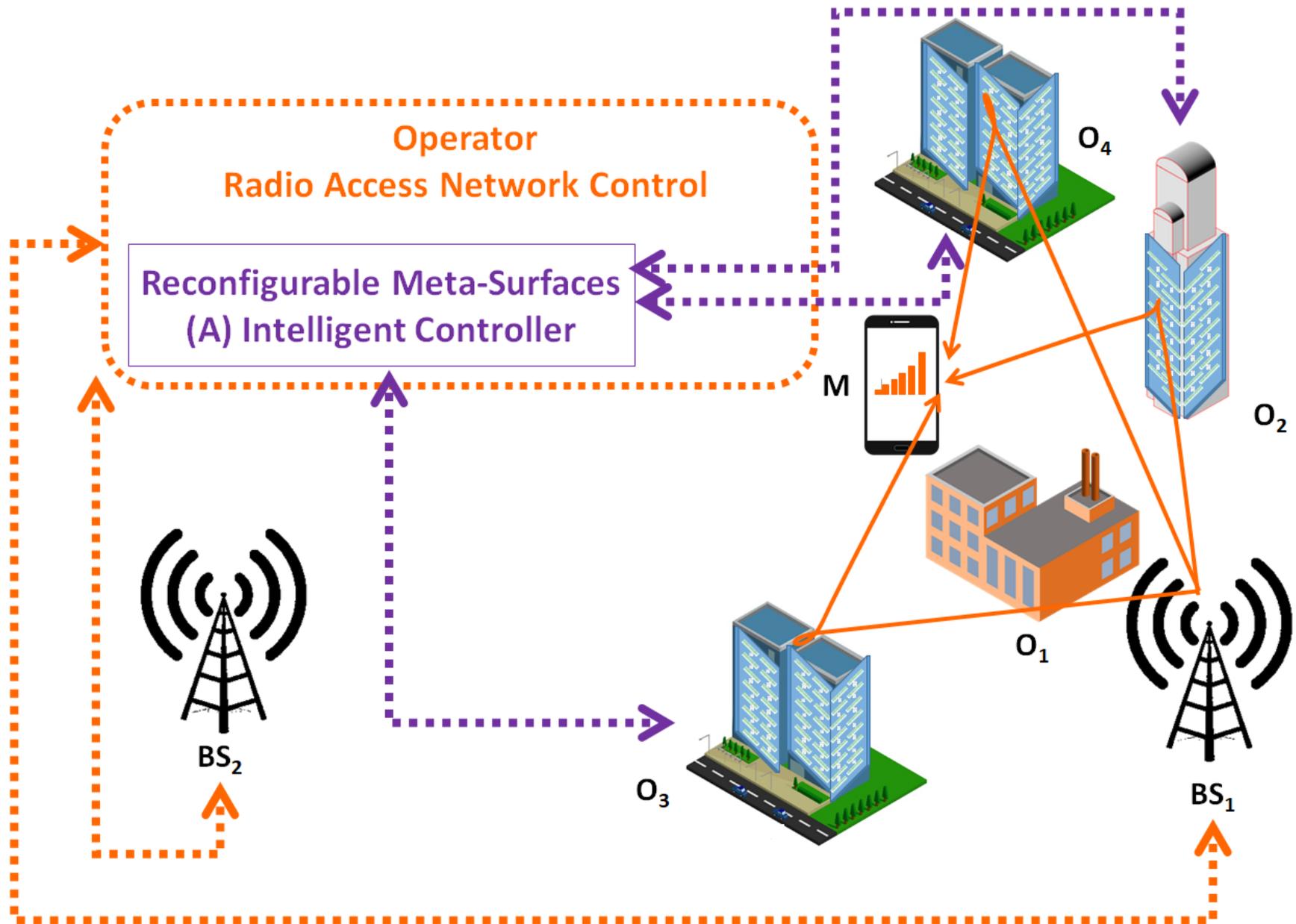
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 - ❑ **No power amplification** is used after configuration (during the normal operation phase)
 - ❑ **Minimal digital signal processing** capabilities are needed only to configure the surface (during the control and programming phase)
 - ❑ **Minimal power** is used only to configure the surface (during the control and programming phase)

RIS-Empowered Wireless Networks: The Big Picture



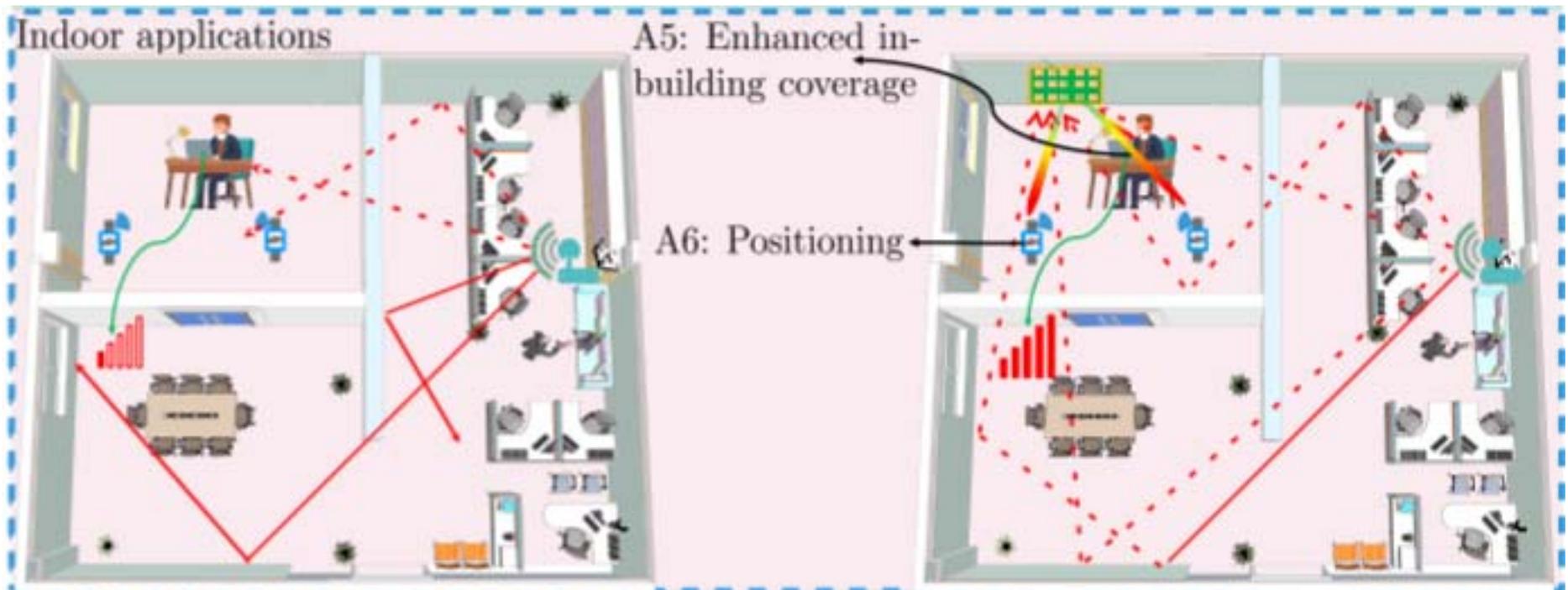
RIS-Empowered Wireless Networks: Outdoors



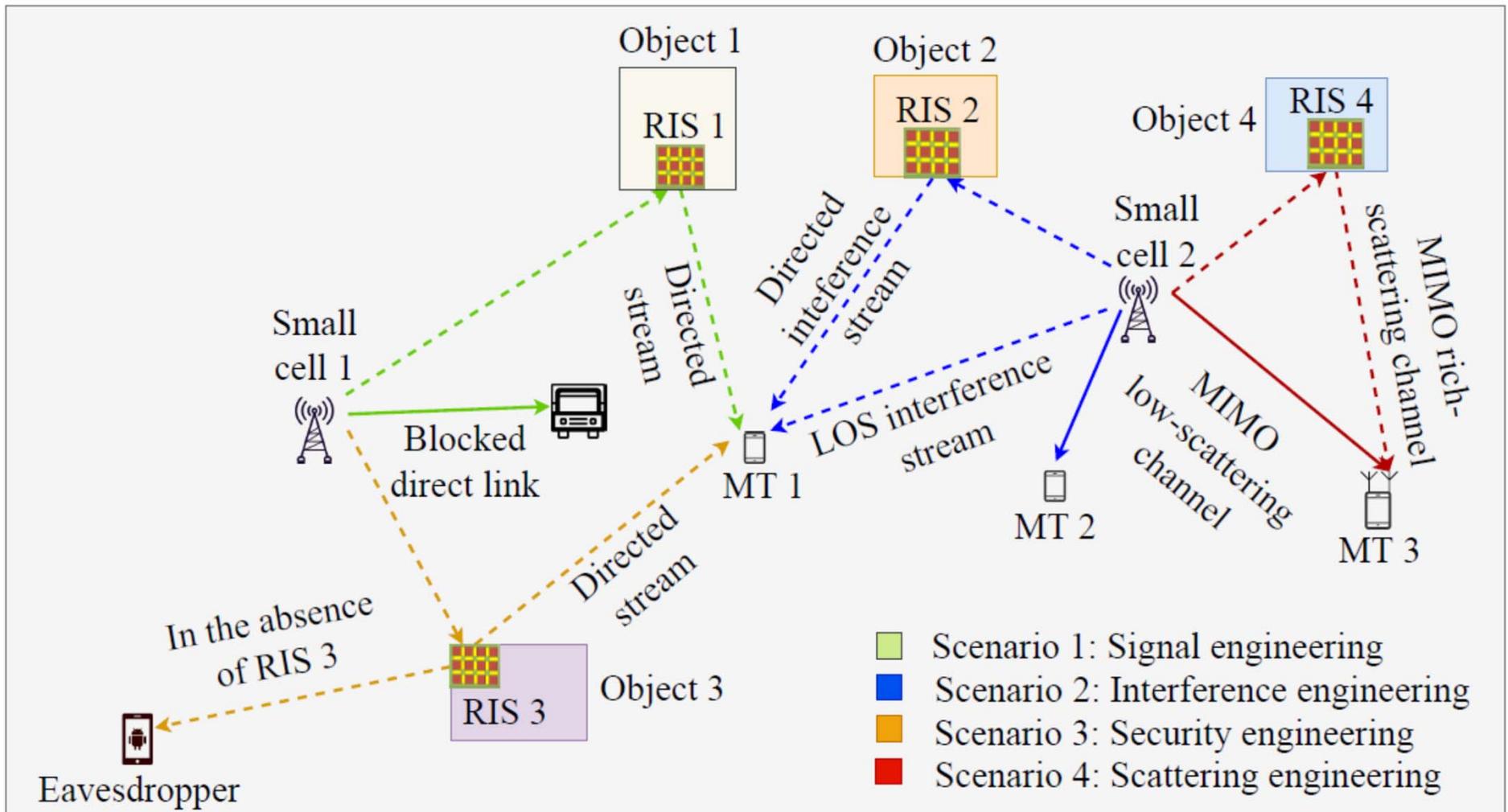
RIS-Empowered Wireless Networks: Outdoors



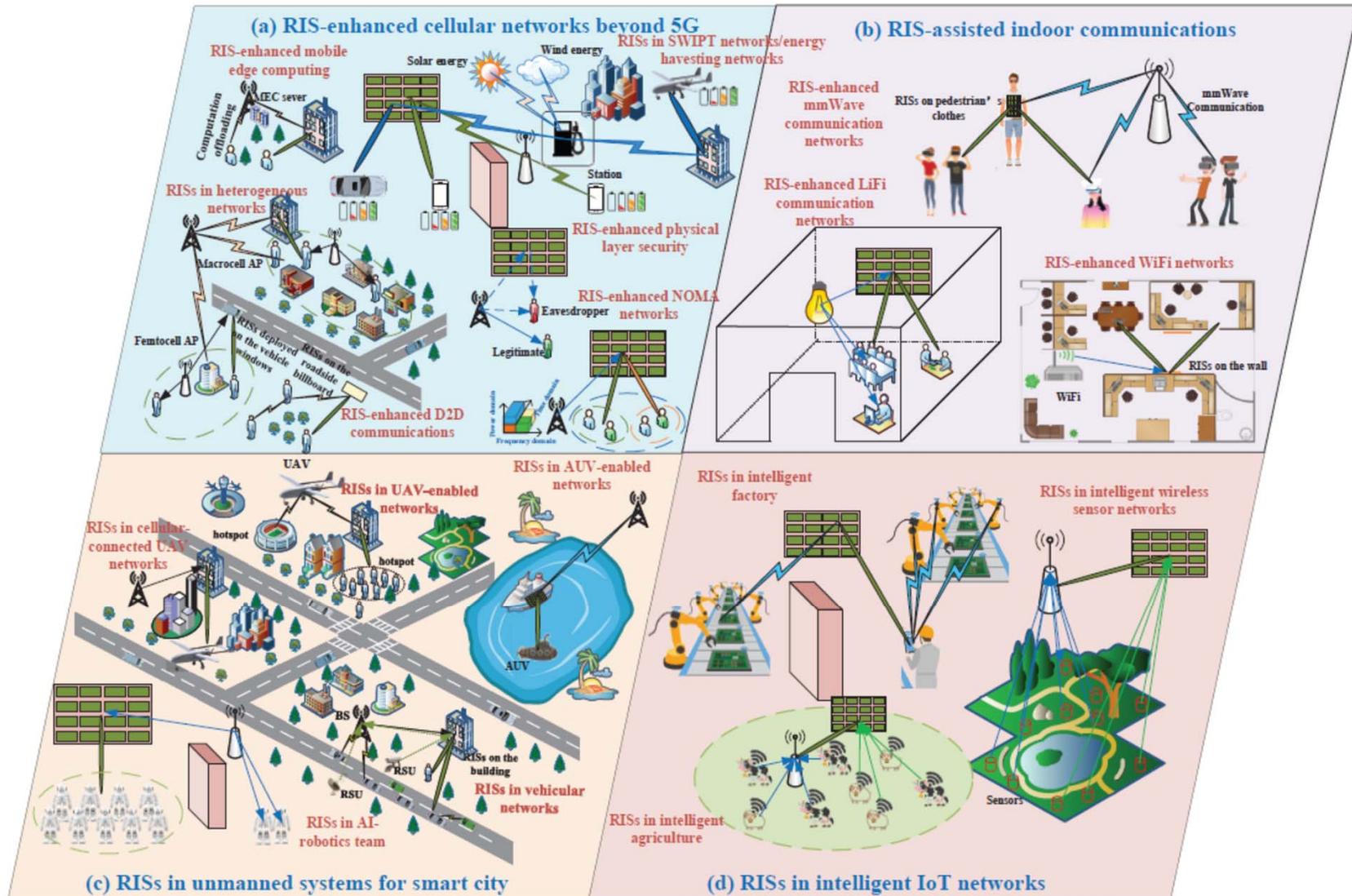
RIS-Empowered Wireless Networks: Indoors



Smart Radio Environments: RIS-Empowered Wireless



Enhancing Coverage, EE, Rate Through RISs



Reconfigurable Intelligent Metasurfaces

Where Are We ?

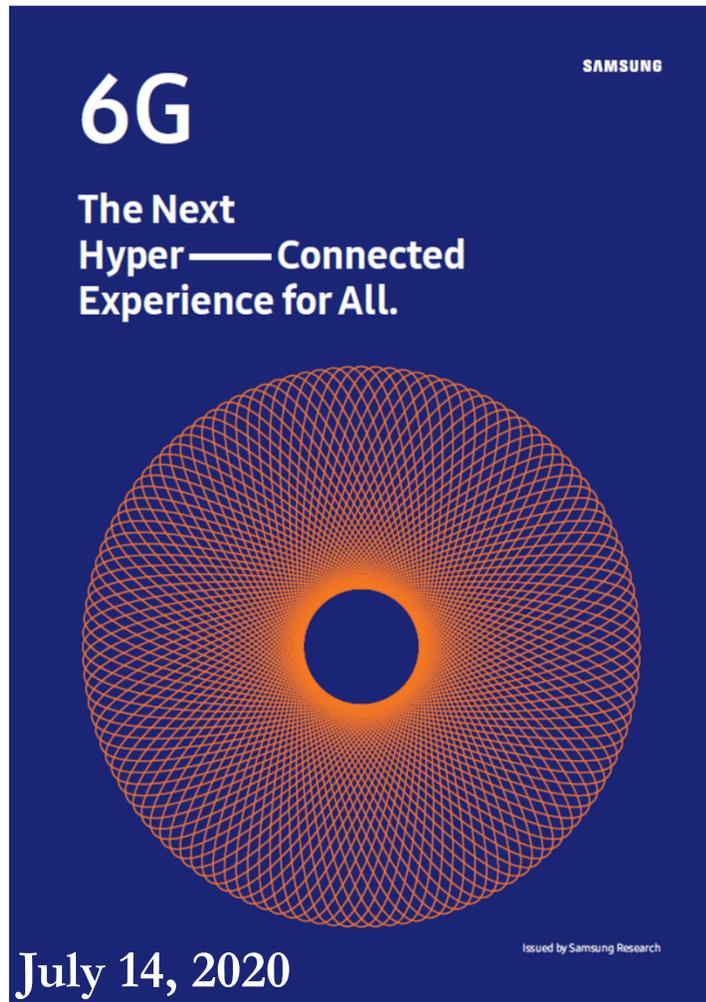
Terminology: RISs & Friends

□ These structures are often referred to as:

Terminology: RISs & Friends

- ❑ These structures are often referred to as:
 - ❑ Large intelligent surfaces (LISs)
 - ❑ Intelligent reflecting surfaces (IRSs)
 - ❑ Digitally controllable scatterers (DCSs)
 - ❑ Software-controllable surfaces
 - ❑ **Reconfigurable intelligent surfaces (RISs)**

Terminology: RISs & Friends



Novel Antenna Technologies

- *Reconfigurable intelligent surface (RIS)* can be used to provide a propagation path where no LoS link exists [25]. An example of signal reflection via RIS is illustrated in Figure 12.

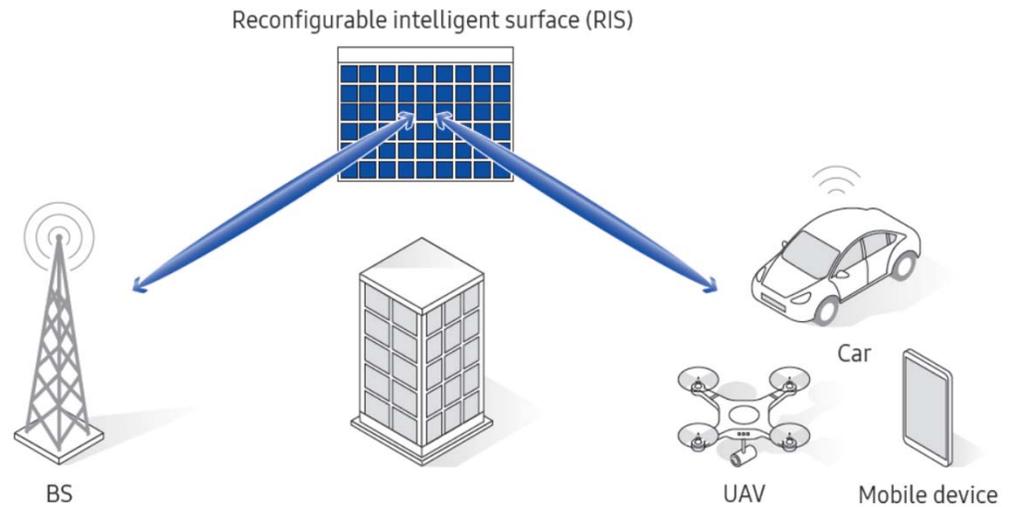


Figure 12

RIS-aided communication between a BS and a mobile user, where the LoS path is blocked.

Nearly-Passive RISs: Advantages and Limitations

Nearly-Passive RISs: Advantages and Limitations

The image shows a browser window displaying the Pivotal Commware website. The browser's address bar shows the URL 'pivotalcommware.com'. The website's navigation menu includes links for 'About', 'Technology', 'Products', 'News & Events', 'Careers', and 'Contact'. The main content area features a large banner with the following text: 'Inventors of Holographic Beam Forming®', 'Essential Element in the 5G Ecosystem', and '5G is PIVOTAL™'. Below this text is a call to action: 'Click Here to watch Pivotal's live demo from Mobile World Congress Los Angeles 2019.' The banner image depicts a woman using a smartphone, with orange signal waves emanating from the phone and a white Pivotal RIS device on a desk in the background.

← → ↻ 🔒 pivotalcommware.com 🔍 ☆ 🌐 👤 ⋮

PIVOTAL
COMMWARE®

About Technology Products News & Events Careers Contact

**Inventors of Holographic
Beam Forming®**
Essential Element in the 5G Ecosystem

5G is PIVOTAL™

[Click Here](#) to watch Pivotal's live demo from Mobile World Congress Los Angeles 2019.

Nearly-Passive RISs: Advantages and Limitations

The image is a screenshot of the Pivotal Commware website. At the top, the browser address bar shows 'pivotalcommware.com'. The navigation menu includes 'About', 'Technology' (circled in red), 'Products', 'News & Events', 'Careers', and 'Contact'. The main content area features the Pivotal Commware logo on the left and a hero image on the right. The hero image shows a woman using a smartphone, a desk lamp, and a white RIS device with orange signal waves emanating from it. Text on the left side of the hero section reads: 'Inventors of Holographic Beam Forming®', 'Essential Element in the 5G Ecosystem', '5G is PIVOTAL™', and 'Click Here to watch Pivotal's live demo from Mobile World Congress Los Angeles 2019.'

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PIVOTAL
COMMWARE®

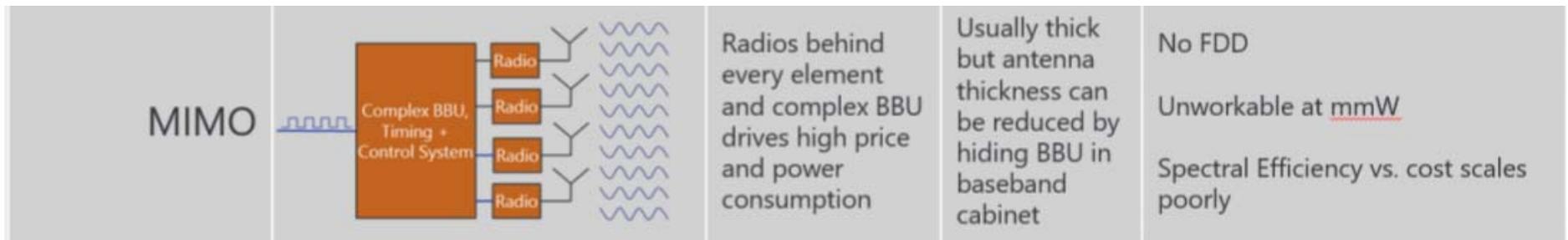
About **Technology** Products News & Events Careers Contact

Inventors of Holographic Beam Forming®
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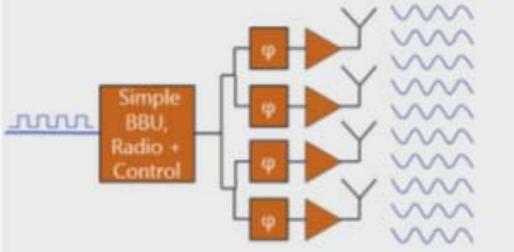
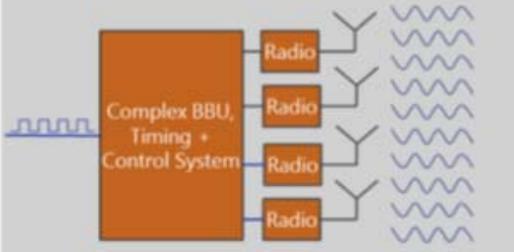
5G is PIVOTAL™

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Nearly-Passive RISs: Advantages and Limitations



Nearly-Passive RISs: Advantages and Limitations

<p>Phased Array</p>		<p>Distributed phase shifters and amplifiers pushes moderate price</p>	<p>Trades cost for thickness. Thin is very expensive</p>	<p>Thermal challenges difficult due to distributed amplification.</p> <p>Multi-beam significantly increases cost (more phase shifters, distribution layers)</p>
<p>MIMO</p>		<p>Radios behind every element and complex BBU drives high price and power consumption</p>	<p>Usually thick but antenna thickness can be reduced by hiding BBU in baseband cabinet</p>	<p>No FDD</p> <p>Unworkable at <u>mmW</u></p> <p>Spectral Efficiency vs. cost scales poorly</p>

Nearly-Passive RISs: Advantages and Limitations

Architecture	Block Diagram	Cost	Size	Challenges
RIS Holographic Beam Former		Super-sampled COTS design enables low price	Thin, Conformable	Single beam per polarization per sub-aperture.
Phased Array		Distributed phase shifters and amplifiers pushes moderate price	Trades cost for thickness. Thin is very expensive	Thermal challenges difficult due to distributed amplification. Multi-beam significantly increases cost (more phase shifters, distribution layers)
MIMO		Radios behind every element and complex BBU drives high price and power consumption	Usually thick but antenna thickness can be reduced by hiding BBU in baseband cabinet	No FDD Unworkable at <u>mmW</u> Spectral Efficiency vs. cost scales poorly

Nearly-Passive RISs: Advantages and Limitations

Example of Power Consumption

Nearly-Passive RISs: Advantages and Limitations

Example of Power Consumption

	Phased Array	RIS HBF	Unit
Number of Unit Cells	256	640	#
Antenna Gain	28	26	dB
Number of RF chains	256	1	#
Transmit Power per chain	6.2	2512	mW
Total RF Transmit Power	1.58	2.51	W
Power Added Efficiency	4.0%	25.0%	%
DC Draw for RF	39.6	10.0	W
HBF Controller	0	2.9	W
Total DC Power	39.6	12.9	W

Nearly-Passive RISs: Advantages and Limitations

Example of Power Consumption

	Phased Array	RIS HBF	Unit
Number of Unit Cells	256	640	#

Nearly-Passive RISs: Advantages and Limitations

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Nearly-Passive RISs: Advantages and Limitations

Example of Power Consumption

	Phased Array	RIS HBF	Unit
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Compared with other transmission technologies, e.g., phased arrays, multi-antenna transmitters, and relays, RISs require **the largest number of scattering elements**, but each of them needs to be **backed by the fewest and least costly components**. Also, **no power amplifiers** are usually needed.

Nearly-Passive RISs: Advantages and Limitations

Example of Power Consumption

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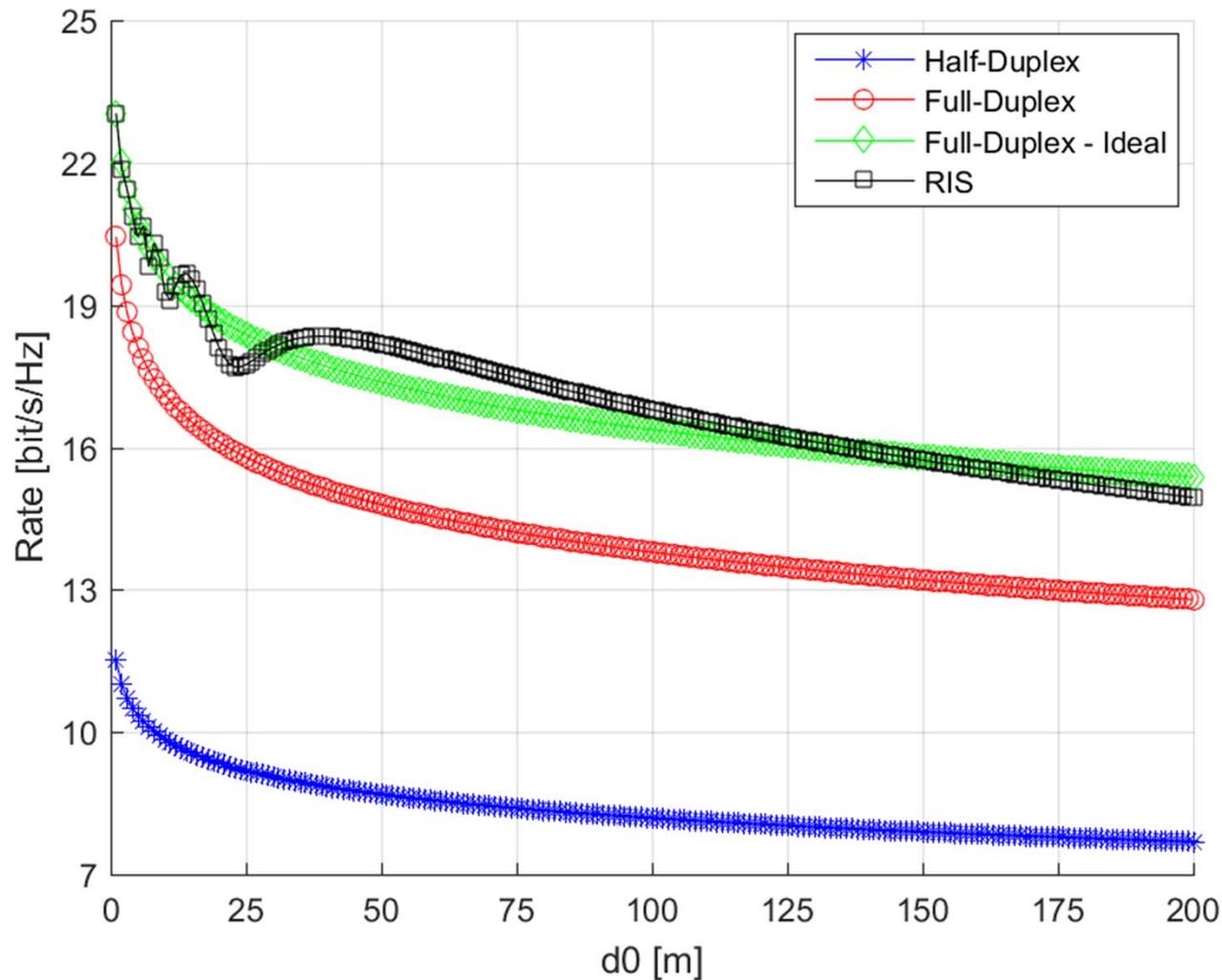
... no free lunch rule ...

Nearly-Passive RISs: Advantages and Limitations

Example: RIS vs. Relay

Nearly-Passive RISs: Advantages and Limitations

Example: RIS (1.5m = 140λ , reflector) vs. Relay (1-antenna)



Nearly-Passive RISs: Advantages and Limitations

Further Information

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Digital Object Identifier 10.1109/OJCOMS.2020.3002955

Reconfigurable Intelligent Surfaces vs. Relaying: Differences, Similarities, and Performance Comparison

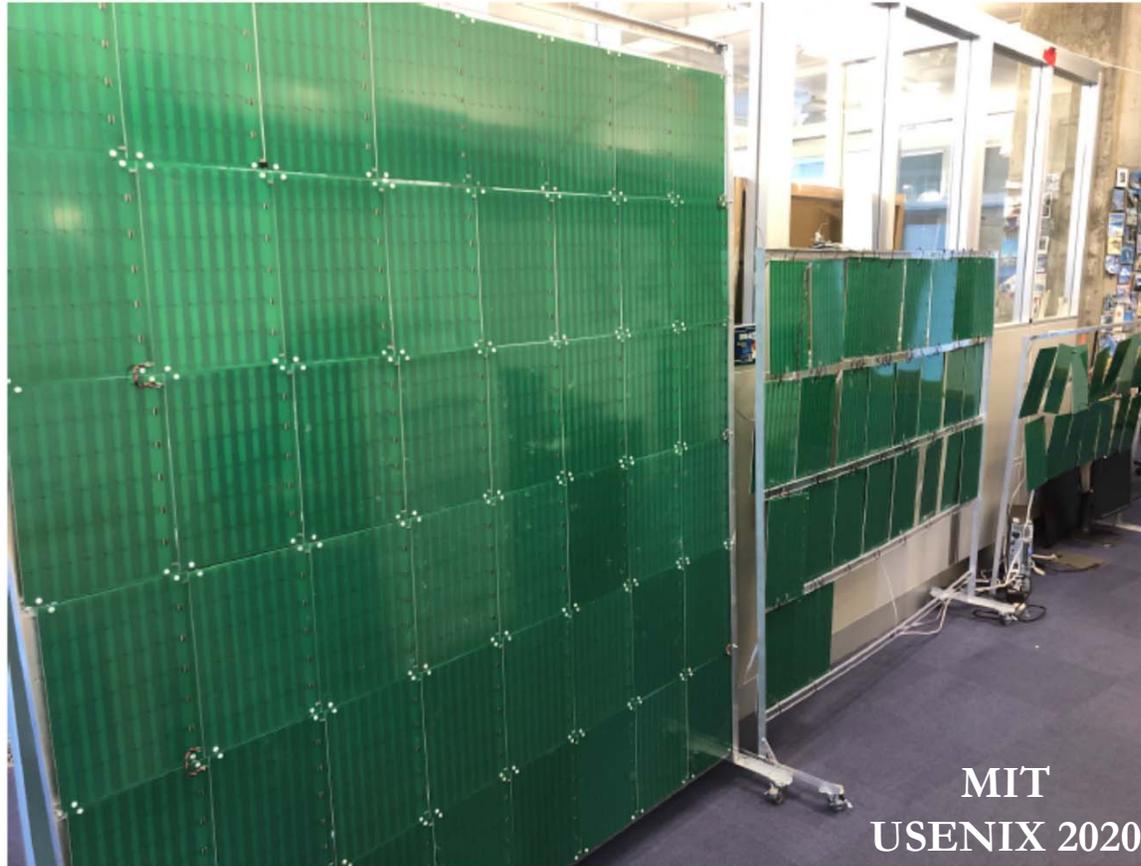
MARCO DI RENZO¹ (Fellow, IEEE), KONSTANTINOS NTONTIN² (Member, IEEE), JIAN SONG¹,
FADIL H. DANUFANE¹, XUEWEN QIAN¹, FOTIS LAZARAKIS², JULIEN DE ROSNY³,
DINH-THUY PHAN-HUY⁴ (Member, IEEE), OSVALDO SIMEONE⁵ (Fellow, IEEE),
RUI ZHANG⁶ (Fellow, IEEE), MEROAUNE DEBBAH⁷ (Fellow, IEEE), GEOFFROY LEROSEY⁸,
MATHIAS FINK³ (Member, IEEE), SERGEI TRETAKOV⁹ (Fellow, IEEE),
AND SHLOMO SHAMAI¹⁰ (Life Fellow, IEEE)

Nearly-Passive RISs: Advantages and Limitations

How Large/Big Can an RIS Be ?

Nearly-Passive RISs: Advantages and Limitations

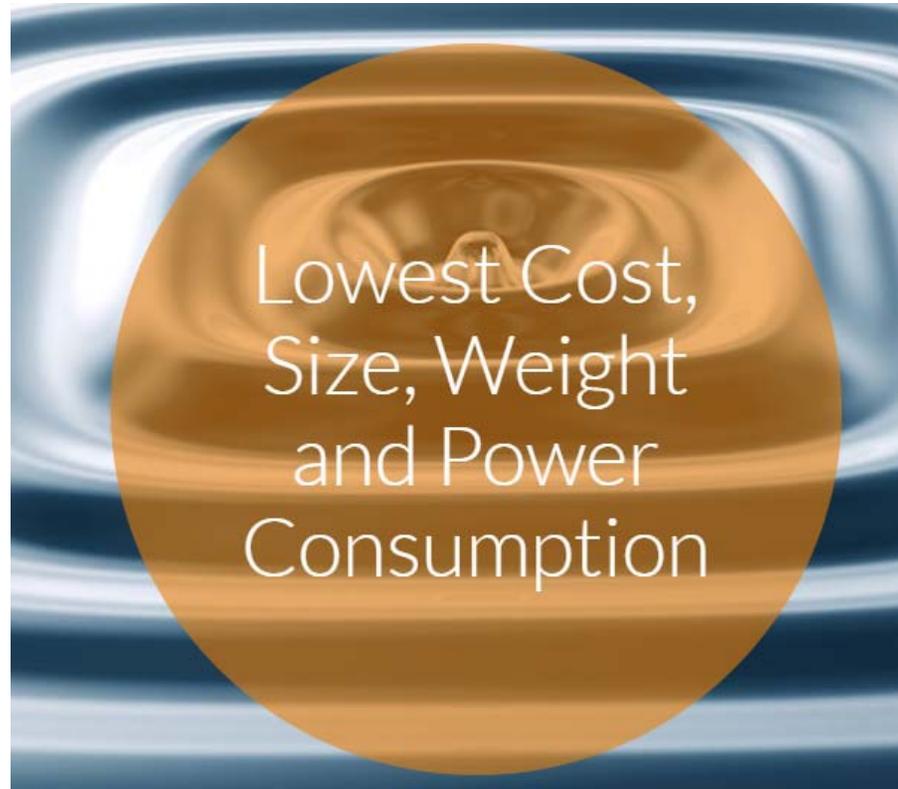
How Large/Big Can an RIS Be ?



“ Our prototype has **3,720 inexpensive antennas** (at scale, each of the antenna elements is on the order of a few cents or less) **on a 6 square-meter surface**. We believe this configuration may be the largest number of antennas ever used to improve communication links ” 141

Nearly-Passive RISs: Advantages and Limitations

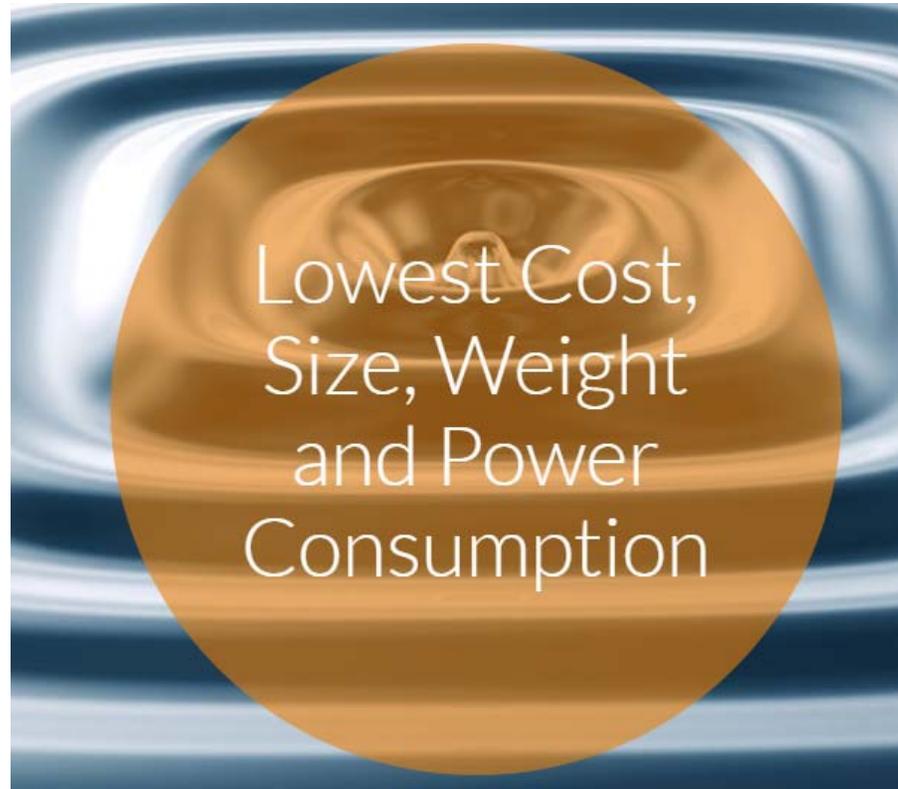
C-SWaP



For these reasons, RISs may constitute an emerging and promising **software-defined architecture that can be realized at reduced cost, size, weight, and power (C-SWaP design)**

Nearly-Passive RISs: Advantages and Limitations

C-SWaP



Sustainable wireless design (e.g., low EMF exposure) without generating new waves and possibly made of physically & aesthetically unobtrusive and recyclable material

Some Recent Results

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... from theory to simulations and experiments...

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- Joint Encoding – Capacity-Optimal Design (ISIT 2020)
 - M. Di Renzo et al., Beyond max-SNR: Joint Encoding for Reconfigurable Intelligent Surfaces ([arXiv:1911.09443](#))
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 - M. Di Renzo et al., Beamforming Through Reconfigurable Intelligent Surfaces in Single-User MIMO Systems: SNR Distribution and Scaling Laws in the Presence of Channel Fading and Phase Noise ([arXiv:2005.07472](#))
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- ... and many others on channel modeling, performance analysis, spectral & energy efficiency optimization, experiments...

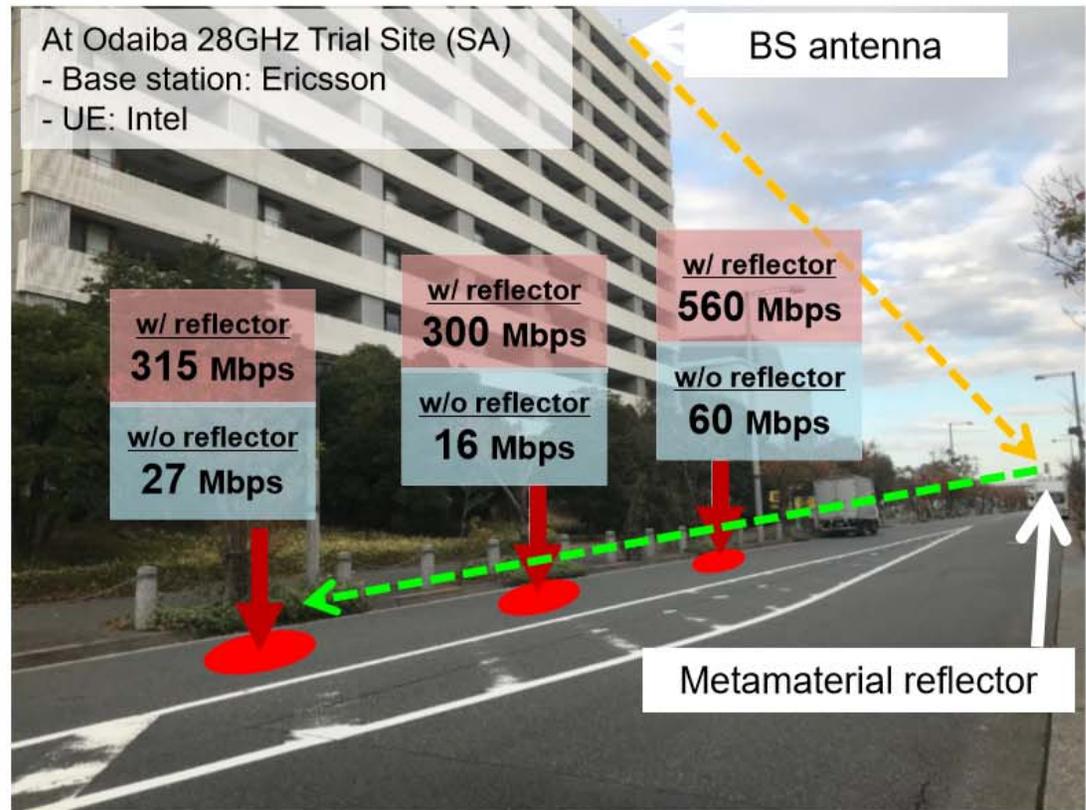
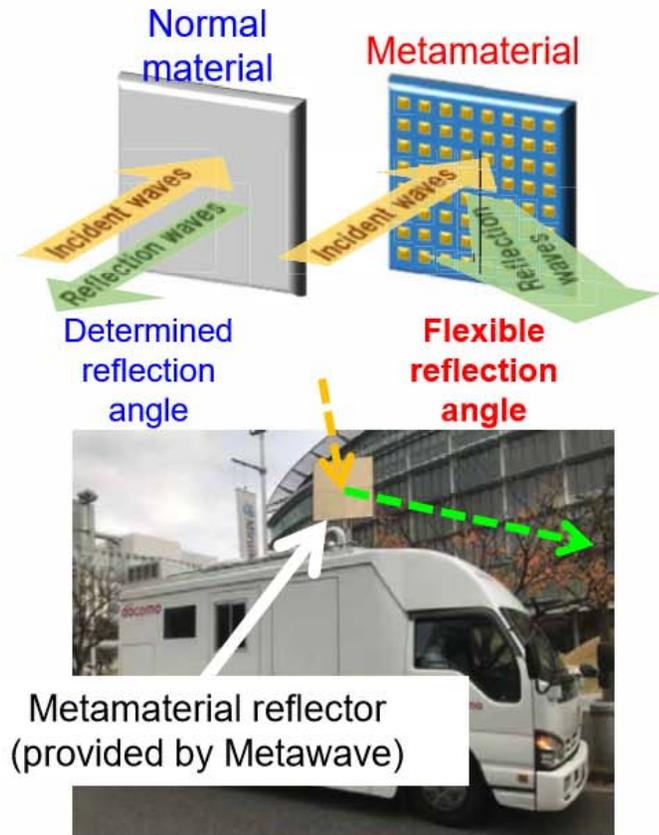
Some Recent Results

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RISs for Outdoor Coverage Enhancement (mmWave)

**RISs: Metasurfaces Spaced $< \lambda/2$
(DOCOMO & MetaWave, Jan. 2019)**



A Transparent Dynamic RIS (reflection/refraction)



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Press Release

January 17, 2020

DOCOMO Conducts World's First Successful Trial of Transparent Dynamic Metasurface

— Dynamic wave manipulation and high transparency expected to optimize 5G network construction —

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TOKYO, JAPAN, January 17, 2020 --- NTT DOCOMO, INC., working in collaboration with the global glass

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▶ **2020**

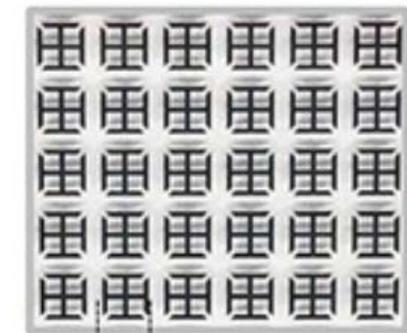
▶ [2019](#)

▶ [2018](#)

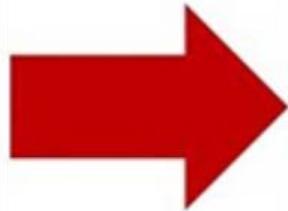
A Transparent Dynamic RIS (reflection/refraction)

**RISs: Metasurfaces Spaced $< \lambda/2$
(transparent and dynamic, Jan. 2020)**

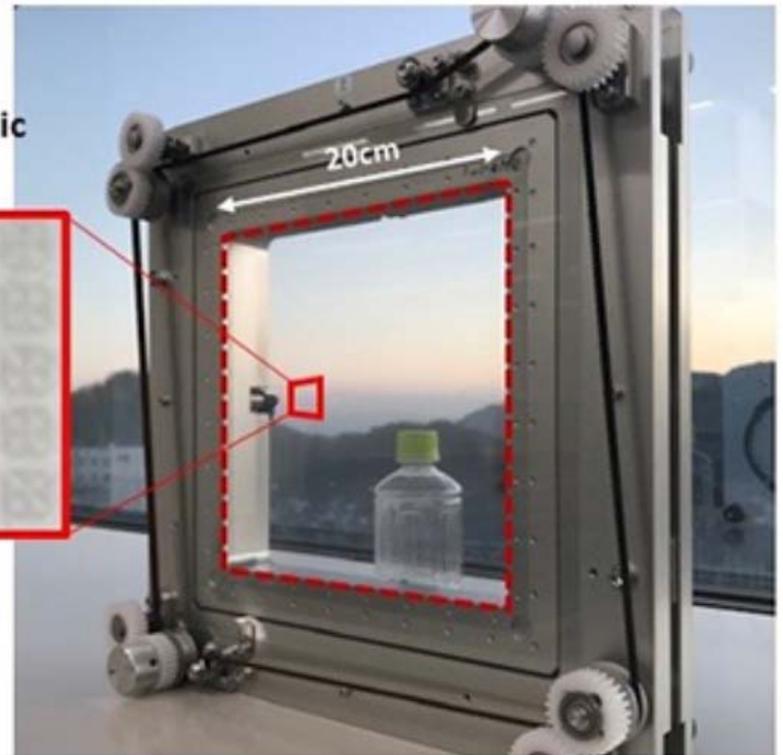
Conventional metasurface



Approx. 2mm



Prototype transparent dynamic metasurface

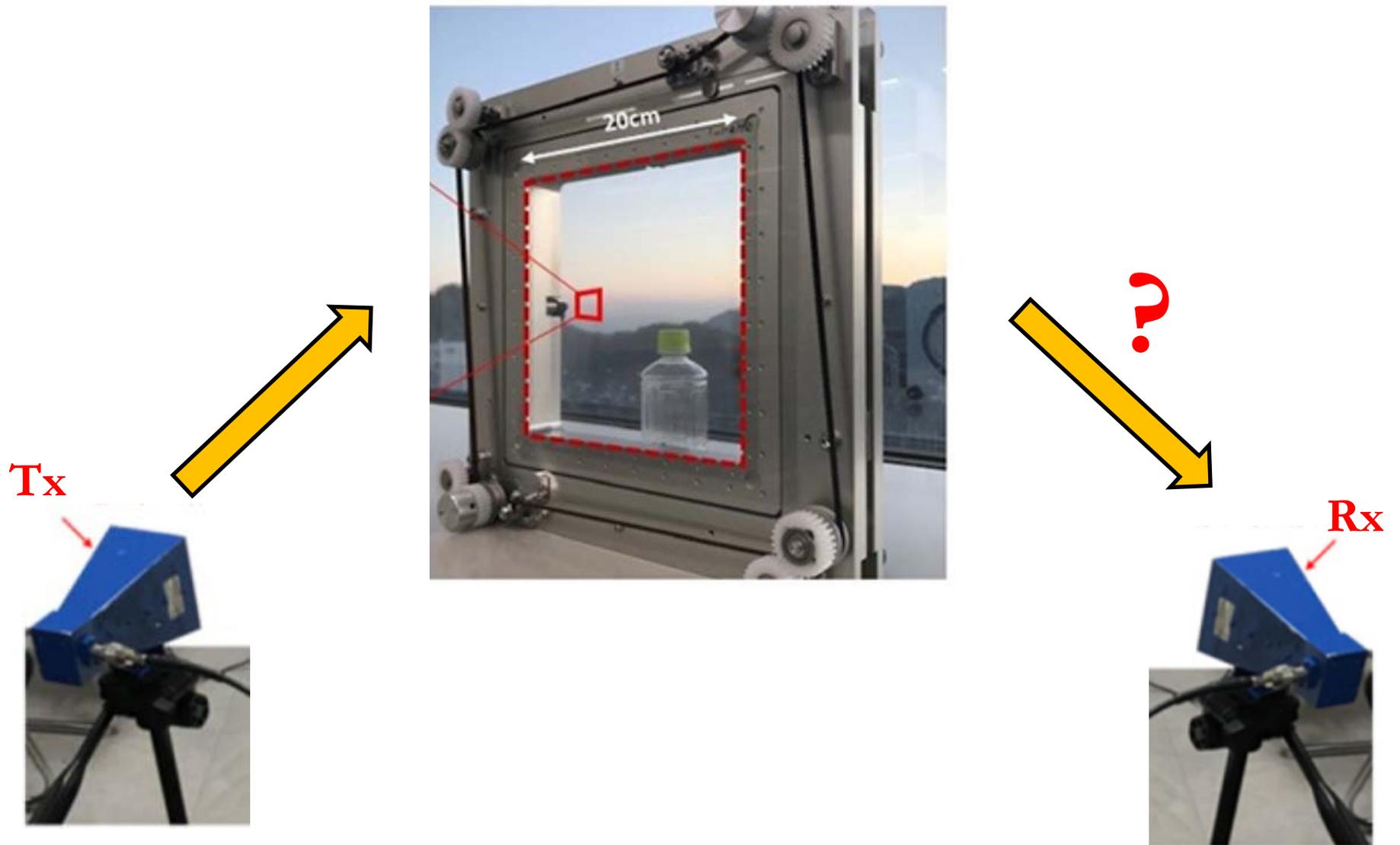


Prototype of transparent dynamic metasurface

RIS-Empowered Wireless Networks: Outdoors



What is the Power Scattered by an RIS ?

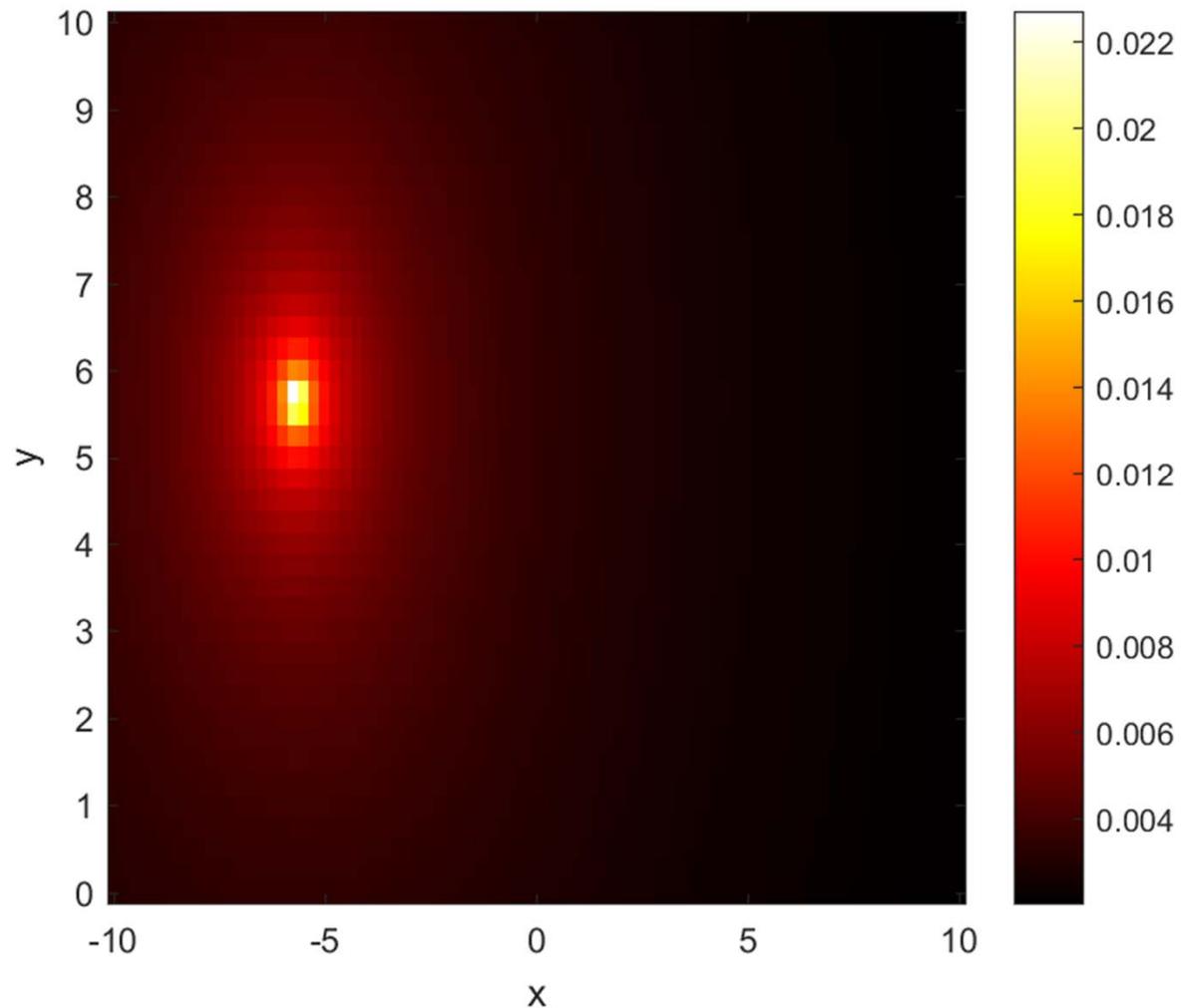


Path-Loss Modeling – Homogenized Metasurfaces

System Model

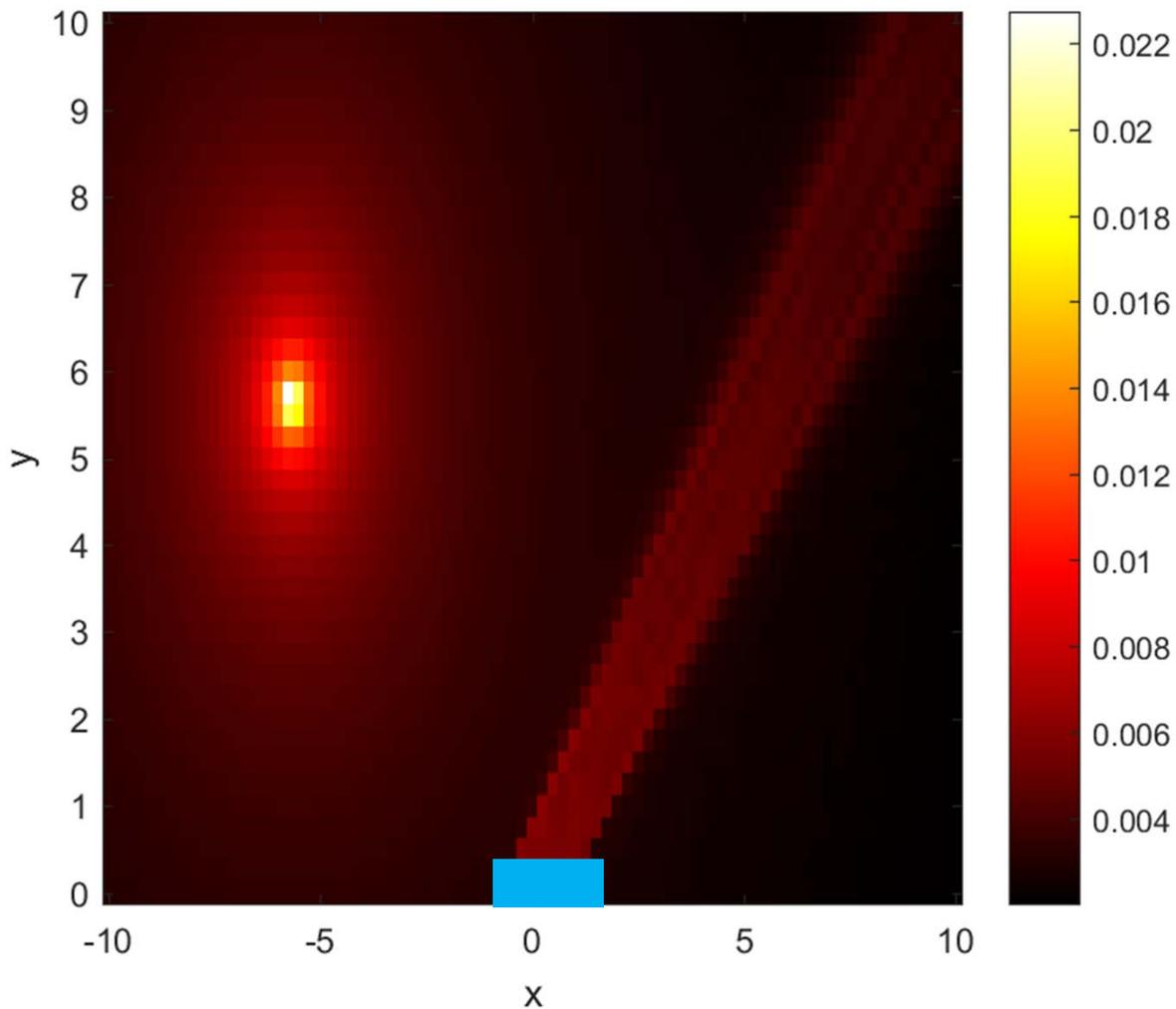
Path-Loss Modeling – Homogenized Metasurfaces

System Model (2D)



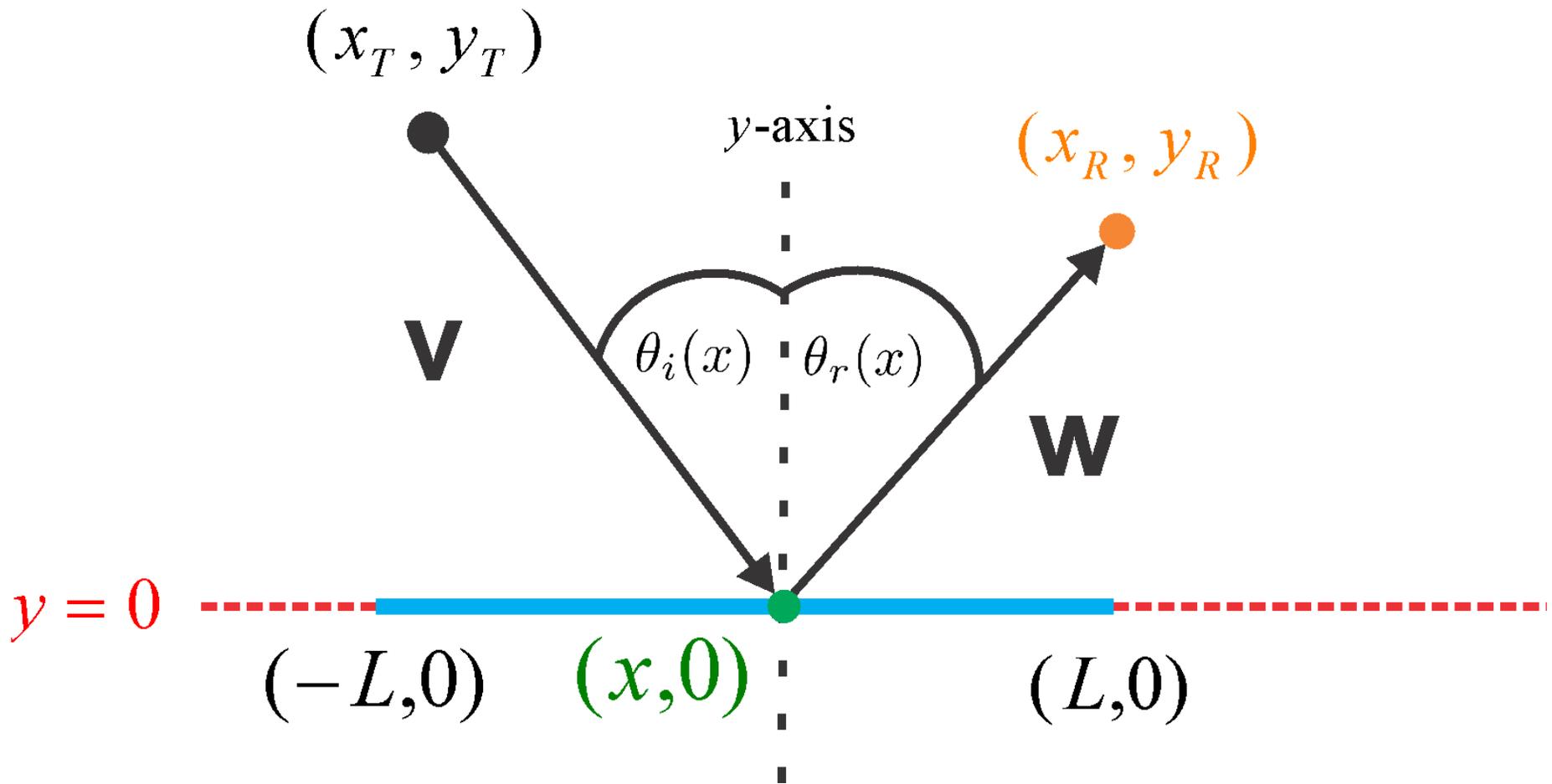
Path-Loss Modeling – Homogenized Metasurfaces

System Model (2D)

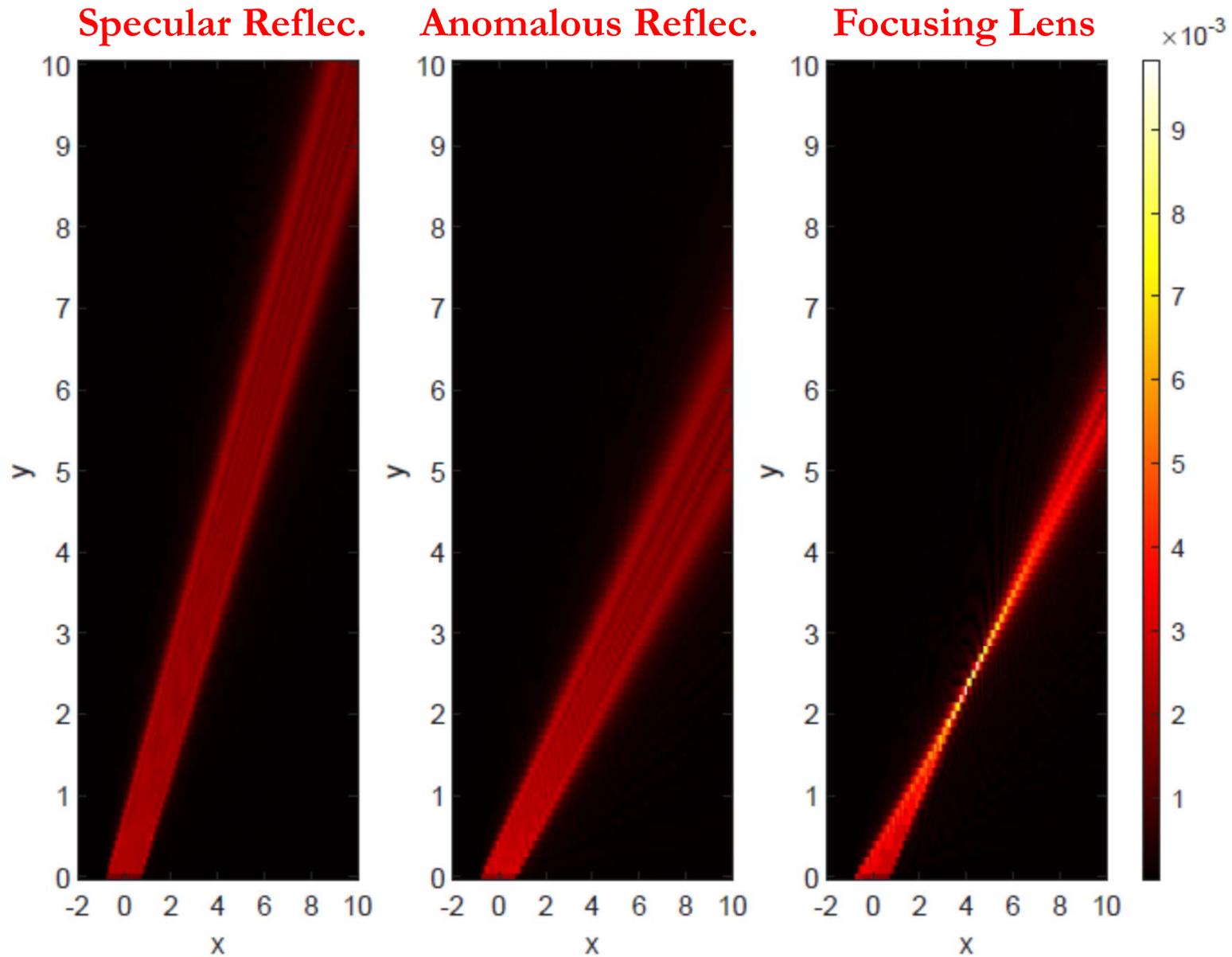


Path-Loss Modeling – Homogenized Metasurfaces

System Model (2D)

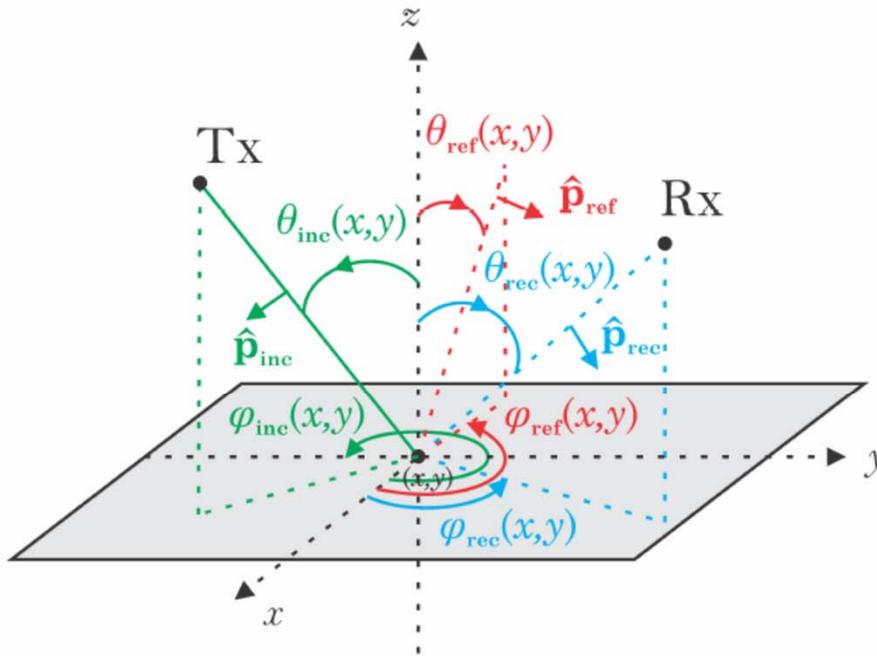


Path-Loss Modeling – Homogenized Metasurfaces

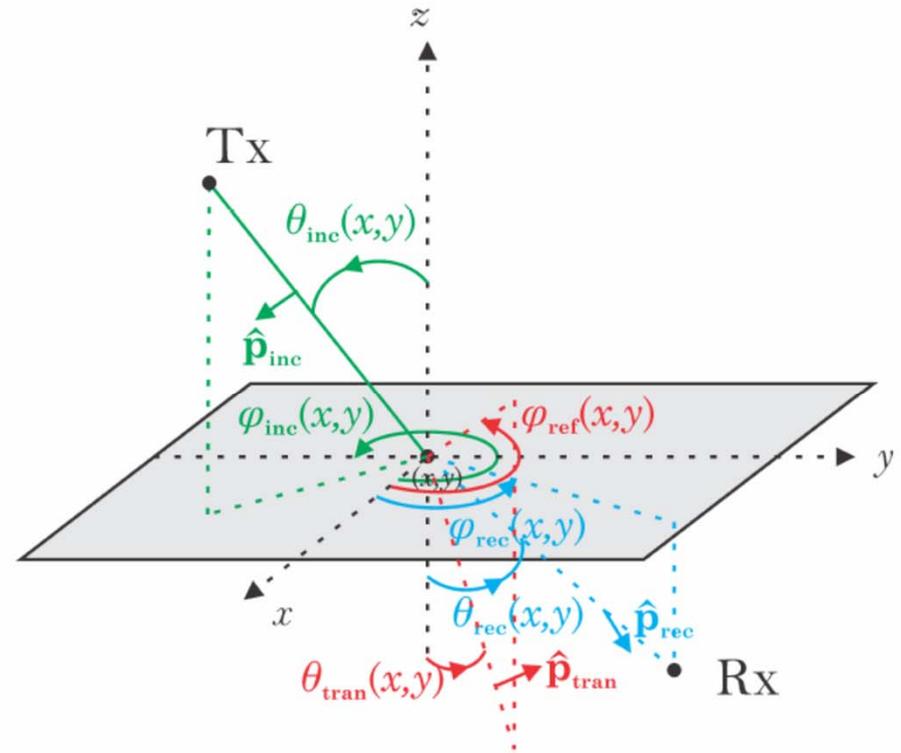


Path-Loss Modeling – Homogenized Metasurfaces

System Model (3D)

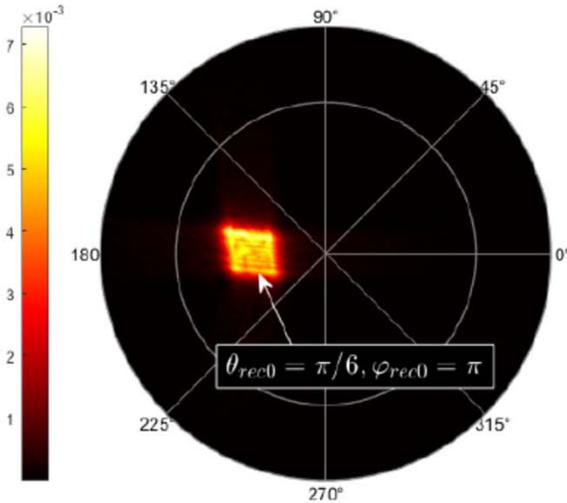


(a) Tx and Rx are on the same side of the surface.

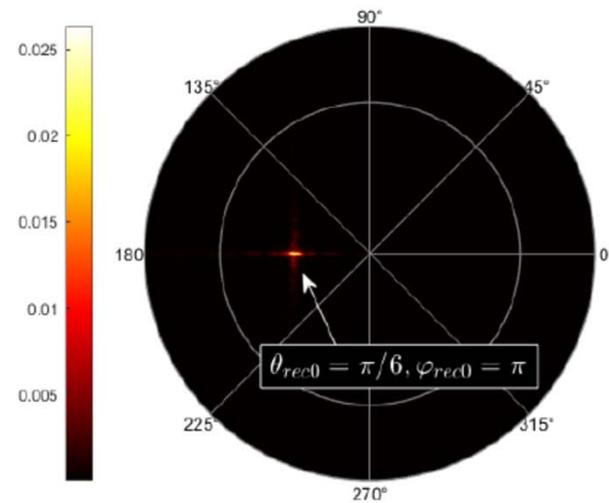


(b) Tx and Rx are on opposite sides of the surface.

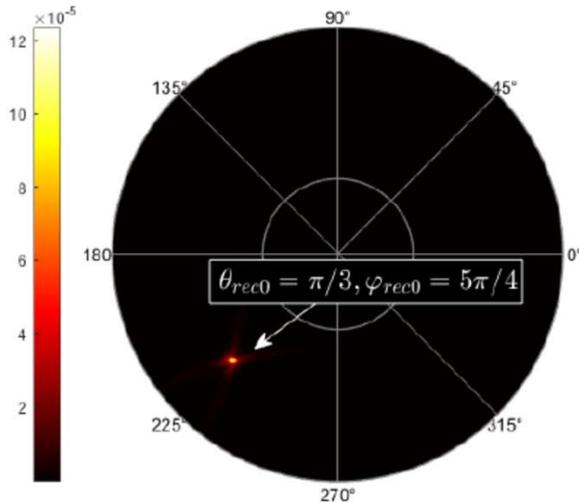
Path-Loss Modeling – Homogenized Metasurfaces



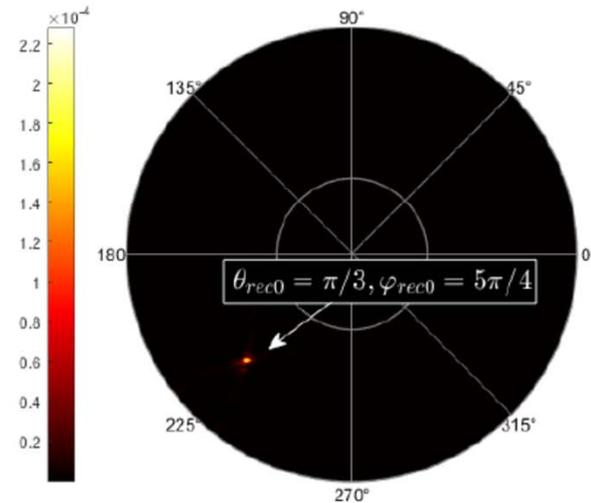
(a) Anomalous reflection, $d_{Tx0} = d_{Rx0} = 5$ m



(b) Focusing lens (reflection), $d_{Tx0} = d_{Rx0} = 5$ m



(c) Anomalous transmission, $d_{Tx0} = d_{Rx0} = 50$ m.



(d) Focusing lens (transmission), $d_{Tx0} = d_{Rx0} = 50$ m.

Path-Loss Modeling – Homogenized Metasurfaces

Main Theorem (TWC, under submission)

Proposition 1. Let $\hat{\mathbf{s}}_{(x,y)} = \sin \theta_{\text{inc}}(x, y) \cos \varphi_{\text{inc}}(x, y) \hat{\mathbf{x}} + \sin \theta_{\text{inc}}(x, y) \sin \varphi_{\text{inc}}(x, y) \hat{\mathbf{y}} + \cos \theta_{\text{inc}}(x, y) \hat{\mathbf{z}}$, be the unit-norm propagation vector from \mathbf{r}_{Tx} to $\mathbf{s} = x\hat{\mathbf{x}} + y\hat{\mathbf{y}} \in \mathcal{S}$. Define $\Omega_{\text{ref}}(x, y; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) = (k^2/\epsilon_0) p_{\text{dm}} (\tilde{\mathbf{p}}_{\text{rec}} \cdot \tilde{\mathbf{p}}_{\text{ref}} - (\hat{\mathbf{s}}_{(x,y)} \cdot \tilde{\mathbf{p}}_{\text{rec}}) (\hat{\mathbf{s}}_{(x,y)} \cdot \tilde{\mathbf{p}}_{\text{ref}})) \mathcal{E}(\hat{\mathbf{p}}_{\text{inc}}, \hat{\mathbf{p}}_{\text{ref}})$. Under the assumptions stated in Lemma 2, the electric field $\mathbf{E}(\mathbf{r}_{\text{Rx}})$ projected onto $\hat{\mathbf{p}}_{\text{rec}}$ can be formulated as follows:

$$\begin{aligned} \mathbf{E}(\mathbf{r}_{\text{Rx}}) \cdot \hat{\mathbf{p}}_{\text{rec}} &\approx \hat{\mathbf{p}}_{\text{rec}} \cdot \mathbf{E}_{0,\text{inc}}(\mathbf{r}_{\text{Rx}}; \hat{\mathbf{p}}_{\text{inc}}) G(\mathbf{r}_{\text{Rx}}, \mathbf{r}_{\text{Tx}}) \\ &+ \mathcal{I}_0 \int_{-L_y}^{L_y} \int_{-L_x}^{L_x} \mathcal{I}_R(x, y) e^{-jk\mathcal{P}_R(x,y)} dx dy \end{aligned} \quad (21)$$

where $\mathcal{I}_0 = jk/(16\pi^2)$, and the following shorthand notation is used:

$$\mathcal{P}_R(x, y) = d_{\text{Tx}}(x, y) + d_{\text{Rx}}(x, y) - (\phi_{\text{rec}} + \phi_{\text{ref}} + \angle \Gamma_{\text{ref}}(x, y))/k \quad (22)$$

$$\mathcal{I}_R(x, y) = \frac{|\Gamma_{\text{ref}}(x, y)| \Omega_{\text{ref}}(x, y; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}})}{d_{\text{Tx}}(x, y) d_{\text{Rx}}(x, y)} (\cos \theta_{\text{inc}}(x, y) + \cos \theta_{\text{rec}}(x, y)) \quad (23)$$

Path-Loss Modeling – Homogenized Metasurfaces

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$$\mathbf{E}(\mathbf{r}_{\text{Rx}}) \cdot \hat{\mathbf{p}}_{\text{rec}} \approx \hat{\mathbf{p}}_{\text{rec}} \cdot \mathbf{E}_{0,\text{inc}}(\mathbf{r}_{\text{Rx}}; \hat{\mathbf{p}}_{\text{inc}}) G(\mathbf{r}_{\text{Rx}}, \mathbf{r}_{\text{Tx}}) + \mathcal{I}_0 \int_{-L_y}^{L_y} \int_{-L_x}^{L_x} \mathcal{I}_R(x, y) e^{-jk\mathcal{P}_R(x,y)} dx dy \quad (21)$$

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$$\mathcal{I}_R(x, y) = \frac{|\Gamma_{\text{ref}}(x, y)| \Omega_{\text{ref}}(x, y; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}})}{d_{\text{Tx}}(x, y) d_{\text{Rx}}(x, y)} (\cos \theta_{\text{inc}}(x, y) + \cos \theta_{\text{rec}}(x, y)) \quad (23)$$

Path-Loss Modeling – Homogenized Metasurfaces

Main Theorem (TWC, under submission)

Proposition 1. Let $\hat{\mathbf{s}}_{(x,y)} = \sin \theta_{\text{inc}}(x, y) \cos \varphi_{\text{inc}}(x, y) \hat{\mathbf{x}} + \sin \theta_{\text{inc}}(x, y) \sin \varphi_{\text{inc}}(x, y) \hat{\mathbf{y}} + \cos \theta_{\text{inc}}(x, y) \hat{\mathbf{z}}$, be the unit-norm propagation vector from \mathbf{r}_{Tx} to $\mathbf{s} = x\hat{\mathbf{x}} + y\hat{\mathbf{y}} \in \mathcal{S}$. Define $\Omega_{\text{ref}}(x, y; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) = (k^2/\epsilon_0)p_{\text{dm}}(\tilde{\mathbf{p}}_{\text{rec}} \cdot \tilde{\mathbf{p}}_{\text{ref}} - (\hat{\mathbf{s}}_{(x,y)} \cdot \tilde{\mathbf{p}}_{\text{rec}})(\hat{\mathbf{s}}_{(x,y)} \cdot \tilde{\mathbf{p}}_{\text{ref}})) \mathcal{E}(\hat{\mathbf{p}}_{\text{inc}}, \hat{\mathbf{p}}_{\text{ref}})$. Under the assumptions stated in Lemma 2, the electric field $\mathbf{E}(\mathbf{r}_{\text{Rx}})$ projected onto $\hat{\mathbf{p}}_{\text{rec}}$ can be formulated as follows:

$$\begin{aligned} \mathbf{E}(\mathbf{r}_{\text{Rx}}) \cdot \hat{\mathbf{p}}_{\text{rec}} &\approx \hat{\mathbf{p}}_{\text{rec}} \cdot \mathbf{E}_{0,\text{inc}}(\mathbf{r}_{\text{Rx}}; \hat{\mathbf{p}}_{\text{inc}}) G(\mathbf{r}_{\text{Rx}}, \mathbf{r}_{\text{Tx}}) \\ &+ \mathcal{I}_0 \int_{-L_y}^{L_y} \int_{-L_x}^{L_x} \mathcal{I}_R(x, y) e^{-jk\mathcal{P}_R(x,y)} dx dy \end{aligned} \quad (21)$$

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$$\begin{aligned} \mathbf{E}(\mathbf{r}_{\text{Rx}}) \cdot \hat{\mathbf{p}}_{\text{rec}} &\approx \hat{\mathbf{p}}_{\text{rec}} \cdot \mathbf{E}_{0,\text{inc}}(\mathbf{r}_{\text{Rx}}; \hat{\mathbf{p}}_{\text{inc}}) G(\mathbf{r}_{\text{Rx}}, \mathbf{r}_{\text{Tx}}) \\ &+ \mathcal{I}_0 \int_{-L_y}^{L_y} \int_{-L_x}^{L_x} \mathcal{I}_R(x, y) e^{-jk\mathcal{P}_R(x,y)} dx dy \end{aligned} \quad (21)$$

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Path-Loss Modeling – Homogenized Metasurfaces

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$$\begin{aligned} \mathbf{E}(\mathbf{r}_{\text{Rx}}) \cdot \hat{\mathbf{p}}_{\text{rec}} &\approx \hat{\mathbf{p}}_{\text{rec}} \cdot \mathbf{E}_{0,\text{inc}}(\mathbf{r}_{\text{Rx}}; \hat{\mathbf{p}}_{\text{inc}}) G(\mathbf{r}_{\text{Rx}}, \mathbf{r}_{\text{Tx}}) \\ &+ \mathcal{I}_0 \int_{-L_y}^{L_y} \int_{-L_x}^{L_x} \mathcal{I}_R(x, y) e^{-jk\mathcal{P}_R(x,y)} dx dy \end{aligned} \quad (21)$$

where $\mathcal{I}_0 = jk/(16\pi^2)$, and the following shorthand notation is used:

$$\mathcal{P}_R(x, y) = d_{\text{Tx}}(x, y) + d_{\text{Rx}}(x, y) - (\phi_{\text{rec}} + \phi_{\text{ref}} + \angle \Gamma_{\text{ref}}(x, y))/k \quad (22)$$

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Path-Loss Modeling – Homogenized Metasurfaces

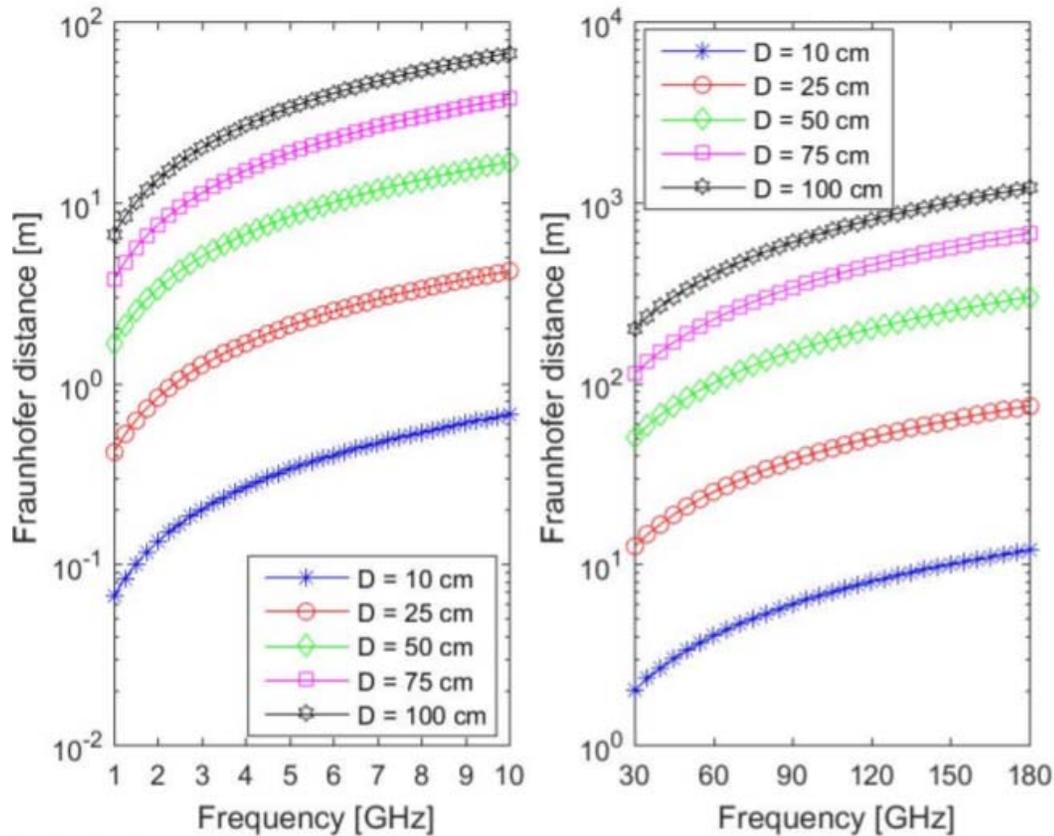
Electrically-Large (near-field) vs. Electrically-Small (far-field)

Path-Loss Modeling – Homogenized Metasurfaces

Electrically-Large (near-field) vs. Electrically-Small (far-field)

$$d_F = 4D^2/\lambda$$

Fraunhofer distance (d_F)

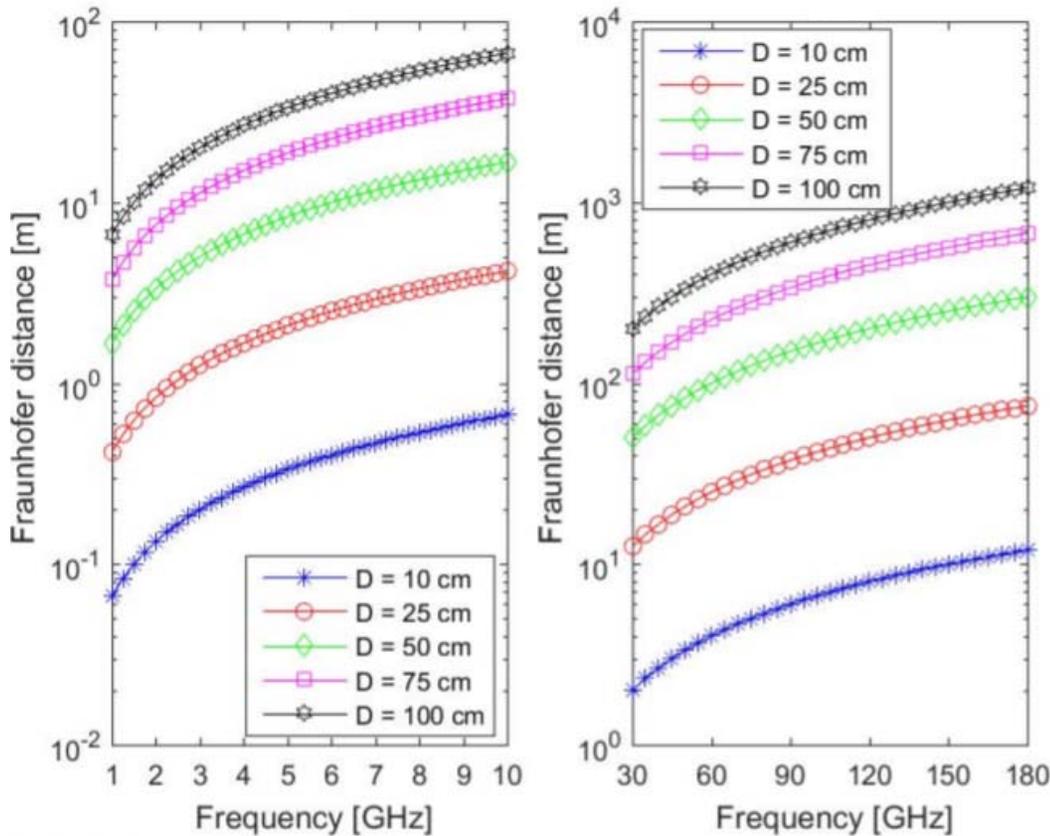


Path-Loss Modeling – Homogenized Metasurfaces

Electrically-Large (near-field) vs. Electrically-Small (far-field)

$$d_F = 4D^2/\lambda$$

Fraunhofer distance (d_F)



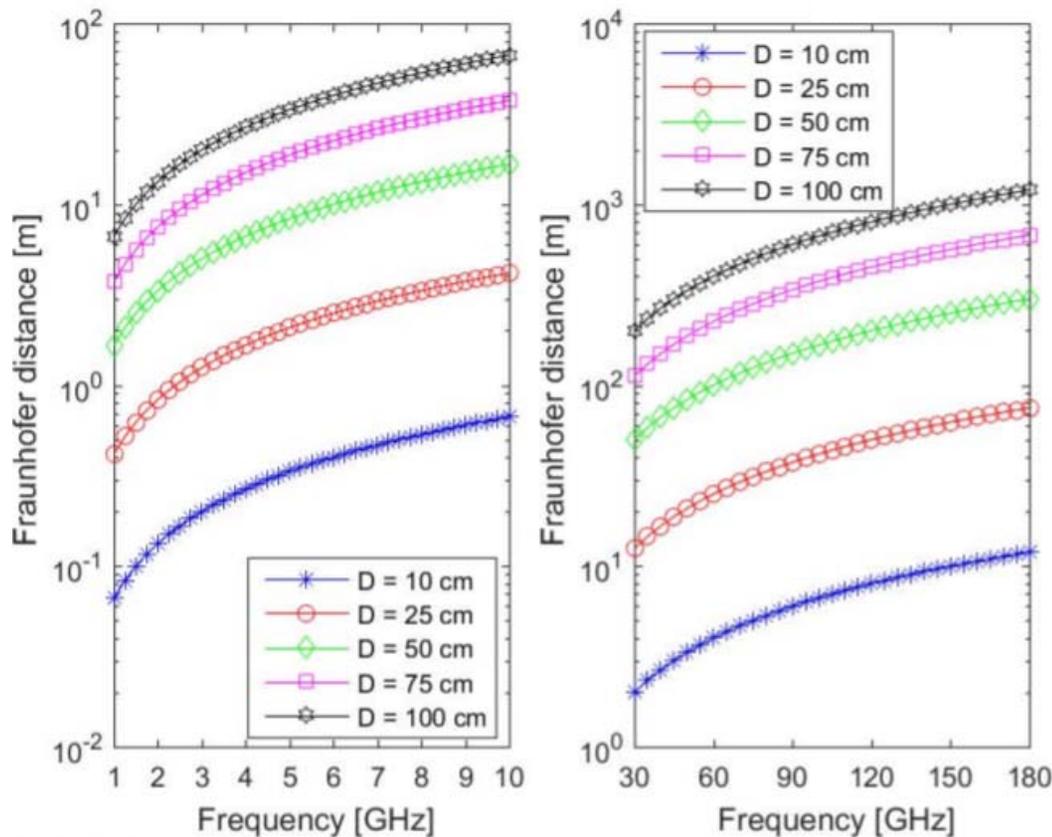
- 0.1x0.1 m² RIS @ 6 GHz
→ 0.8 m
- 1.0x1.0 m² RIS @ 6 GHz
→ 80 m
- 6 m² RIS @ 6 GHz
→ 480 m

Path-Loss Modeling – Homogenized Metasurfaces

Electrically-Large (near-field) vs. Electrically-Small (far-field)

$$d_F = 4D^2/\lambda$$

Fraunhofer distance (d_F)



□ 0.1x0.1 m² RIS @ 6 GHz
→ 0.8 m

□ 1.0x1.0 m² RIS @ 6 GHz
→ 80 m

□ 6 m² RIS @ 6 GHz
→ 480 m

□ 0.1x0.1 m² RIS @ 60 GHz
→ 8 m

□ 1.0x1.0 m² RIS @ 60 GHz
→ 800 m

Path-Loss Modeling – Anomalous Reflection

Electrically-Large vs. Electrically-Small

Path-Loss Modeling – Anomalous Reflection

Electrically-Large vs. Electrically-Small

Corollary 4. Consider $\zeta'_1 > 0$, $\zeta'_2 > 0$. Define $K_1 = (\mathcal{R}_1\zeta'_1 + \frac{1}{2}\mathcal{R}_3\zeta'_2)/\sqrt{\mathcal{R}_1\zeta'_1{}^2 + \mathcal{R}_2\zeta'_2{}^2 + \mathcal{R}_3\zeta'_1\zeta'_2}$, $K_2 = (\mathcal{R}_2\zeta'_2 + \frac{1}{2}\mathcal{R}_3\zeta'_1)/\sqrt{\mathcal{R}_1\zeta'_1{}^2 + \mathcal{R}_2\zeta'_2{}^2 + \mathcal{R}_3\zeta'_1\zeta'_2}$. Then, (29) can be approximated as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{|\Gamma_{\text{ref}}(x_s, y_s)| \Omega_{\text{ref}}(x_s, y_s; \hat{\mathbf{P}}_{\text{ref}}, \hat{\mathbf{P}}_{\text{rec}})}{8\pi(K_1 d_{\text{Tx}}(x_s, y_s) + K_2 d_{\text{Rx}}(x_s, y_s))} e^{-jk(d_{\text{Tx}}(x_s, y_s) + d_{\text{Rx}}(x_s, y_s) - (\alpha_R x_s + \beta_R y_s) - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)}$$

Path-Loss Modeling – Anomalous Reflection

Electrically-Large vs. Electrically-Small

Corollary 5. *In the electrically-small regime, $F_R(\mathbf{r}_{\text{Rx}})$ can be approximated as follows:*

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{jk\Omega_{\text{ref}}(0, 0; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) (\cos \theta_{\text{inc}0} + \cos \theta_{\text{rec}0})}{16\pi^2 d_{\text{Tx}0} d_{\text{Rx}0}} e^{-jk(d_{\text{Tx}0} + d_{\text{Rx}0} - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)} \quad (31)$$

$$\int_{-L_y}^{L_y} \int_{-L_x}^{L_x} |\Gamma_{\text{ref}}(x, y)| e^{jk(\mathcal{D}_{\alpha_R} x + \mathcal{D}_{\beta_R} y)} dx dy$$

where the shorthand notation $\mathcal{D}_{\alpha_R} = \alpha_R + \mathcal{D}_x$ and $\mathcal{D}_{\beta_R} = \beta_R + \mathcal{D}_y$ is used. If $|\Gamma_{\text{ref}}(x, y)| = \Gamma_{\text{ref}} > 0$ for $(x, y) \in \mathcal{S}$, then $F_R(\mathbf{r}_{\text{Rx}})$ can be further simplified as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{jk\Gamma_{\text{ref}}\Omega_{\text{ref}}(0, 0; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) L_x L_y (\cos \theta_{\text{inc}0} + \cos \theta_{\text{rec}0})}{4\pi^2 d_{\text{Tx}0} d_{\text{Rx}0}} \text{sinc}(kL_x \mathcal{D}_{\alpha_R}) \text{sinc}(kL_y \mathcal{D}_{\beta_R}) e^{-jk(d_{\text{Tx}0} + d_{\text{Rx}0} - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)} \quad (32) \mathbf{1}$$

Path-Loss Modeling – Anomalous Reflection

Electrically-Large (4) vs. Electrically-Small (5)

Corollary 4. Consider $\zeta'_1 > 0$, $\zeta'_2 > 0$. Define $K_1 = (\mathcal{R}_1\zeta'_1 + \frac{1}{2}\mathcal{R}_3\zeta'_2)/\sqrt{\mathcal{R}_1\zeta'_1{}^2 + \mathcal{R}_2\zeta'_2{}^2 + \mathcal{R}_3\zeta'_1\zeta'_2}$, $K_2 = (\mathcal{R}_2\zeta'_2 + \frac{1}{2}\mathcal{R}_3\zeta'_1)/\sqrt{\mathcal{R}_1\zeta'_1{}^2 + \mathcal{R}_2\zeta'_2{}^2 + \mathcal{R}_3\zeta'_1\zeta'_2}$. Then, (29) can be approximated as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{|\Gamma_{\text{ref}}(x_s, y_s)| \Omega_{\text{ref}}(x_s, y_s; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}})}{8\pi(K_1 d_{\text{Tx}}(x_s, y_s) + K_2 d_{\text{Rx}}(x_s, y_s))} e^{-jk(d_{\text{Tx}}(x_s, y_s) + d_{\text{Rx}}(x_s, y_s) - (\alpha_R x_s + \beta_R y_s) - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)}$$

Corollary 5. In the electrically-small regime, $F_R(\mathbf{r}_{\text{Rx}})$ can be approximated as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{jk\Omega_{\text{ref}}(0, 0; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) (\cos \theta_{\text{inc}0} + \cos \theta_{\text{rec}0})}{16\pi^2 d_{\text{Tx}0} d_{\text{Rx}0}} e^{-jk(d_{\text{Tx}0} + d_{\text{Rx}0} - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)} \quad (31)$$

$$\int_{-L_y}^{L_y} \int_{-L_x}^{L_x} |\Gamma_{\text{ref}}(x, y)| e^{jk(\mathcal{D}_{\alpha_R} x + \mathcal{D}_{\beta_R} y)} dx dy$$

where the shorthand notation $\mathcal{D}_{\alpha_R} = \alpha_R + \mathcal{D}_x$ and $\mathcal{D}_{\beta_R} = \beta_R + \mathcal{D}_y$ is used. If $|\Gamma_{\text{ref}}(x, y)| = \Gamma_{\text{ref}} > 0$ for $(x, y) \in \mathcal{S}$, then $F_R(\mathbf{r}_{\text{Rx}})$ can be further simplified as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{jk\Gamma_{\text{ref}}\Omega_{\text{ref}}(0, 0; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) L_x L_y (\cos \theta_{\text{inc}0} + \cos \theta_{\text{rec}0})}{4\pi^2 d_{\text{Tx}0} d_{\text{Rx}0}} \text{sinc}(kL_x \mathcal{D}_{\alpha_R}) \text{sinc}(kL_y \mathcal{D}_{\beta_R}) e^{-jk(d_{\text{Tx}0} + d_{\text{Rx}0} - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)} \quad (32) \quad 2$$

Path-Loss Modeling – Anomalous Reflection

Electrically-Large (4) vs. Electrically-Small (5)

Corollary 4. Consider $\zeta'_1 > 0$, $\zeta'_2 > 0$. Define $K_1 = (\mathcal{R}_1\zeta'_1 + \frac{1}{2}\mathcal{R}_3\zeta'_2)/\sqrt{\mathcal{R}_1\zeta'_1{}^2 + \mathcal{R}_2\zeta'_2{}^2 + \mathcal{R}_3\zeta'_1\zeta'_2}$, $K_2 = (\mathcal{R}_2\zeta'_2 + \frac{1}{2}\mathcal{R}_3\zeta'_1)/\sqrt{\mathcal{R}_1\zeta'_1{}^2 + \mathcal{R}_2\zeta'_2{}^2 + \mathcal{R}_3\zeta'_1\zeta'_2}$. Then, (29) can be approximated as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{|\Gamma_{\text{ref}}(x_s, y_s)| \Omega_{\text{ref}}(x_s, y_s; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}})}{8\pi(K_1 d_{\text{Tx}}(x_s, y_s) + K_2 d_{\text{Rx}}(x_s, y_s))} e^{-jk(d_{\text{Tx}}(x_s, y_s) + d_{\text{Rx}}(x_s, y_s) - (\alpha_R x_s + \beta_R y_s) - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)}$$

Corollary 5. In the electrically-small regime, $F_R(\mathbf{r}_{\text{Rx}})$ can be approximated as follows:

$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{jk\Omega_{\text{ref}}(0, 0; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}}) (\cos \theta_{\text{inc}0} + \cos \theta_{\text{rec}0})}{16\pi^2 d_{\text{Tx}0} d_{\text{Rx}0}} e^{-jk(d_{\text{Tx}0} + d_{\text{Rx}0} - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)} \quad (31)$$

$$\int_{-L_y}^{L_y} \int_{-L_x}^{L_x} |\Gamma_{\text{ref}}(x, y)| e^{jk(\mathcal{D}_{\alpha_R} x + \mathcal{D}_{\beta_R} y)} dx dy$$

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Path-Loss Modeling – Anomalous Reflection

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$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{|\Gamma_{\text{ref}}(x_s, y_s)| \Omega_{\text{ref}}(x_s, y_s; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}})}{8\pi(K_1 d_{\text{Tx}}(x_s, y_s) + K_2 d_{\text{Rx}}(x_s, y_s))} e^{-jk(d_{\text{Tx}}(x_s, y_s) + d_{\text{Rx}}(x_s, y_s) - (\alpha_R x_s + \beta_R y_s) - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)}$$

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$$\int_{-L_y}^{L_y} \int_{-L_x}^{L_x} |\Gamma_{\text{ref}}(x, y)| e^{jk(\mathcal{D}_{\alpha_R} x + \mathcal{D}_{\beta_R} y)} dx dy$$

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Path-Loss Modeling – Anomalous Reflection

Electrically-Large (4) vs. Electrically-Small (5)

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$$F_R(\mathbf{r}_{\text{Rx}}) \approx \frac{|\Gamma_{\text{ref}}(x_s, y_s)| \Omega_{\text{ref}}(x_s, y_s; \hat{\mathbf{p}}_{\text{ref}}, \hat{\mathbf{p}}_{\text{rec}})}{8\pi(K_1 d_{\text{Tx}}(x_s, y_s) + K_2 d_{\text{Rx}}(x_s, y_s))} e^{-jk(d_{\text{Tx}}(x_s, y_s) + d_{\text{Rx}}(x_s, y_s) - (\alpha_R x_s + \beta_R y_s) - (\phi_0 + \phi_{\text{ref}} + \phi_{\text{rec}})/k)}$$

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Path-Loss Modeling – Anomalous Reflection

On the Path-Loss of Reconfigurable Intelligent Surfaces

F. H. Danufane, M. Di Renzo, *Fellow, IEEE*, J. de Rosny, and S. Tretyakov, *Fellow, IEEE*

Abstract

In this paper, we introduce a physics-based analytical characterization of the free-space path-loss of a wireless link in the presence of a reconfigurable intelligent surface. The obtained path-loss model can be applied to two-dimensional homogenized metasurfaces, which are made of sub-wavelength scattering elements and that operate either in reflection or transmission mode. The path-loss is formulated in terms of a computable integral that depends on the transmission distances, the polarization of the radio waves, the size of the surface, and the desired surface transformation. Closed-form expressions are obtained in two asymptotic regimes that are representative of far-field and near-field transmissions. Based on the proposed approach, the impact of several design parameters and operating regimes is unveiled.

... in submission ...

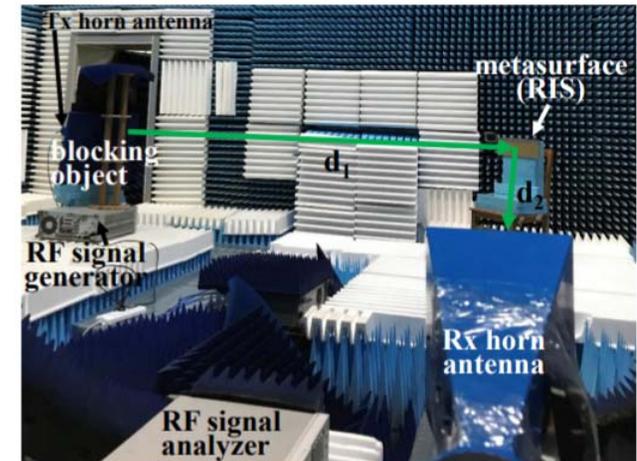
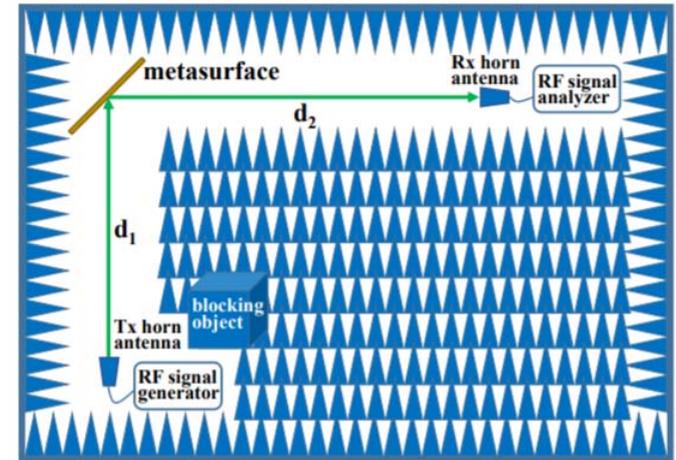
Experimental Validation (joint with Southeast Univ.)

Wireless Communications with Reconfigurable Intelligent Surface: Path Loss Modeling and Experimental Measurement

Wankai Tang, Ming Zheng Chen, Xiangyu Chen, Jun Yan Dai, Yu Han, Marco Di Renzo, Yong Zeng, Shi Jin, Qiang Cheng, and Tie Jun Cui

Abstract

Reconfigurable intelligent surfaces (RISs) comprised of tunable unit cells have recently drawn significant attentions due to their superior capability in manipulating electromagnetic waves. In particular, RIS-assisted wireless communications have the great potential to achieve significant performance improvement and coverage enhancement in a cost-effective and energy-efficient manner, by properly programming the reflection coefficients of the unit cells of RISs. In this paper, the free-space path loss models of RIS-assisted wireless communications are developed for different scenarios by studying the physics and electromagnetic nature of RISs. The proposed models, which are first validated through extensive simulation results, reveal the relationships between the free-space path loss of RIS-assisted wireless communications and the distances from the transmitter/receiver to the RIS, the size of the RIS, the near-field/far-field effects of the RIS, and the radiation patterns of antennas and unit cells. In addition, three fabricated RISs (metasurfaces) are utilized to further corroborate theoretical findings through experimental measurements conducted in a microwave anechoic chamber. The measurement results match well with the modeling results, thus validating the proposed free-space path loss models for RIS, which may pave the way for further theoretical studies and practical applications in this field.



arXiv:1911.05326

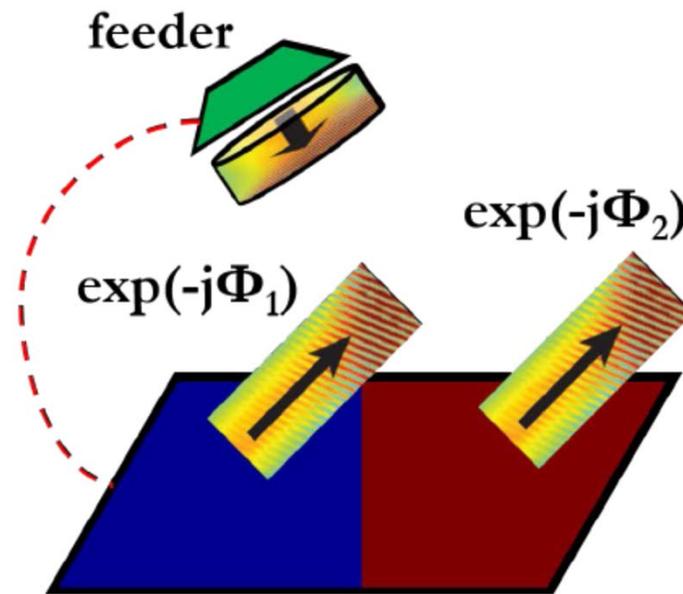
Some Recent Results

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Joint Encoding for RISs

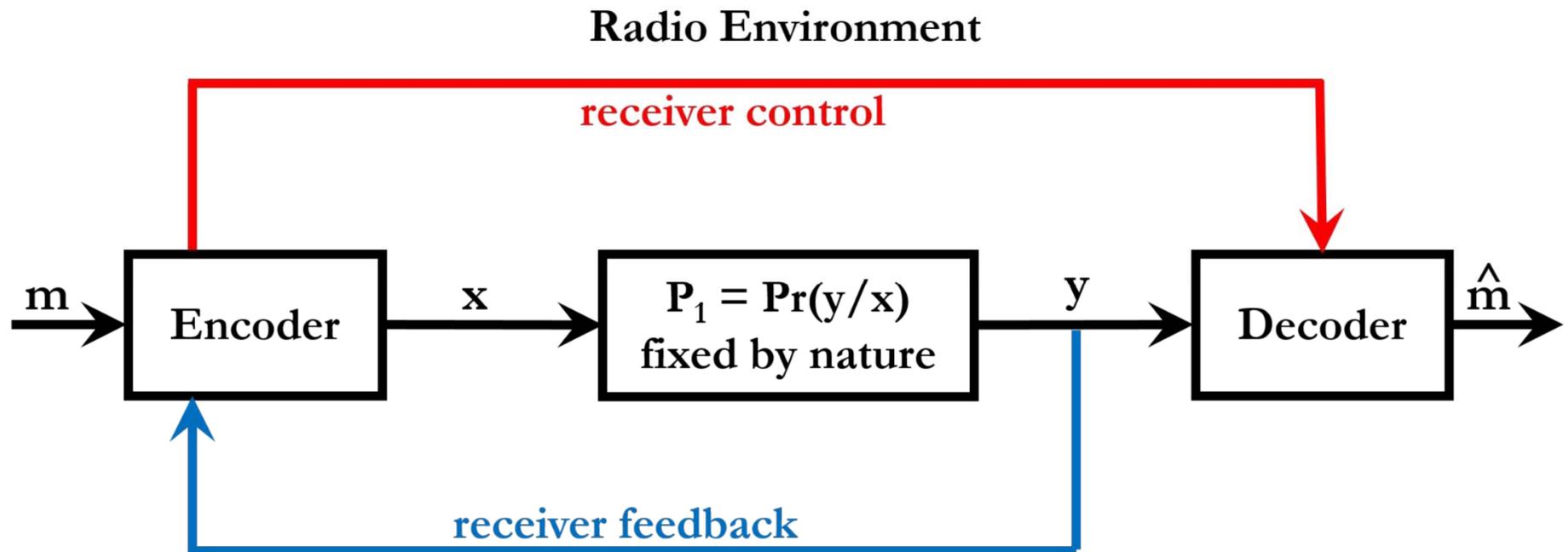
Rethinking Communication-Theoretic Models



Joint Encoding &
Single-RF Transmitter

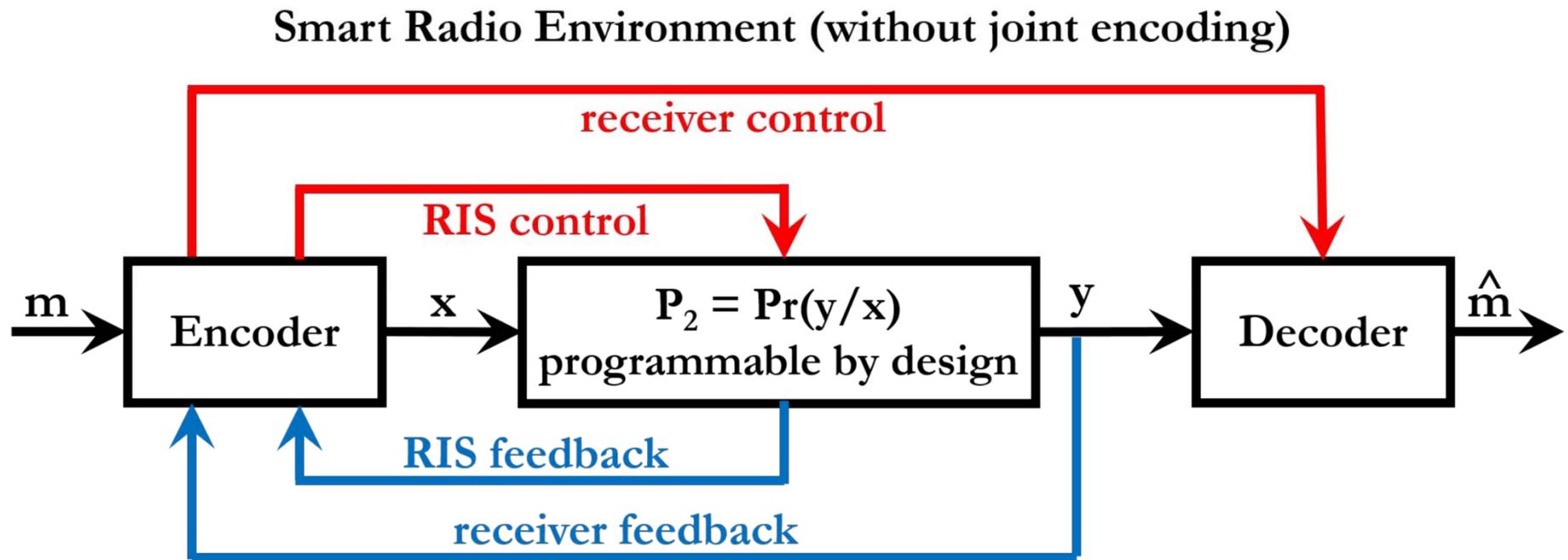
Joint Encoding for RISs

Rethinking Communication-Theoretic Models



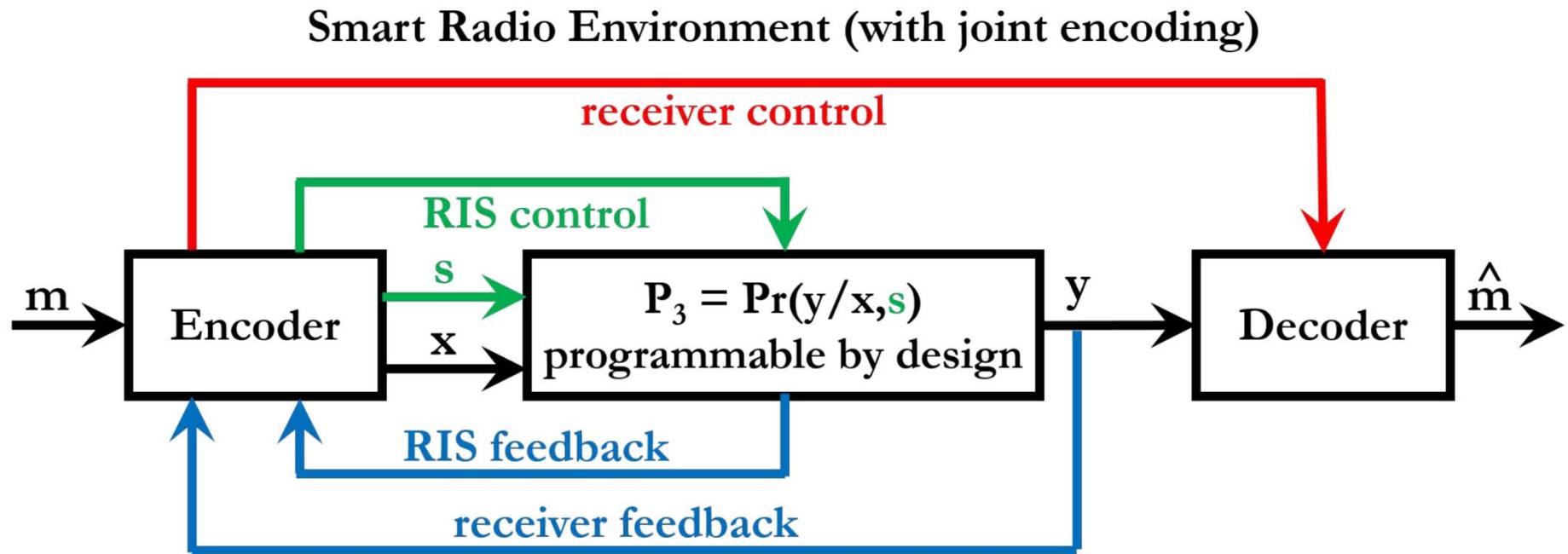
Joint Encoding for RISs

Rethinking Communication-Theoretic Models



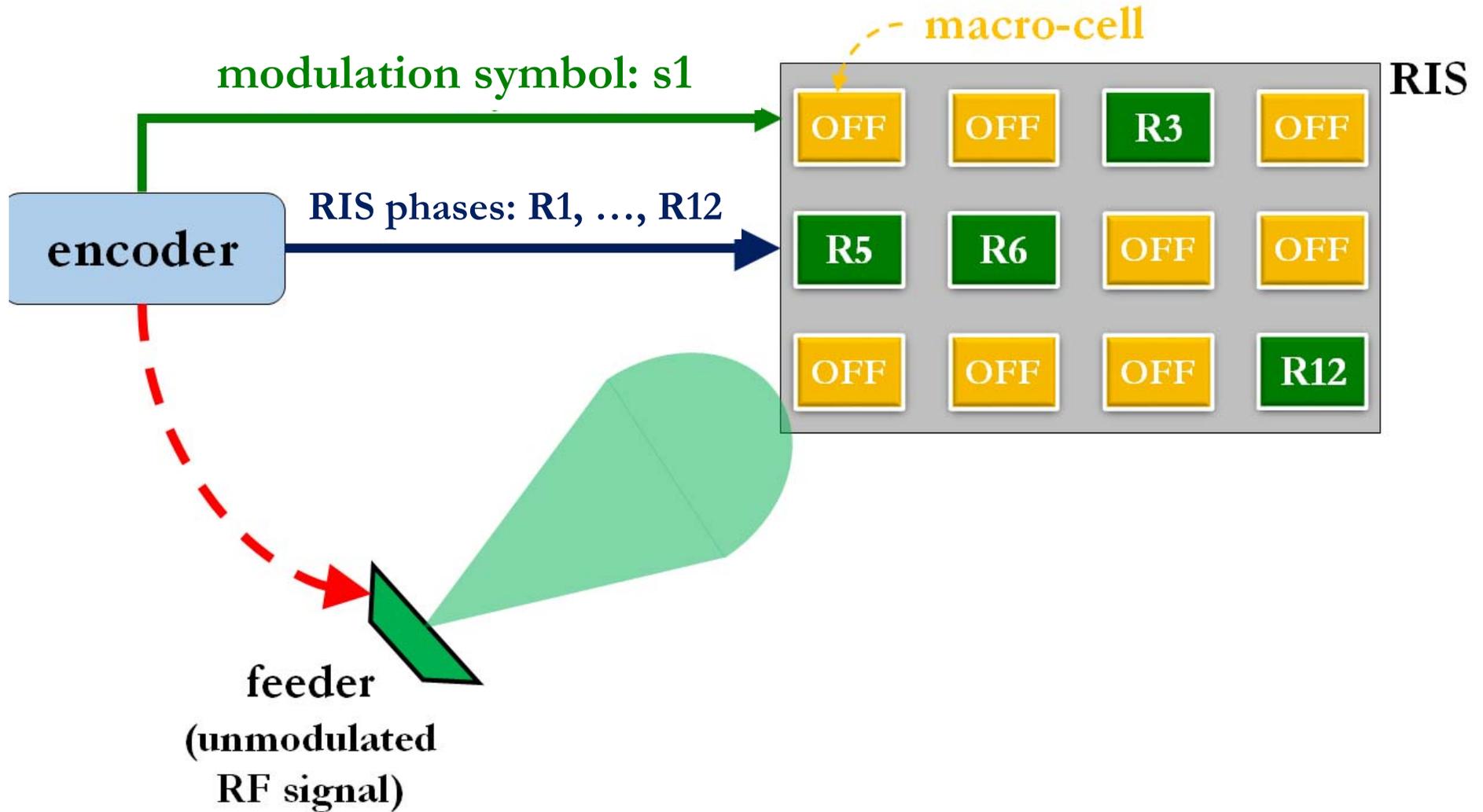
Joint Encoding for RISs

Rethinking Communication-Theoretic Models



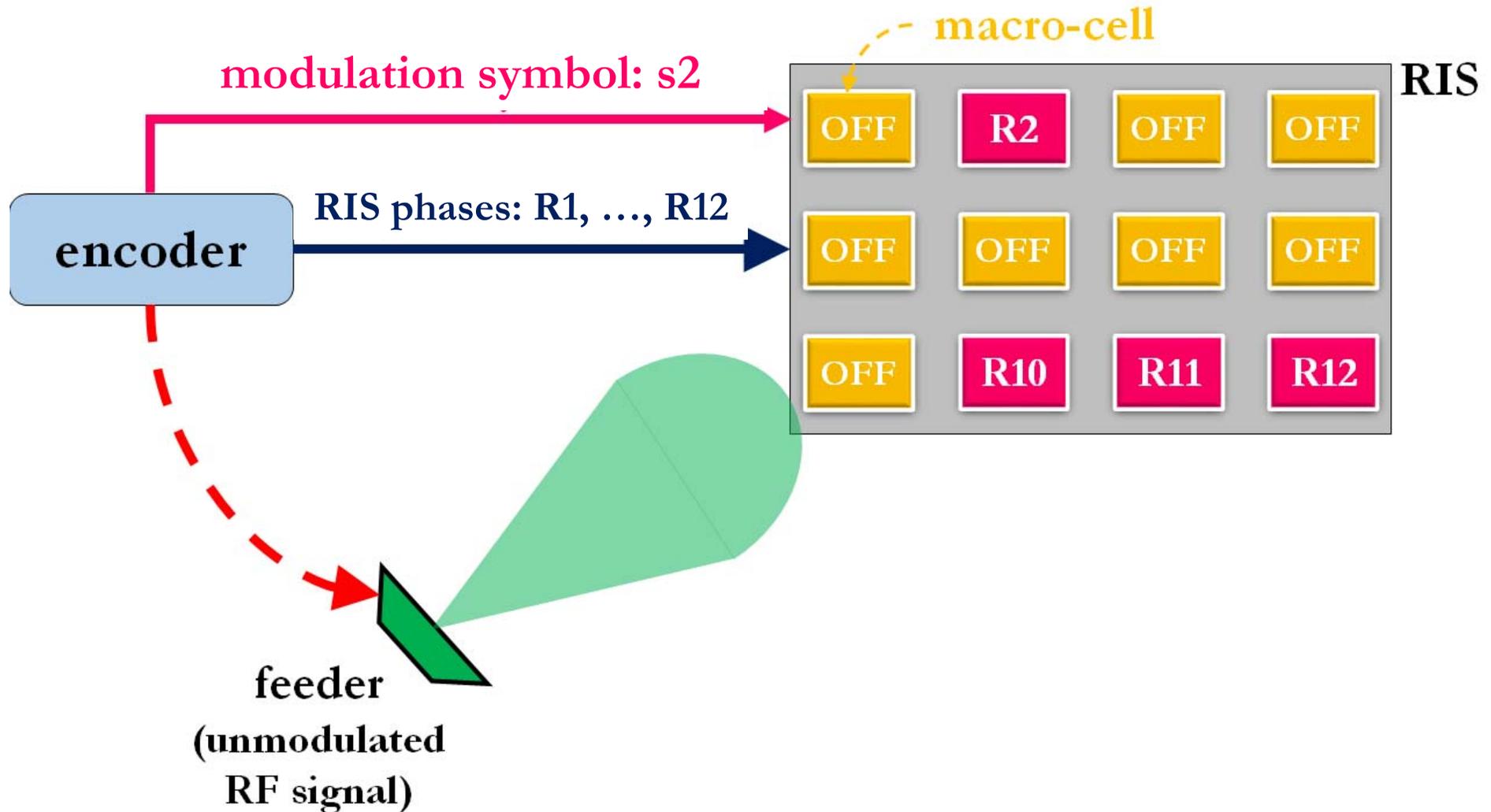
Joint Encoding for RISs (index-based modulation)

Rethinking Communication-Theoretic Models

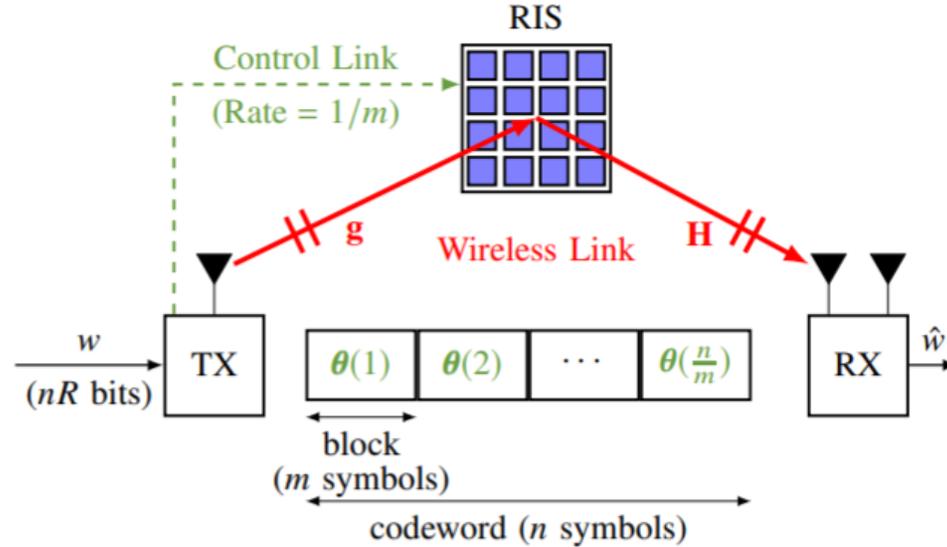


Joint Encoding for RISs (index-based modulation)

Rethinking Communication-Theoretic Models



Joint Encoding for RISs (*capacity achieving*)



Proposition 1: The capacity of the channel (1) is given as

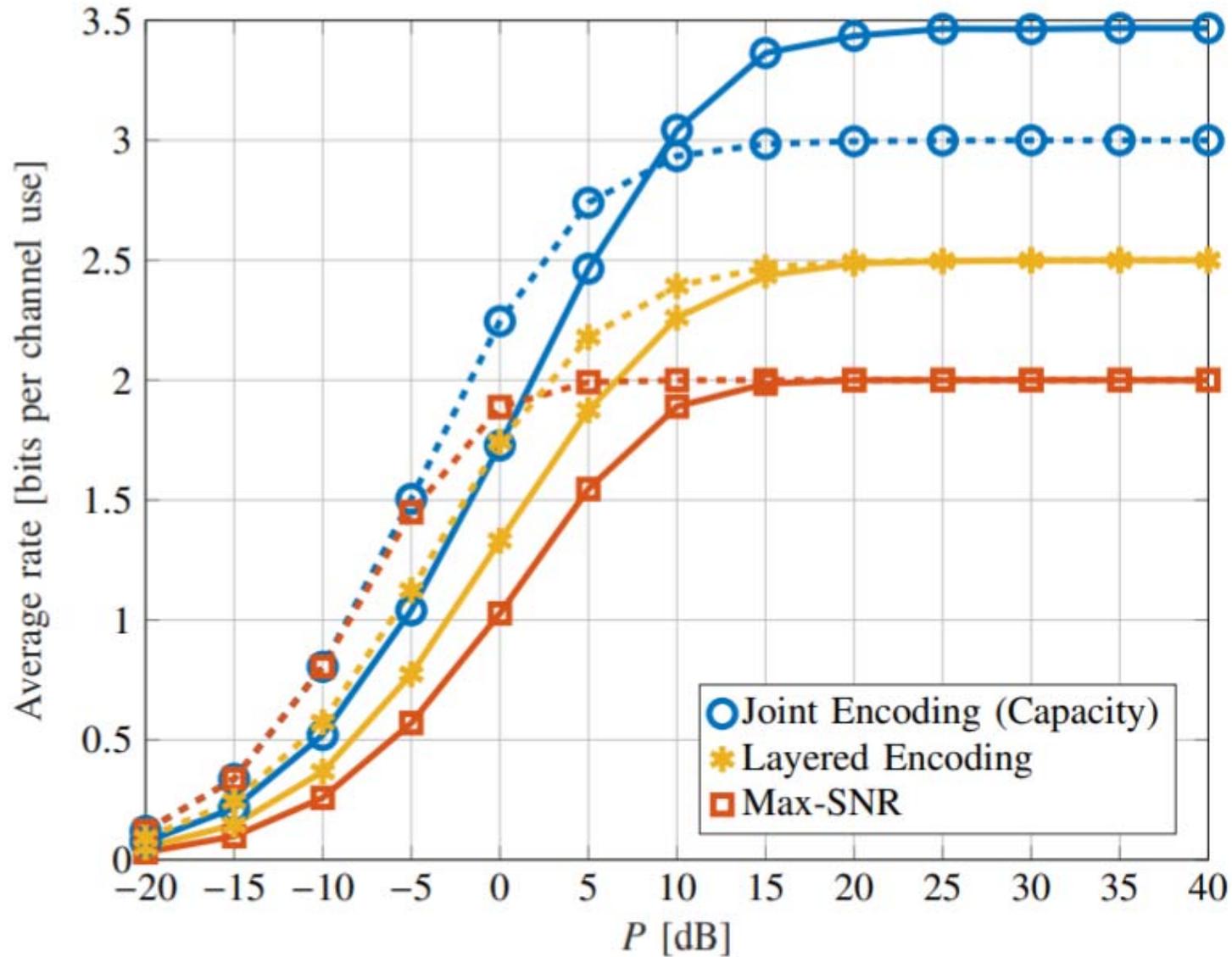
$$C(\mathbf{g}, \mathbf{H}) = -N \log_2(e) - \frac{1}{m} \min_{\substack{p(\mathbf{x}, \boldsymbol{\theta}): \\ \mathbb{E}[|x_i|^2] \leq P, \\ \mathbf{x} \in \mathcal{B}^m, \boldsymbol{\theta} \in \mathcal{A}^K}} \sum_{\mathbf{x} \in \mathcal{B}^m} \sum_{\boldsymbol{\theta} \in \mathcal{A}^K} p(\mathbf{x}, \boldsymbol{\theta}) \mathbb{E}[f_c(\mathbf{x}, \boldsymbol{\theta}, \mathbf{Z})], \quad (5)$$

where we have defined function

$$f_c(\mathbf{x}, \boldsymbol{\theta}, \mathbf{Z}) \triangleq \log_2 \left(\sum_{\mathbf{x}' \in \mathcal{B}^m} \sum_{\boldsymbol{\theta}' \in \mathcal{A}^K} p(\mathbf{x}', \boldsymbol{\theta}') \exp \left(-\|\mathbf{Z} + \mathbf{H}(\mathbf{S}\mathbf{g}\mathbf{x} - \mathbf{S}'\mathbf{g}\mathbf{x}')\|_F^2 \right) \right) \quad (6)$$

with matrices $\mathbf{S} = \text{diag}(\exp(j\theta_1), \dots, \exp(j\theta_K))$ and $\mathbf{S}' = \text{diag}(\exp(j\theta'_1), \dots, \exp(j\theta'_K))$, and the expectation in (5) being taken with respect to a matrix \mathbf{Z} whose elements are i.i.d. as $\mathcal{CN}(0, 1)$.

Joint Encoding for RISs (capacity achieving)

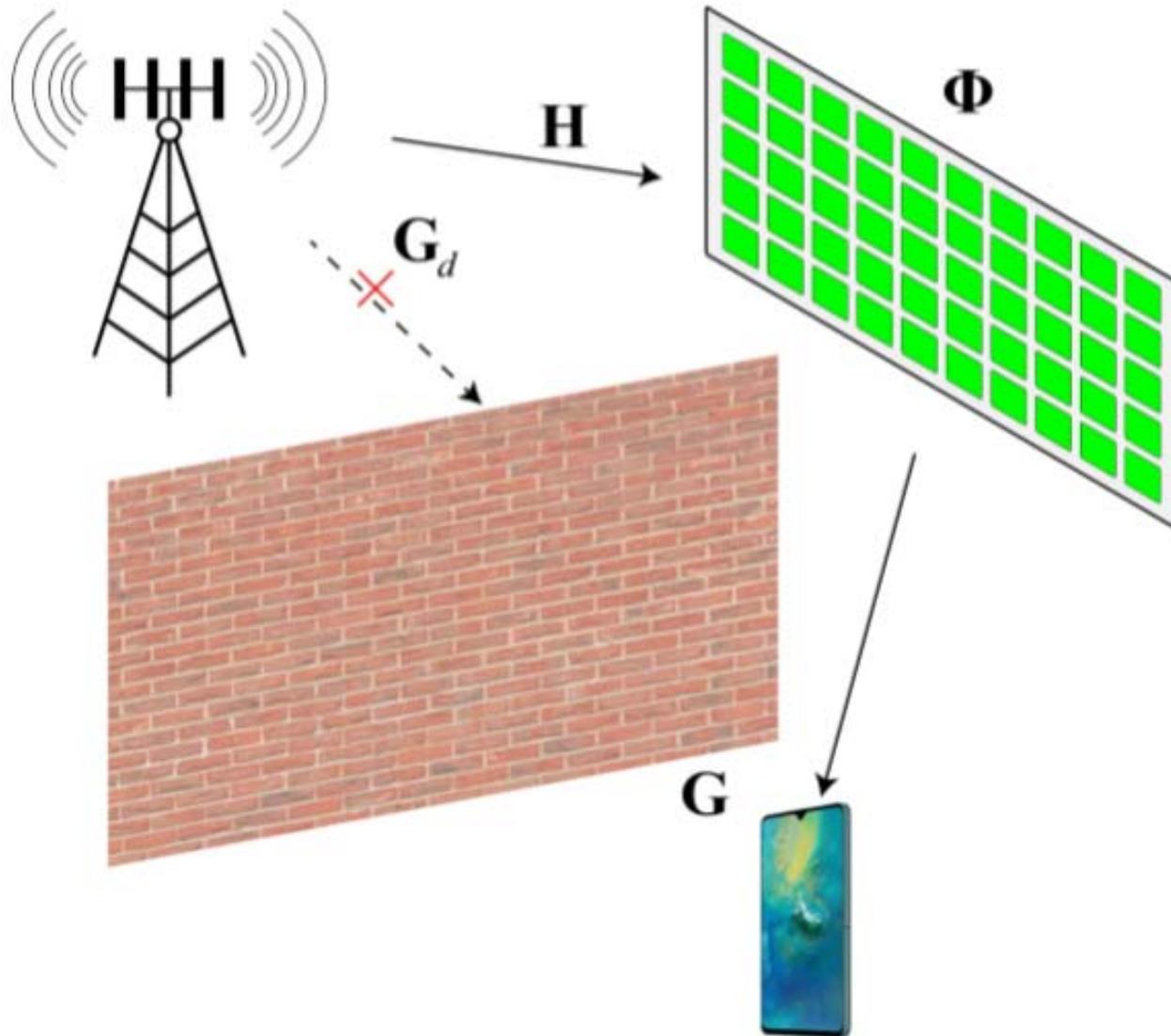


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RIS-Aided Transmission: MIMO System Model



Making Information Transmission More Reliable

... Amount of Fading (RMT) $\sim 1/N$...

Proposition 3: Define $D = \{RR, LR\}$, and assume $s_1 = 0$ and $N \gg 1$. Let $AF_{\text{SNR}_D} = \mathbb{V} \{ \text{SNR}_D \} / (\mathbb{E} \{ \text{SNR}_D \})^2$ be the AF of SNR_D . As a function of N , while keeping the other system parameters fixed, the following scaling laws hold true:

$$\begin{aligned} \mathbb{E} \{ \text{SNR}_D \} &\stackrel{N \gg 1}{\propto} o_{e0} N^1 \mathbf{1}(c_1 = 0) + o_{e1} N^2 \mathbf{1}(c_1 \neq 0) \\ \mathbb{V} \{ \text{SNR}_D \} &\stackrel{N \gg 1}{\propto} o_{v0} N^2 \mathbf{1}(c_1 = 0) + o_{v1} N^3 \mathbf{1}(c_1 \neq 0) \quad (20) \\ AF_{\text{SNR}_D} &\stackrel{N \gg 1}{\propto} \frac{o_{v0}}{o_{e0}^2} N^0 \mathbf{1}(c_1 = 0) + \frac{o_{v1}}{o_{e1}^2} N^{-1} \mathbf{1}(c_1 \neq 0) \end{aligned}$$

where o_{e0} , o_{e1} , o_{v0} , and o_{v1} are defined in Table III.

Impact of Phase Noise on Inexpensive Antennas

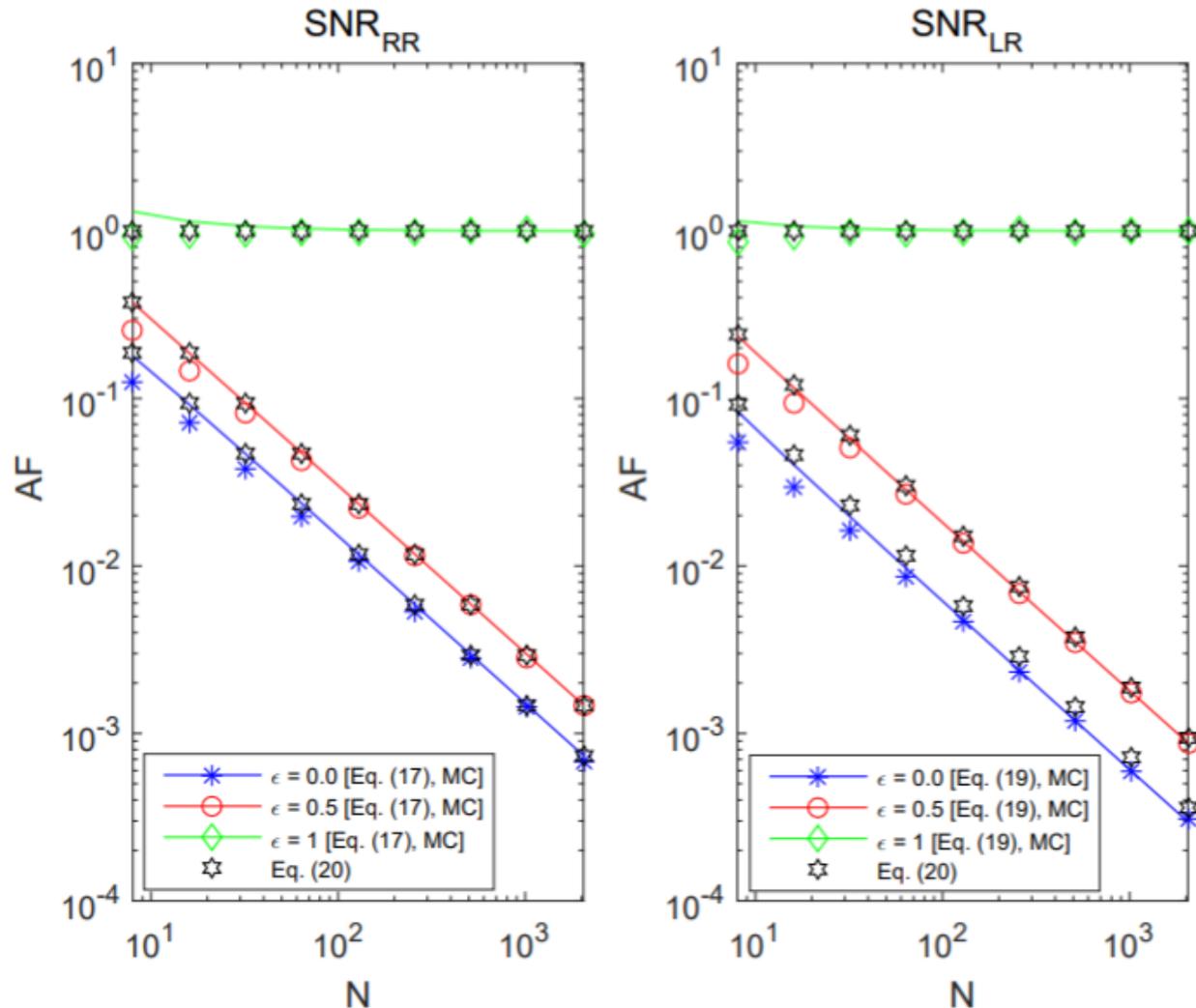


Fig. 1: AF ($\gamma_0 = 1$, $N_T = N_R = 4$, $\delta_n \sim \mathcal{U}(-\varepsilon\pi, \varepsilon\pi)$).

Impact of Phase Noise on Inexpensive Antennas

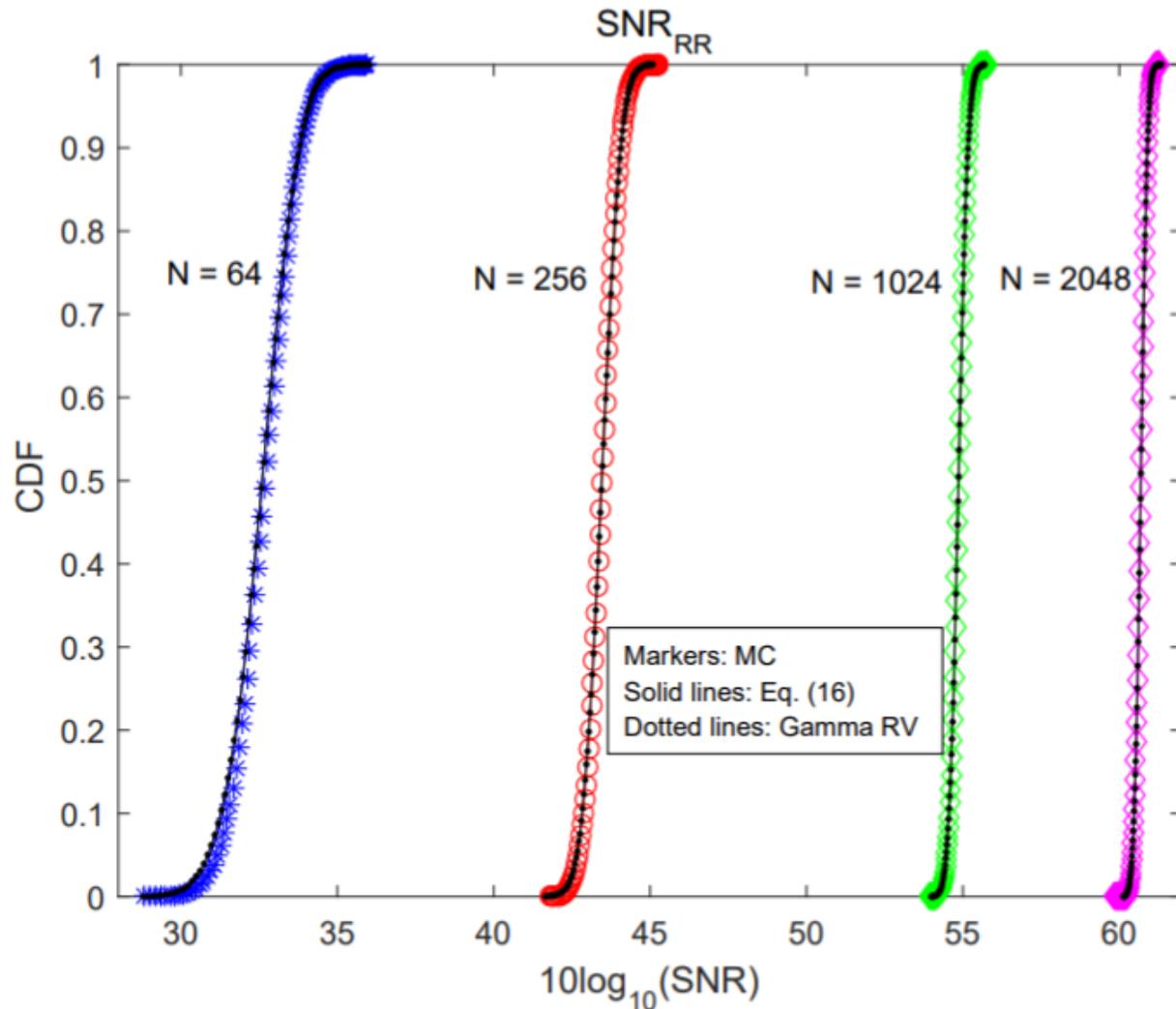


Fig. 2: CDF ($\gamma_0 = 1$, $N_T = N_R = 4$, $\delta_n \sim \mathcal{U}(-\varepsilon\pi, \varepsilon\pi)$).

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Overhead-Aware Optimization of RISs

Active/Passive Beamforming, Power, Bandwidth

Overhead-Aware Optimization of RISs

Active/Passive Beamforming, Power, Bandwidth

Denoting by T the total duration of the time slot comprising channel estimation, feedback, and data communication, the system achievable rate can be expressed as

$$R(p, B, p_F, B_F, \Phi, \mathbf{q}, \mathbf{w}) = \left(1 - \frac{T_E + T_F}{T}\right) B \log \left(1 + \frac{p |\mathbf{w}^H \mathbf{G} \Phi \mathbf{H} \mathbf{q}|^2}{BN_0}\right), \quad (1)$$

while the system energy efficiency is written as

$$\text{EE}(p, B, p_F, B_F, \Phi, \mathbf{q}, \mathbf{w}) = \frac{R(p, B, p_F, B_F, \Phi, \mathbf{q}, \mathbf{w})}{P_{tot}(p, B, p_F, B_F)}, \quad (2)$$

wherein P_{tot} denotes the total power consumption in the whole timeframe T , which is equal to

$$P_{tot}(p, B, p_F, B_F) = P_E + \frac{1}{T} [(T - T_E - T_F)\mu p + \mu_F p_F T_F + T P_c], \quad (3)$$

Overhead-Aware Optimization of RISs

Active/Passive Beamforming, Power, Bandwidth

Denoting by T the total duration of the time slot comprising channel estimation, feedback, and data communication, the system achievable rate can be expressed as

$$R(p, B, p_F, B_F, \Phi, \mathbf{q}, \mathbf{w}) = \left(1 - \frac{T_E + T_F}{T}\right) B \log \left(1 + \frac{p |\mathbf{w}^H \mathbf{G} \Phi \mathbf{H} \mathbf{q}|^2}{BN_0}\right), \quad (1)$$

while the system energy efficiency is written as

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$$P_{tot}(p, B, p_F, B_F) = P_E + \frac{1}{T} [(T - T_E - T_F)\mu p + \mu_F p_F T_F + T P_c], \quad (3)$$

Overhead-Aware Optimization of RISs

Joint Active and Passive Beamforming Optimization

$$\begin{aligned} & \max_{\Phi, \mathbf{q}, \mathbf{w}} |\mathbf{w}^H \mathbf{G} \Phi \mathbf{H} \mathbf{q}|^2 \\ & \text{s.t. } \|\mathbf{q}\| = \|\mathbf{w}\| = 1, 0 \leq \phi_n \leq 2\pi, \forall n = 1, \dots, N. \end{aligned}$$

Proposition 1: For any p, B, p_F, B_F , defining

$$\bar{j}(i) = \operatorname{argmax}_j \mu_{j,H}^2 \left(\sum_{n=1}^N \left| \mathbf{v}_{i,G}^{(n)} \right| \left| \mathbf{u}_{j,H}^{(n)} \right| \right)^2, \forall i = 1, \dots, r_G, \bar{i} = \operatorname{argmax}_i \mu_{i,G}^2 \mu_{\bar{j}(i),H}^2 \left(\sum_{n=1}^N \left| \mathbf{v}_{i,G}^{(n)} \right| \left| \mathbf{u}_{\bar{j}(i),H}^{(n)} \right| \right)^2 \quad (8)$$

the global maximizer of the upper-bound in (6) is obtained by setting the beamforming vector as $\mathbf{q} = \mathbf{v}_{\bar{j}(\bar{i}),H}$, the receive filter as $\mathbf{w} = \mathbf{u}_{\bar{i},G}$, and the RIS phase shifts are $\phi_n = -\angle \left\{ \mathbf{v}_{\bar{i},G}^{*(n)} \mathbf{u}_{\bar{j}(\bar{i}),H}^{(n)} \right\}$, with $(*)$ denoting complex conjugate.

Overhead-Aware Optimization of RISs

Joint Spectral/Energy Efficiency Optimization

$$\max_{p, p_F, B} \left\{ R(p, p_F, B, \Phi^{\text{opt}}, \mathbf{q}^{\text{opt}}, \mathbf{w}^{\text{opt}}), \text{EE}(p, p_F, B, \Phi^{\text{opt}}, \mathbf{q}^{\text{opt}}, \mathbf{w}^{\text{opt}}) \right\}$$

$$\text{s.t. } p + p_F \leq P_{\max}$$

$$0 \leq B \leq B_{\max}, p \geq 0, p_F \geq 0$$

$$\frac{d}{(B_{\max} - B) \log \left(1 + \frac{p_F |h_F|^2}{(B_{\max} - B) N_0} \right)} \leq \beta,$$

Algorithm 3 Rate-EE Maximization

Set $M > 0$ and compute $\Delta = \frac{B_{\max} \log \left(1 + \frac{P_{\max} |h_F|^2}{B_{\max} N_0} \right) - \frac{d}{\beta}}{M}$

for $m = 1, \dots, M$ **do**

$$\tilde{y}_m = \frac{d}{\beta} + (m - 1)\Delta;$$

Solve (39) by bisection over t and compute

$$F_m = \min \left\{ \alpha (R(p^*, p_F^*, B^*, \Phi^{\text{opt}}, \mathbf{q}^{\text{opt}}, \mathbf{w}^{\text{opt}}) - R_{\text{opt}}), (1 - \alpha) (\text{EE}(p^*, p_F^*, B^*, \Phi^{\text{opt}}, \mathbf{q}^{\text{opt}}, \mathbf{w}^{\text{opt}}) - \text{EE}_{\text{opt}}) \right\} \quad (40)$$

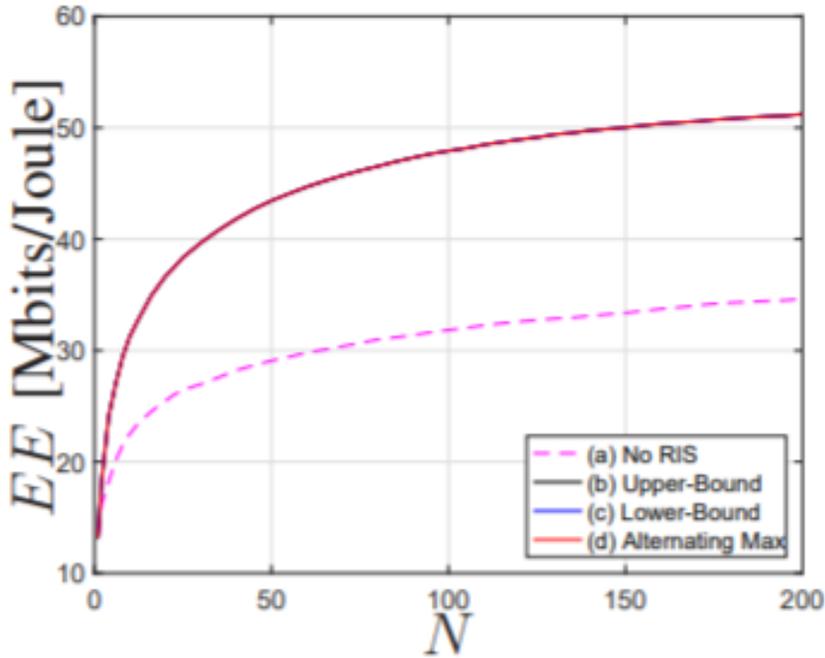
end for

Compute $m^* = \text{argmax } F_m$;

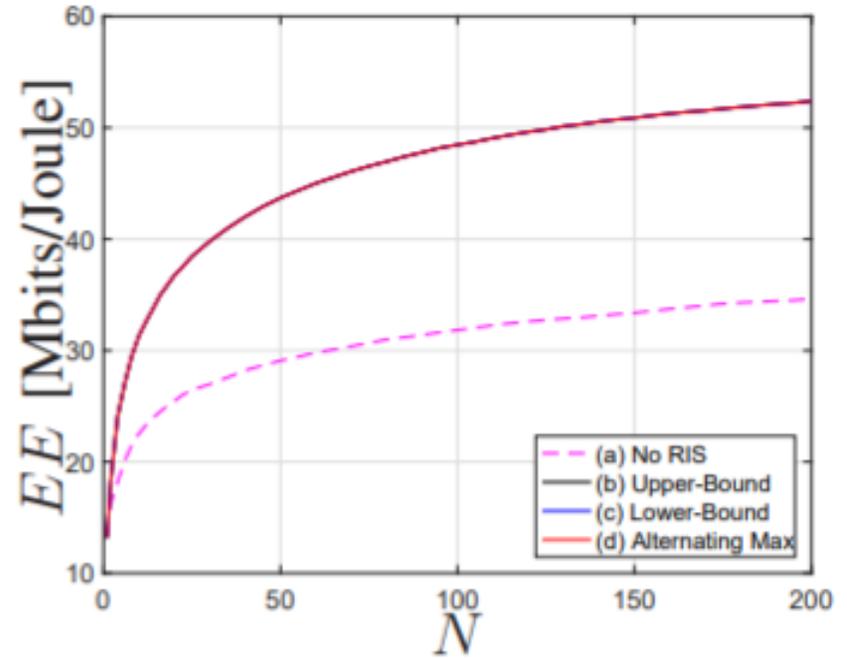
Output $p_{m^*}^*, p_{m^*, F}^*, B_{m^*}^*, B_{m^*, F}^* = B_{\max} - B_{m^*}^*$;

Overhead-Aware Optimization of RISs

$$\text{EE} - N_r = 1 \text{ and } N_t = 1$$



(a) EE for $T_0 = 0.8 \mu s$, $P_0 = 2.5 \text{ mW}$

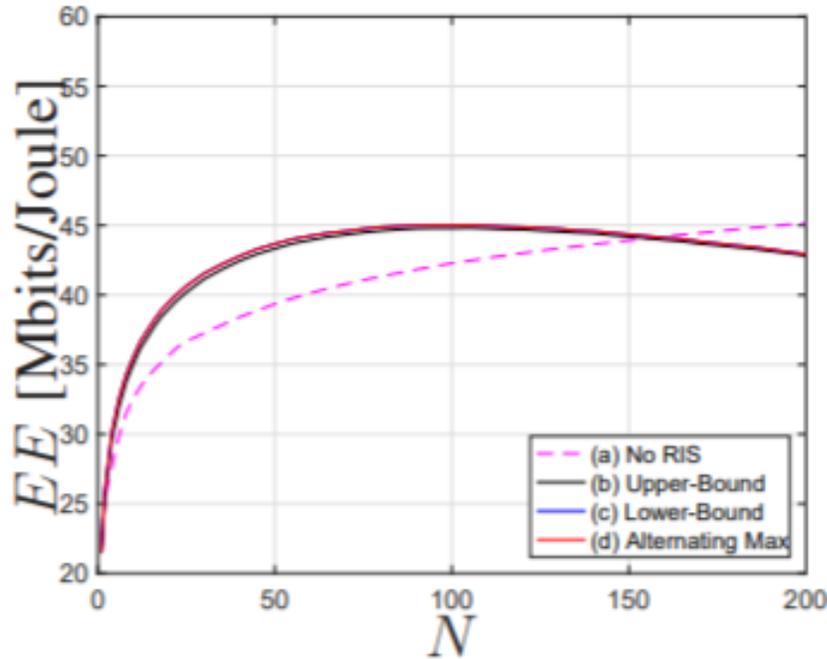


(b) EE for $T_0 = 0.15 \mu s$, $P_0 = 0.5 \text{ mW}$

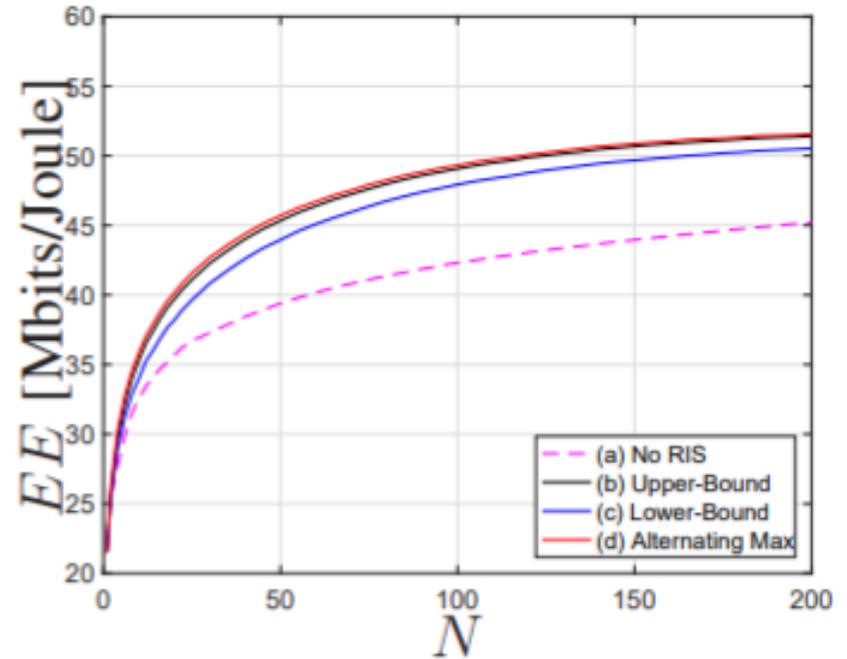
Fig. 4: Achieved EE in [Mbit/Joule] as a function of N for $N_T = N_R = 1$.

Overhead-Aware Optimization of RISs

$$\text{EE} - N_r = 1 \text{ and } N_t = 8$$



(a) EE for $T_0 = 0.8 \mu s$, $P_0 = 2.5 \text{ mW}$

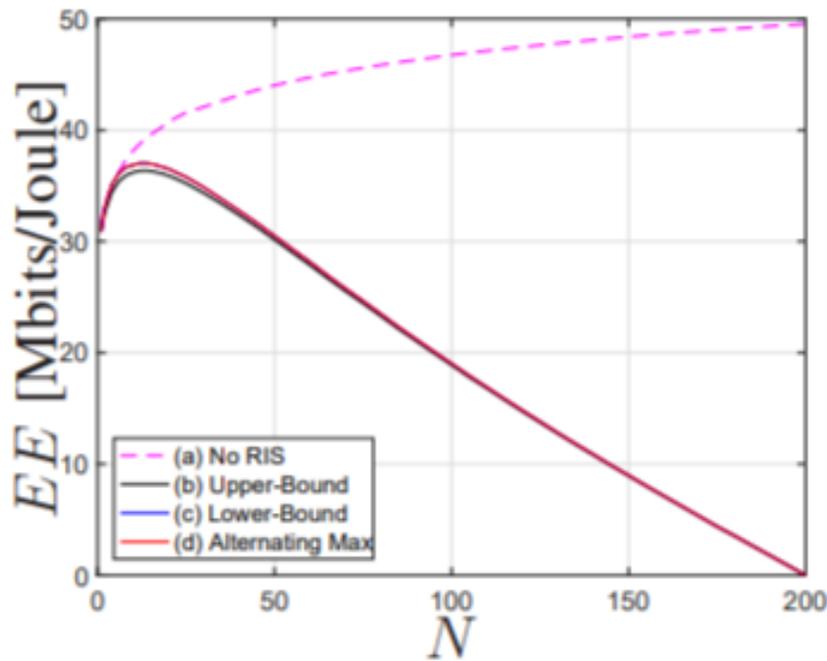


(b) EE for $T_0 = 0.15 \mu s$, $P_0 = 0.5 \text{ mW}$

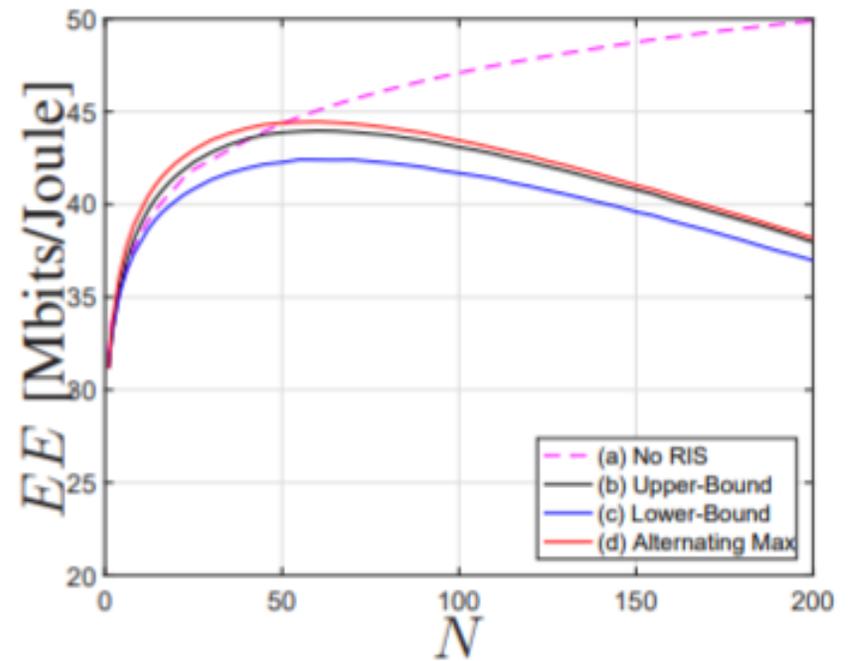
Fig. 5: Achieved EE in [Mbit/Joule] as a function of N for $N_T = 1$, $N_R = 8$.

Overhead-Aware Optimization of RISs

$$EE - N_r = 8 \text{ and } N_t = 8$$



(a) EE for $T_0 = 0.8 \mu s$, $P_0 = 2.5 \text{ mW}$



(b) EE for $T_0 = 0.15 \mu s$, $P_0 = 0.5 \text{ mW}$

Fig. 6: Achieved EE in [Mbit/Joule] as a function of N for $N_T = 8$, $N_R = 8$.

*Programming the Environment: Towards **Wireless 2.0***

Di Renzo et al. *EURASIP Journal on Wireless Communications and Networking* (2019) 2019:129
<https://doi.org/10.1186/s13638-019-1438-9>

EURASIP Journal on Wireless
Communications and Networking

REVIEW

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Smart radio environments empowered by reconfigurable AI meta-surfaces: an idea whose time has come



Marco Di Renzo^{1*} , Merouane Debbah², Dinh-Thuy Phan-Huy³, Alessio Zappone⁴, Mohamed-Slim Alouini⁵, Chau Yuen⁶, Vincenzo Sciancalepore⁷, George C. Alexandropoulos⁸, Jakob Hoydis⁹, Haris Gacanin¹⁰, Julien de Rosny, Ahcene Bounceur¹², Geoffroy Lerosey¹³ and Mathias Fink¹¹

Abstract

Future wireless networks are expected to constitute a distributed intelligent wireless communications, sensing, and computing platform, which will have the challenging requirement of interconnecting the physical and digital worlds in a seamless and sustainable manner. Currently, two main factors prevent wireless network operators from building such networks: (1) the lack of control of the wireless environment, whose impact on the radio waves cannot be customized, and (2) the current operation of wireless radios, which consume a lot of power because new signals are generated whenever data has to be transmitted. In this paper, we challenge the usual “more data needs more power and emission of radio waves” status quo, and motivate that future wireless networks necessitate a smart radio environment: a transformative wireless concept, where the environmental objects are coated with artificial thin films of electromagnetic and reconfigurable material (that are referred to as reconfigurable intelligent meta-surfaces), which are capable of sensing the environment and of applying customized transformations to the radio waves. Smart radio environments have the potential to provide future wireless networks with uninterrupted wireless connectivity,

Wireless 2.0: 6G Wireless + 3G Metasurfaces (JSAC)

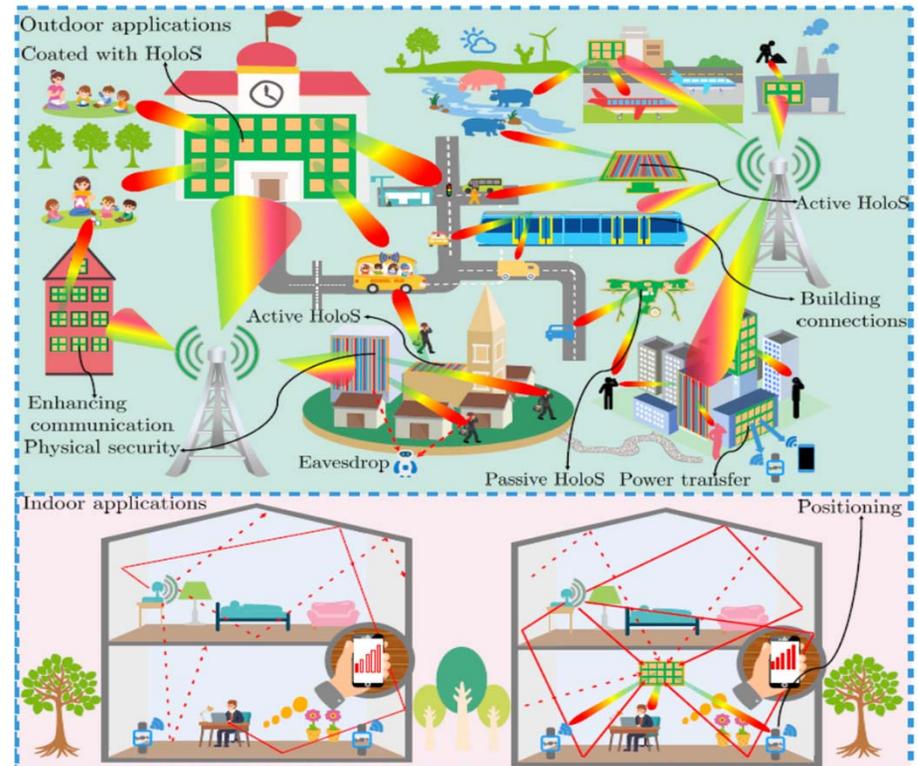
Smart Radio Environments Empowered by Reconfigurable Intelligent Surfaces: How it Works, State of Research, and Road Ahead

Marco Di Renzo, *Fellow, IEEE*, Alessio Zappone, *Senior Member, IEEE*, Merouane Debbah, *Fellow, IEEE*, Mohamed-Slim Alouini, *Fellow, IEEE*, Chau Yuen, *Senior Member, IEEE*, Julien de Rosny, and Sergei Tretyakov, *Fellow, IEEE*

[arXiv:2004.09352](https://arxiv.org/abs/2004.09352) (76 pages)

Abstract—What is a reconfigurable intelligent surface? What is a smart radio environment? What is a metasurface? How do metasurfaces work and how to model them? How to reconcile the mathematical theories of communication and electromagnetism? What are the most suitable uses and applications of reconfigurable intelligent surfaces in wireless networks? What are the most promising smart radio environments for wireless applications? What is the current state of research? What are the most important and challenging research issues to tackle?

These are a few of the many questions that we investigate in this short opus, which has the threefold objective of introducing the emerging research field of smart radio environments empowered by reconfigurable intelligent surfaces, putting forth the need of reconciling and reuniting C. E. Shannon's mathematical theory of communication with G. Green's and J. C. Maxwell's mathematical theories of electromagnetism, and reporting pragmatic guidelines and recipes for employing appropriate physics-based models of metasurfaces in wireless communications.



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- ❑ H2020 ARIADNE (6 million Euro, Nov. 2019)
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 - ❑ University of Piraeus Research Center, Greece
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 - ❑ CentraleSupélec, France
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The Road Ahead

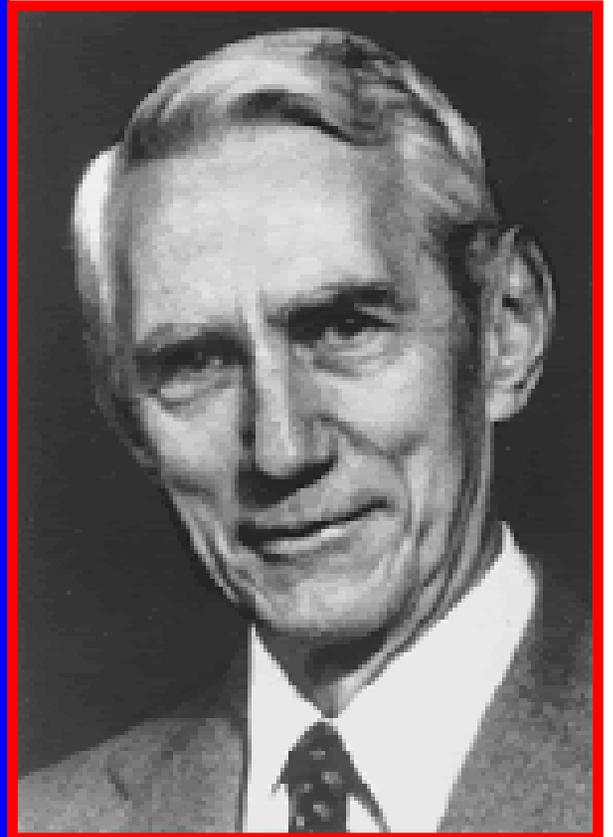
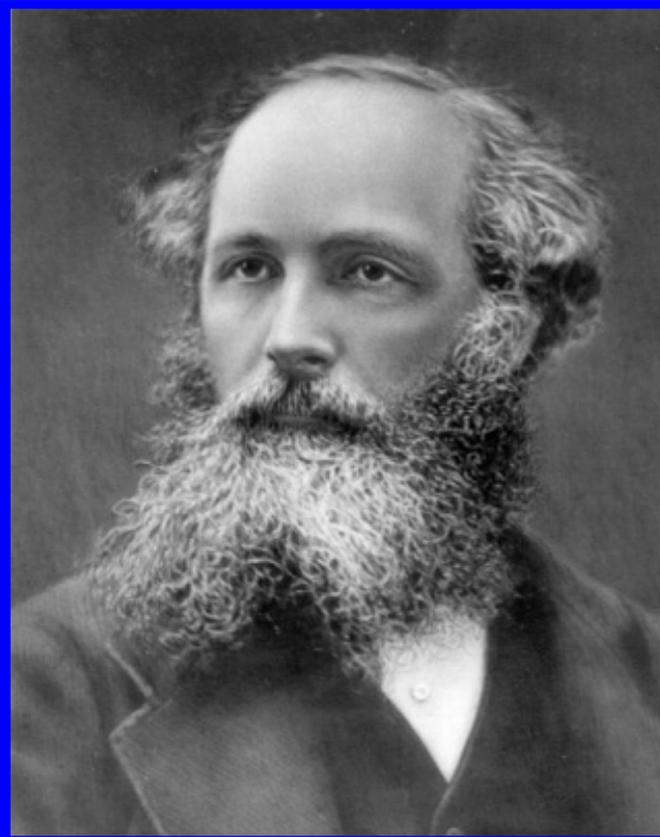
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- ❑ Path-loss and channel modeling
- ❑ Fundamental performance limits
- ❑ Robust optimization and resource allocation
- ❑ Constrained system design and optimization
- ❑ EM-based communications: “Layer-0” networking
- ❑ Large-scale networks: Deployment, analysis, optimization
- ❑ Ray tracing and system-level simulators
- ❑ Beyond far-field communications
- ❑ Beyond communications
- ❑ Advantages and limitations

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... do RISs bring any (substantial) gains as compared with other well-established technologies in wireless networks ?

The Road Ahead: Reconciling COMM, SP, IT, EM, ...

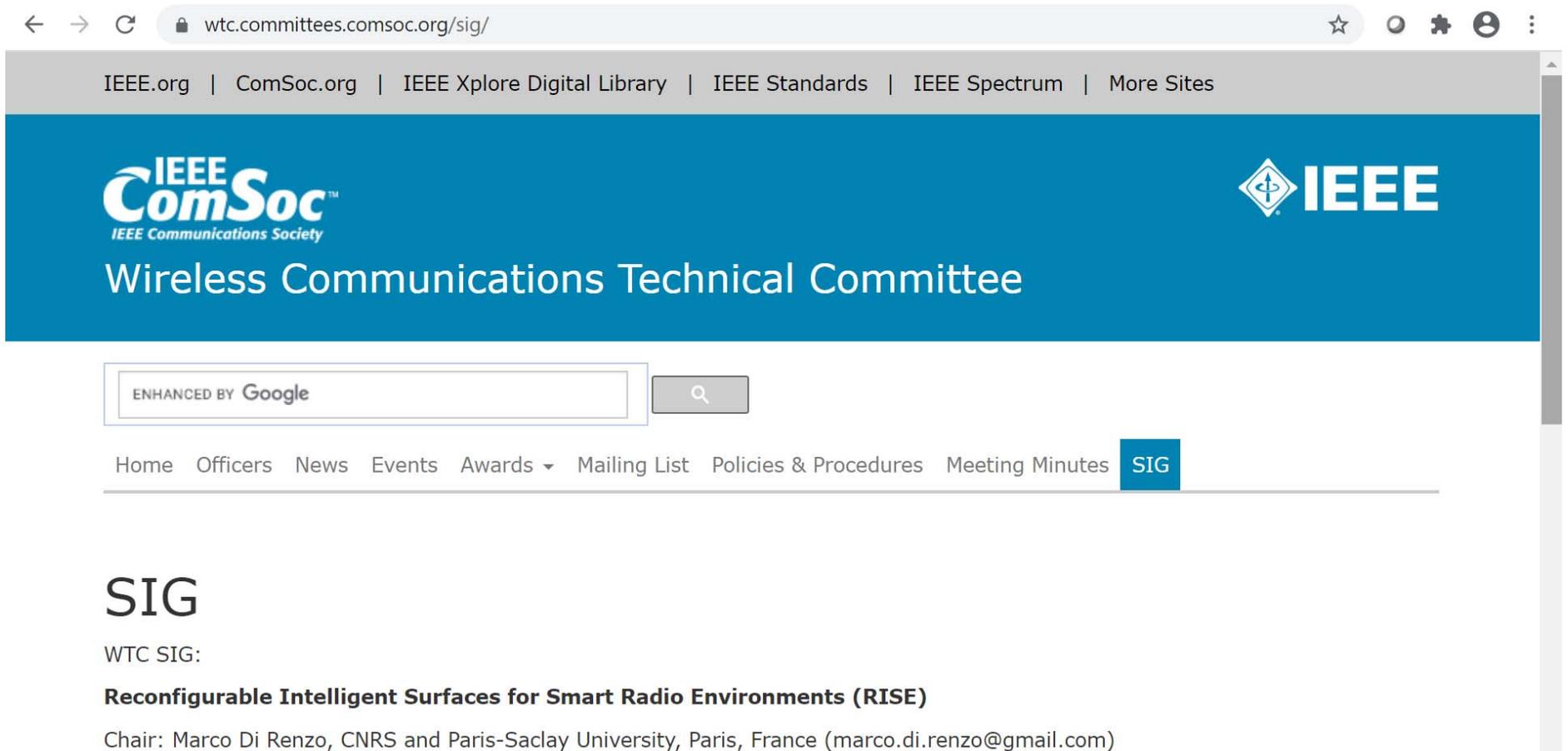


G. Green, “An Essay on the Application of Mathematical Analysis to the Theories of Electricity and Magnetism”, 1828.

J. C. Maxwell, “A Dynamical Theory of the Electromagnetic Field”, 1865.

C. E. Shannon, “A (The) Mathematical Theory of Communication”, 1948.

Special Interest Group @ WTC: “RISE”



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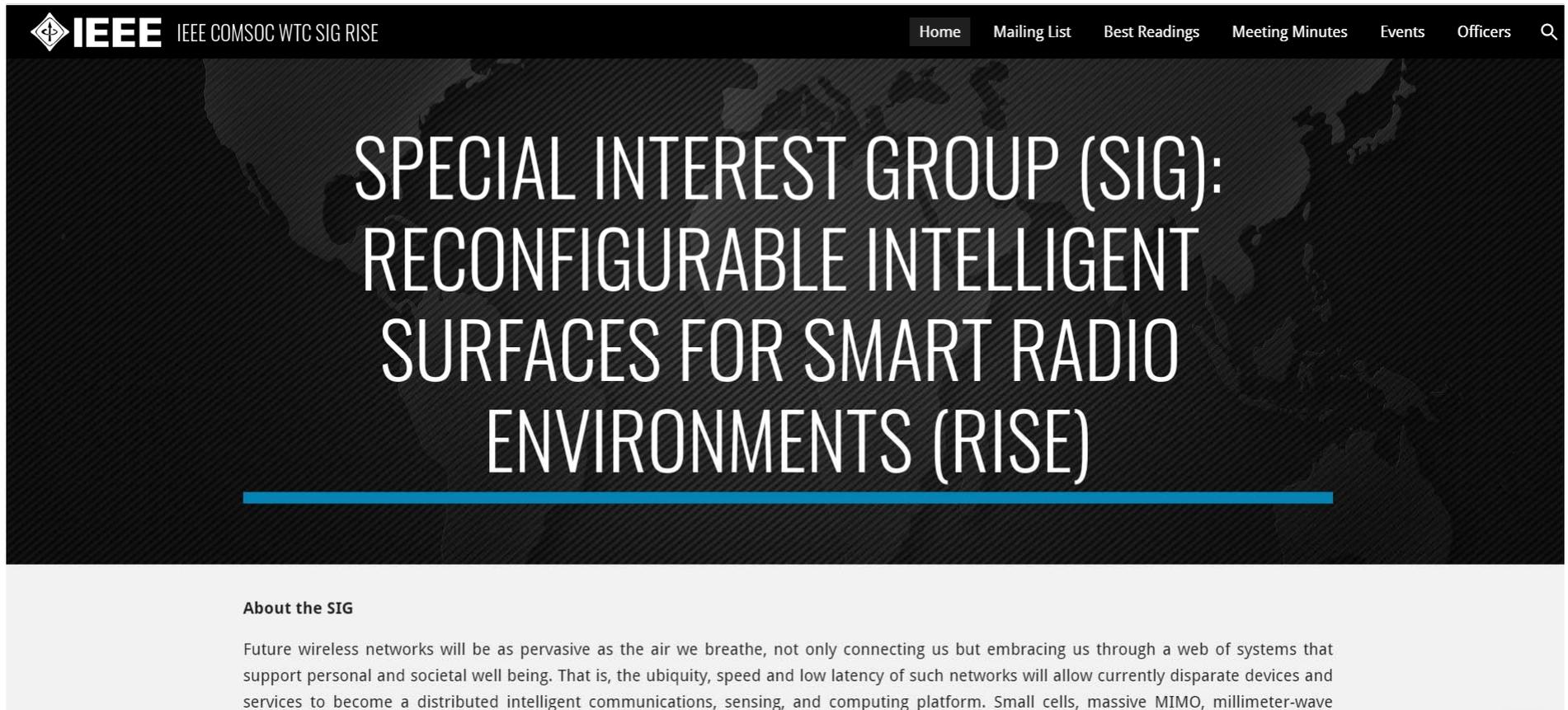
Reconfigurable Intelligent Surfaces for Smart Radio Environments (RISE)

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RIS @ IEEE-COMSOC

Special Interest Group @ WTC: “RISE”

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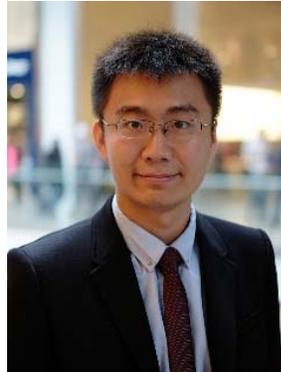
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SPECIAL INTEREST GROUP (SIG): RECONFIGURABLE INTELLIGENT SURFACES FOR SMART RADIO ENVIRONMENTS (RISE)

About the SIG

Future wireless networks will be as pervasive as the air we breathe, not only connecting us but embracing us through a web of systems that support personal and societal well being. That is, the ubiquity, speed and low latency of such networks will allow currently disparate devices and services to become a distributed intelligent communications, sensing, and computing platform. Small cells, massive MIMO, millimeter-wave

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**Emerging Technology Initiative on “RIS” @
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Wireless Networks Empowered by Reconfigurable Intelligent Surfaces

Publication Date

Third Quarter 2020

Manuscript Submission Deadline

15 December 2019

Open Special Issues

Reconfigurable Intelligent Surface-Based Communications for 6G Wireless Networks, [IEEE Open Journal of the Communications Society](#), First Quarter 2021.

<https://www.comsoc.org/publications/journals/ieee-ojcoms/cfp/reconfigurable-intelligent-surface-based-communications-6g>

Manuscript Submission Deadline: 1 September 2020

Intelligent Surfaces for Smart Wireless Communications, [IEEE Transactions on Cognitive Communications and Networking](#), Second Quarter 2021.

<https://www.comsoc.org/publications/journals/ieee-tccn/cfp/intelligent-surfaces-smart-wireless-communications>

Manuscript Submission Deadline: 1 September 2020

Wireless Communications with Reconfigurable Intelligent Surfaces, [China Communications](#), Feature Topic, Vol.18, No.2, 2021.

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WS-01: RECONFIGURABLE INTELLIGENT SURFACES FOR WIRELESS COMMUNICATION FOR BEYOND 5G

WS-01: RECONFIGURABLE INTELLIGENT SURFACES FOR WIRELESS COMMUNICATION FOR BEYOND 5G

5G wireless networks will be rolled out shortly, featuring innovative technologies such as infrastructure densification, antenna densification, use of frequency bands in the mmWave range, which promise to achieve the targets of 1000x higher data-rates and 2000x higher bit-per-Joule energy efficiency compared to the previous wireless generation. However, as 5G networks take their final form, connectivity demands continue to increase at an exponential rate and new services pose more constraints on the performance that end-users expect.

In order to face these new challenges, it will not be sufficient to develop only a more performing transmission technology, as it was the case for all previous wireless generations, which focused only on improving the efficiency of the transmission and reception technology. Being simply able to transmit data at a faster rate does not ensure the flexibility required to accommodate diverse classes of users with extremely diverse service requirements. Besides developing faster transmission technologies, future research efforts should be aimed also at improving the network infrastructure itself, making it flexible enough to automatically adapt to sudden wireless scenario changes and rapid traffic evolutions, and customizable according to traffic conditions and requirements.

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- **ICT-ARIADNE (H2020, 5G-PPP, grant 871464)**
 - **November 1st, 2019 – October 31st, 2022**
- A collaborative research project on RISs & AI**



Marco Di Renzo, Ph.D., H.D.R.

Directeur de Recherche CNRS (CNRS Professor)

Highly Cited Researcher, Web of Science

IEEE Fellow, IEEE Communications Society

Editor-in-Chief, IEEE Communications Letters

Distinguished Lecturer, IEEE Communications Society

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